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Volume II - Appendices A through K

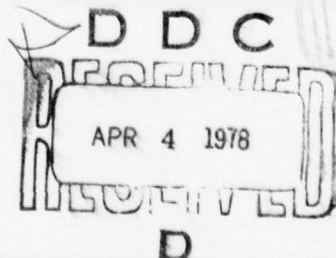
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This technical report has been reviewed and is approved for publication.

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20. structure integral trim system produced specified steady-state performance and limit accommodation in the presence of simulated degradation effects and instrument errors.

The resulting control logic was extensively tested on a hybrid simulation of the F100 turbofan and will be used to control an engine in an altitude test cell. The details of the design procedure, linear model analysis and a summary of digital and hybrid simulation tests results are presented in this report.

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FOREWORD

This final report was submitted by Systems Control, Inc. (Vt), Palo Alto CA under Air Force Contract F33615-75-C-2053. The effort was sponsored by the National Aeronautics and Space Administration, Lewis Research Center, Cleveland OH, and the Air Force Aero-Propulsion Laboratory, Air Force Systems Command, Wright-Patterson Air Force Base OH under Project 3066, Task 306603 and Work Unit 30660370 with Charles A. Skira, AFAPL/TBC, as Project Engineer. This program was initiated with FY 75 Aero-Propulsion Laboratory Director's Funds. Dr. W. Earl Hall, Jr. of Systems Control, Inc. (Vt) was Project Manager for this effort. Project Engineer was Dr. Ronald L. De Hoff. Ms. Deborah Buenz responsible for the technical publication of this report.

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This report consists of two volumes:

Volume I - Development of F100 Control System

Volume II - Appendices A through K

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APPENDIX A

EIGENSYSTEM SENSITIVITY MINIMIZATION AND CALCULATION

A.1 EIGENVALUE DERIVATIVES

Consider an $n \times n$ matrix A with n distinct eigenvalues $\lambda_1, \lambda_2, \dots, \lambda_n$. Let the diagonal matrix Λ be given as

$$\Lambda = \begin{bmatrix} \lambda_1 & & 0 \\ & \lambda_2 & \\ 0 & & \ddots \\ & & & \lambda_n \end{bmatrix} \quad (\text{A.1})$$

Let the i th column of the matrix U, u_i be the right eigenvector corresponding to the eigenvalue λ_i . Then

$$AU = U\Lambda \quad (\text{A.2})$$

Let the i th column of the matrix V, v_i be the left eigenvector corresponding to the eigenvalue λ_i . Then

$$V^H A = \Lambda V^H \quad (\text{A.3})$$

or

$$A^H V = V \Lambda^H = V \bar{\Lambda} \quad (\text{A.4})$$

where the "H" superscript indicates the Hermitian transpose, or the complex conjugate of the ordinary transpose.

When A is not symmetric, the right eigenvectors u_i are not mutually orthogonal. However, the right and left eigensystems have a property called biorthogonality. A right eigenvector u_i and a left eigenvector v_j corresponding to distinct eigenvalues λ_i and λ_j are orthogonal.

Proof [52]

By definition

$$Au_i = \lambda_i u_i \quad ; \quad A^H v_j = \bar{\lambda}_j v_j \quad (A.5)$$

Form the two inner products:

$$v_j Au_i = \lambda_i v_j u_i \quad ; \quad u_i A^H v_j = \bar{\lambda}_j u_i v_j \quad (A.6)$$

The second relation gives

$$v_j Au_i = \bar{\lambda}_j v_j u_i \quad (A.7)$$

Subtracting this from the first inner product gives

$$(\lambda_i - \bar{\lambda}_j) v_j u_i = 0 \quad (A.8)$$

If $\lambda_i \neq \bar{\lambda}_j$, then v_j and u_i are orthogonal.

We can now show that the inverse of the matrix U is a matrix of left eigenvectors of A :

$$(U^{-1})^H A = \Lambda (U^{-1})^H \quad (A.9)$$

Proof [52]

Define V such that $V^H = P^{-1}$. By definition of U

$$AU = UA \quad (A.10)$$

Since $V^H U = U V^H = I$, we have

$$V^H A U = \Lambda \quad (A.11)$$

$$V^H A = \Lambda V^H \quad (A.12)$$

Equation (A.12) is the same as Eq. (A.3).

Now we can consider eigenvalue and eigenvector derivatives. Differentiating Eq. (A.2) by some parameter θ gives

$$A_\theta U + A U_\theta = U_\theta \Lambda + U \Lambda_\theta \quad (A.13)$$

Multiply through by $U^{-1} = V^H$

$$V^H A_\theta U + \Lambda V^H U_\theta = V^H U_\theta \Lambda + \Lambda_\theta \quad (A.14)$$

The i, j elements of Eq. (A.14) can be written as

$$[V^H A_\theta U]_{ij} + [V^H U_\theta]_{ij} \lambda_i = [V^H U_\theta]_{ij} \lambda_i + [\Lambda_\theta]_{ij} \quad (A.15)$$

For $i=j$ we have

$$[V^H A_\theta U]_{ii} = \frac{\partial}{\partial \theta} \lambda_i \quad (A.16)$$

or

$$[U^{-1} A_\theta U]_{ii} = \frac{\partial}{\partial \theta} \lambda_i \quad (A.17)$$

A.1.1 Computation Using Real Arithmetic

If the matrix A is not symmetric, then its eigenvalues and eigenvectors will be complex. During numerical computations, the use of complex arithmetic should be avoided; it is time-consuming and installation dependent. Complex arithmetic can

be avoided by using a block diagonalizing transformation U_b rather than the diagonalizing transformation \bar{U} [54]. The complex block diagonal matrix

$$\mathcal{K} = \text{diag} \left\{ \frac{1}{2} \begin{bmatrix} 1 & -j \\ 1 & j \end{bmatrix}, \dots, \frac{1}{2} \begin{bmatrix} 1 & -j \\ 1 & j \end{bmatrix} \right\} \quad (\text{A.18})$$

transforms A to a block diagonal real matrix

$$\begin{aligned} B &= \mathcal{K}^{-1} A \mathcal{K} = \mathcal{K}^{-1} U^{-1} A U \mathcal{K} \\ &= \text{diag} \left\{ \begin{bmatrix} \sigma_1 & \omega_1 \\ -\omega_1 & \sigma_1 \end{bmatrix}, \dots, \begin{bmatrix} \sigma_n & \omega_n \\ -\omega_n & \sigma_n \end{bmatrix} \right\} \end{aligned} \quad (\text{A.19})$$

The matrix $U \mathcal{K}$ is also real. If U is given as

$$U = [(p_1 + q_1 j) : (p_1 - q_1 j) : \dots : (p_n + q_n j) : (p_n - q_n j)] \quad (\text{A.20})$$

then $U_b = U$ is

$$U_b = [p_1 : q_1 : \dots : p_n : q_n] \quad (\text{A.21})$$

The eigenvalues are then given in terms of U_b as

$$[\mathcal{K} \mathcal{K}^{-1} U^{-1} A_\theta U \mathcal{K} \mathcal{K}^{-1}]_{ii} = \frac{\partial}{\partial \theta} \lambda_i \quad (\text{A.22})$$

$$[\mathcal{K} U_b^{-1} A_\theta U_b \mathcal{K}^{-1}]_{ii} = \frac{\partial}{\partial \theta} \lambda_i \quad (\text{A.23})$$

If the complex matrix \mathcal{K} is represented as

$$\mathcal{K} = \mathcal{K}_r + \mathcal{K}_{ij} \quad (\text{A.24})$$

and \mathcal{K}^{-1} is represented as

$$\mathcal{K}^{-1} = (\mathcal{K}^{-1})_r + j(\mathcal{K}^{-1})_i \quad (\text{A.25})$$

then the real and imaginary parts of the eigenvalue derivatives can be evaluated using real arithmetic as

$$\begin{aligned} \frac{\partial}{\partial \theta} \lambda_i &= [(\mathcal{K})_r U_b^{-1} A_\theta U_b (\mathcal{K}^{-1})_r]_{ii} \\ &\quad - [(\mathcal{K})_i U_b^{-1} A_\theta U_b (\mathcal{K}^{-1})_i]_{ii} \\ &\quad + j [(\mathcal{K})_i U_b^{-1} A_\theta U_b (\mathcal{K}^{-1})_r + (\mathcal{K})_r U_b^{-1} A_\theta U_b (\mathcal{K}^{-1})_i]_{ii} \end{aligned} \quad (\text{A.26})$$

A.1.2 Differentiation of the Euler-Lagrange Equation Matrix

An analytic formula for the derivative of the Euler-Lagrange equation matrix with respect to elements of its constituent matrix is quite complex due to the presence of several matrix triple products such as $H^T A H$ and $GB^{-1}G^T$. For this reason, the derivative of the Euler-Lagrange matrix is formed by a difference approximation to the derivative. The centered difference approximation to the first derivative is used.

$$f'(x) \approx \frac{f(x+h) - f(x-h)}{2h}$$

The resulting approximation is exact when used to evaluate the derivative of the Euler-Lagrange matrix with respect to any of

its constituent matrices. The one exception is elements of the B matrix.

A.2 LQR SENSITIVITY MINIMIZATION [56]

A.2.1 Problem Statement

Consider the system

$$\begin{aligned}\dot{x} &= Fx + Gu + \Gamma w \\ y &= Hx + v\end{aligned}\tag{A.27}$$

where the matrices F , G , Γ , and H contain parameters the values of which are uncertain. If these parameters are considered as Gaussian random variables, a Gaussian random vector may be formed of which they are the components. This vector is specified

$$E(z) = z_n\tag{A.28}$$

where the components of z_n are the nominal values of the parameters, and by

$$E[(z - z_n)(z - z_n)^T]\tag{A.29}$$

is a covariance matrix which is assumed known. Equation (A.27) may then be written as

$$\dot{x} = F(z)x + G(z)u + \Gamma(z)w\tag{A.30}$$

$$y = H(z)x + v\ ,$$

$$x(0) = 0.$$

The control is defined as

$$u = -Cx \quad (A.31)$$

where the values of C may be left free or defined by functional relationships to other parameters of the system. For this definition of u to be valid, Eq. (A.27) generally is required to describe an augmented system that includes the plant and the compensations. The matrices F , G , H , and Γ then have to be defined accordingly. A quadratic PI for this system is

$$J = \lim_{t_f \rightarrow \infty} \frac{1}{t_f} \int_0^{t_f} E(x^T A x + u^T B u) dt \quad (A.32)$$

In this expression, the expected value is taken over the probability distributions of x and u that are derived from both the distributions of the random process w and of the random vector z . Note that w is the process noise of the augmented system. Since w and z are independent, the expected value of a function of x and u is

$$\begin{aligned} E[f(x, u)] &= \int_{x, u} f[x(w, z), u(w, z)] p[x(w, z), u(w, z)] dx du \\ &= \int_w E_z p(w) dw \cdot \int_z E_w p(z) dz, \end{aligned} \quad (A.33)$$

where

$$E_z = \int_z g(w, z) p(z) dz$$

is the expected value over the distribution of z and

$$E_w = \int_w g(w, z) p(w) dw$$

is the expected value over the distribution of w .

A free parameter vector θ is defined by the designer. This vector consists of q parameters of the system matrices that can be varied by the designer.

The problem is now stated as follows. Given the system of Eqs. (A.30) and (A.31) in which the system matrices are functions of a variable parameter vector defined by Eqs. (A.28) and (A.29) determine the value of the free parameter vector θ so that the PI of Eq. (A.32) is minimized.

A.2.2 Derivation of Equations [56]

The cost index Eq. (A.32) may be transformed to the form

$$\begin{aligned} J &= \text{tr} (A + C^T B C) \lim_{t_f \rightarrow \infty} \frac{1}{t_f} \int_0^{t_f} [X_n(t) + \delta X(t)] dt \\ &= \text{tr} [(A + C^T B C) (\bar{X}_n + \overline{\delta X})] \end{aligned} \quad (\text{A.34})$$

where \bar{X}_n and $\overline{\delta X}$ are the time averages over all time of X_n and δX , respectively, and X_n is the nominal state covariance matrix and δX is the addition covariance due to parameter uncertainties.

For a stable system, X_n and δX tend to constant values $X_n(\infty)$ and $\delta X(\infty)$. Since the averaging in Eq. (A.34) is per-

formed over a large time interval, it can be assumed that $\bar{X}_n \rightarrow X_n(\infty)$ and $\bar{\delta X} \rightarrow \delta X(\infty)$. The PI therefore becomes

$$\begin{aligned} J &= \text{tr} [A + C^T BC] [X_n(\infty) + \delta X(\infty)] \\ &= J_O + J_A, \end{aligned} \tag{A.35}$$

where

$$J_O = \text{tr} [(A + C^T BC) X_n(\infty)]$$

is the nominal PI, and

$$J_A = \text{tr} [(A + C^T BC) \delta X(\infty)]$$

is the additional PI due to the parameter variations. The PI of Eq. (A.35) can be minimized computationally by a two-step sequence: (a) the matrices $X_n(\infty)$ and $\delta X(\infty)$ are found for a given value of the free parameter vector, θ ; the PI that corresponds to this value is then determined; and (b) the θ vector is modified in a direction that decreases J . This sequence is repeated until the decrease in J in one cycle is less than a predetermined value.

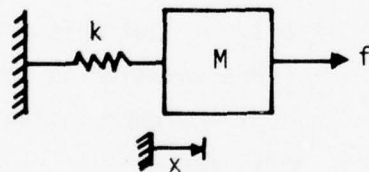
The two parts of this sequence are independent and computer programs for each one can be developed separately.

APPENDIX B

INTEGRAL CONTROL WITH FEEDFORWARDS - AN EXAMPLE

B.1 STEADY-STATE SCHEDULING

The philosophy of steady-state or reference point design can be illustrated with a simple linear example. Many problems with reference point selection in nonlinear, real systems are caused by the nonhomogeneity of the governing equations, rather than the nonlinearity, so a nonhomogeneous linear equation will show the important effects in an analytically tractable form. Consider Figure B.1:



$$\begin{aligned} m\ddot{x} &= f - kx \\ y &= x \end{aligned}$$

$$\text{Let } m = k = 1$$

$$\ddot{x} + x = 2u$$

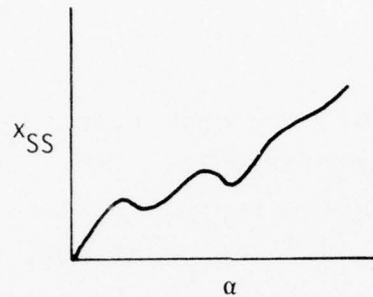
$$\begin{aligned} f &= gu \\ g &= 2 \end{aligned}$$

Equilibria: $\underline{x_{SS}} = 2u_{SS}$ (independent of any control law)

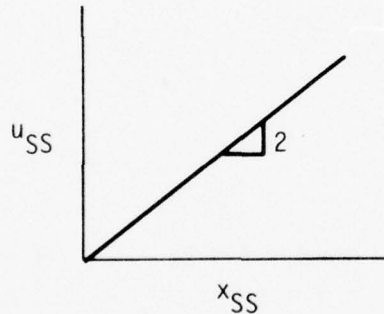
Figure B.1 Example System

Steady-State Schedules

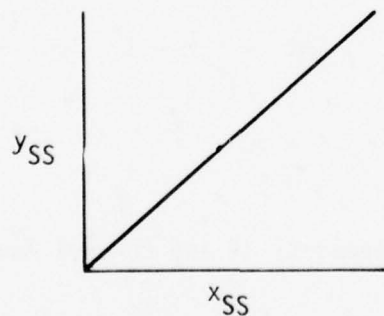
There is a schedule to indicate how the output is to be programmed as a function of input quantities from the operator or the environment; this is shown in Figure B.2:



α is an input specified by "pilot" or environment. By definition, there is some desired output from the system as a function of α .



These three graphs show schematically the desired reference point of the system.



Each of the states and controls is really a function of only α but this graphical representation is more convenient and computationally more efficient.

Figure B.2 Convenient Reference Schedules

An alternative is to represent each of the states and controls as a function of α explicitly, for example, in Figure B.3:

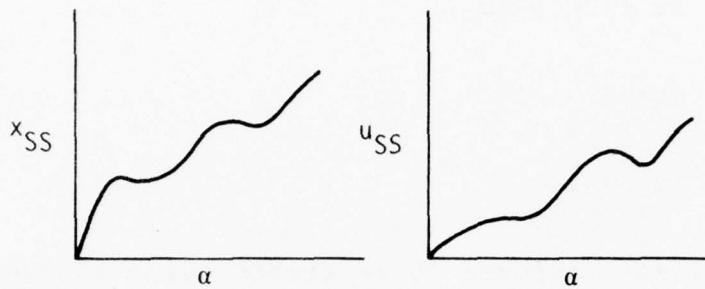


Figure B.3 Alternative Schedules

But this would be much less computationally efficient. In complex systems, convenient, efficient and accurate reference point determination is a major design goal which can be achieved only through a physically meaningful approach and accurate system data.

Returning to the example, a control system can be designed so that the output reaches a desired set point in a well behaved way. Consider the classical design using position and rate feedback (both assumed measured):

$$u = u_d + C_x(x - x_d) + C_v(v - v_d) \quad (B.1)$$

Let

$$C_x = -\frac{1}{2}; C_v = -1 \quad ; \quad v = \dot{x} \quad ; \quad v_d \equiv 0 \quad (B.2)$$

Substituting into system equation:

$$\ddot{x} + 2\dot{x} + 2x - (x_d) = 2(u_d) \quad (B.3)$$

If the reference point is an equilibrium,

$$x_d = 2u_d \quad (B.4)$$

$$\ddot{x} + 2\dot{x} + 2x = 4u_d \quad (B.5)$$

and in steady-state,

$$x = 2u_d = x_d \quad (B.6)$$

The transient response to reference point changes and disturbances is well behaved in a classical sense ($\zeta = 0.707$). The behavior would be different if the actuator effectiveness, g , was specified incorrectly; the equations in terms of g explicitly are:

$$x + gx + (1 + \frac{g}{2})x - \frac{g}{2}x_d = g u_d \quad (B.7)$$

Let $g = 2 + \epsilon$

$$\ddot{x} + (2+\epsilon)\dot{x} + (2 + \frac{\epsilon}{2})x - (1 + \frac{\epsilon}{2})x_d = (2+\epsilon)u_d \quad (B.8)$$

The schedule was based on the incorrect g so that

$$x_d = 2 u_d \quad (B.9)$$

$$\ddot{x} + (2+\epsilon)\dot{x} + (2 + \frac{\epsilon}{2})x = 2(2+\epsilon)u_d$$

and at equilibrium:

$$x_{SS} = \frac{4(2+\epsilon)}{4+\epsilon} u_d \quad (B.10)$$

and the steady-state "hang-off" is

$$\Delta x = x_{SS} - x_d = \frac{2\varepsilon}{4+\varepsilon} u_d \quad (\text{B.11})$$

$$\Delta u = u_{SS} - u_d = \frac{-\varepsilon}{4+\varepsilon} u_d \quad (\text{B.12})$$

The transient response is also degraded but conservative control design should make this effect unimportant. It is possible that the steady-state offset could cause significant problems for high performance systems requiring accurate tracking.

It can be shown that nonlinearities produce effects analogous to modeling errors so it is not possible to specify a reference point for a physical system without some inaccuracy. However, since physical laws can be applied to reference point schedules, a good design technique can reduce the error associated with the approximation.

B.2 INTEGRAL CONTROL FOR REFERENCE POINT TRIM AND LIMITS

Suppose the control law in the previous example is modified. Let

$$u = u_d - \frac{1}{2} (x - x_d) - v - C_I b \quad (\text{B.13})$$

$$\dot{b} = x - x_d \quad (\text{B.14})$$

Differentiating u and replacing in the system equation yields

$$\ddot{x}' + 2\ddot{x} + 2\dot{x} + 2C_I(x - x_d) = 0 \quad (\text{B.15})$$

At equilibrium,

$$x = x_d \quad (B.16)$$

regardless of parameter variations and

$$u_{SS} = \frac{1}{g} x_d \quad (B.17)$$

$$\Delta u = \left(\frac{1}{g} - \frac{1}{2} \right) x_d \quad (B.18)$$

If C_I is chosen so that the system is stable and the variation in g is not so large as to cause instability, then the state, x , will achieve its desired value independent of any system parameters. However, there still will be a hang-off in u .

Many problems arise with this implementation. Most are due to the fact that transient behavior is degraded by the addition of a slow closed-loop root. Feedforward of the reference point is used in practical systems to achieve reasonable transient performance. Also, by raising the order by one, the parameter sensitivity has been increased. The stability region for variations in g and C_I is shown in Figure B.4.

The control law specified in Eq. (B.13) includes a control reference feedforward. However, it was shown that x achieves its desired value without any knowledge of the equilibrium u . Why should this feedforward be included? Consider the Laplace transform of the system with integral control:

$$\left(s^2 + gs + 1 + \frac{g}{2} + \frac{gC_I}{s} \right) x(s) = \frac{gC_I}{s} + \frac{g}{2} x_d + gu_d \quad (B.19)$$

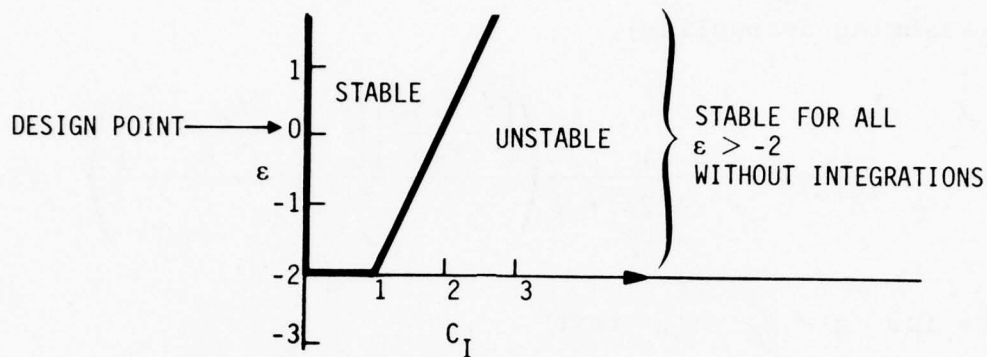


Figure B.4 Stability Limits of Integral System

or for $g = 2$,

$$(s^3 + 2s^2 + 2s + 2C_I) x(s) = (s + 2C_I)x_d + 2su_d \quad (\text{B.20})$$

With no feedforward,

$$u_d \equiv 0$$

and (B.21)

$$\frac{x(s)}{x_d(s)} = \frac{s + 2C_I}{(s^3 + 2s^2 + 2s + 2C_I)}$$

For a reasonably decoupled integral root (say 10x slower)

$$\frac{x(s)}{x_d(s)} \approx \frac{1}{s^2 + 2s + 2} \left(\frac{s + 2C_I}{s + C_I} \right) \quad (\text{B.22})$$

Now, let the feedforward be modeled from the assumed equilibrium condition as follows:

$$u_d = \frac{x_d}{g_m} \quad (\text{B.23})$$

and (assuming decoupling),

$$\frac{x(s)}{x_d(s)} = \frac{1}{s^2 + 2s + 2} \left(\frac{\left[\frac{2 + g_m}{g_m} \right] \left[s + \frac{2g_m}{2 + g_m} C_I \right]}{s + C_I} \right) \quad (\text{B.24})$$

Notice for $g = g_m = 2$, that

$$\frac{x(s)}{x_d(s)} = \frac{2}{s^2 + 2s + 2} \quad (\text{B.25})$$

and the transient response is independent of the integral control for any input. This is a desirable property. It will not be possible to achieve this in general because of modeling inaccuracies and plant nonlinearities. However, it is intuitively clear that the more accurately that g_m approximates g , the more the system behaves like the transient regulator design without the additional integration.

The step response for various values of integral feedback gain is compared to that of the system with control reference feedforwards in Figure B.5.

The moral of the story is that integral control provides a method for compensating small reference point specification errors and plant nonlinearity, but cannot replace carefully devised reference point specification algorithms because of degraded transient behavior.

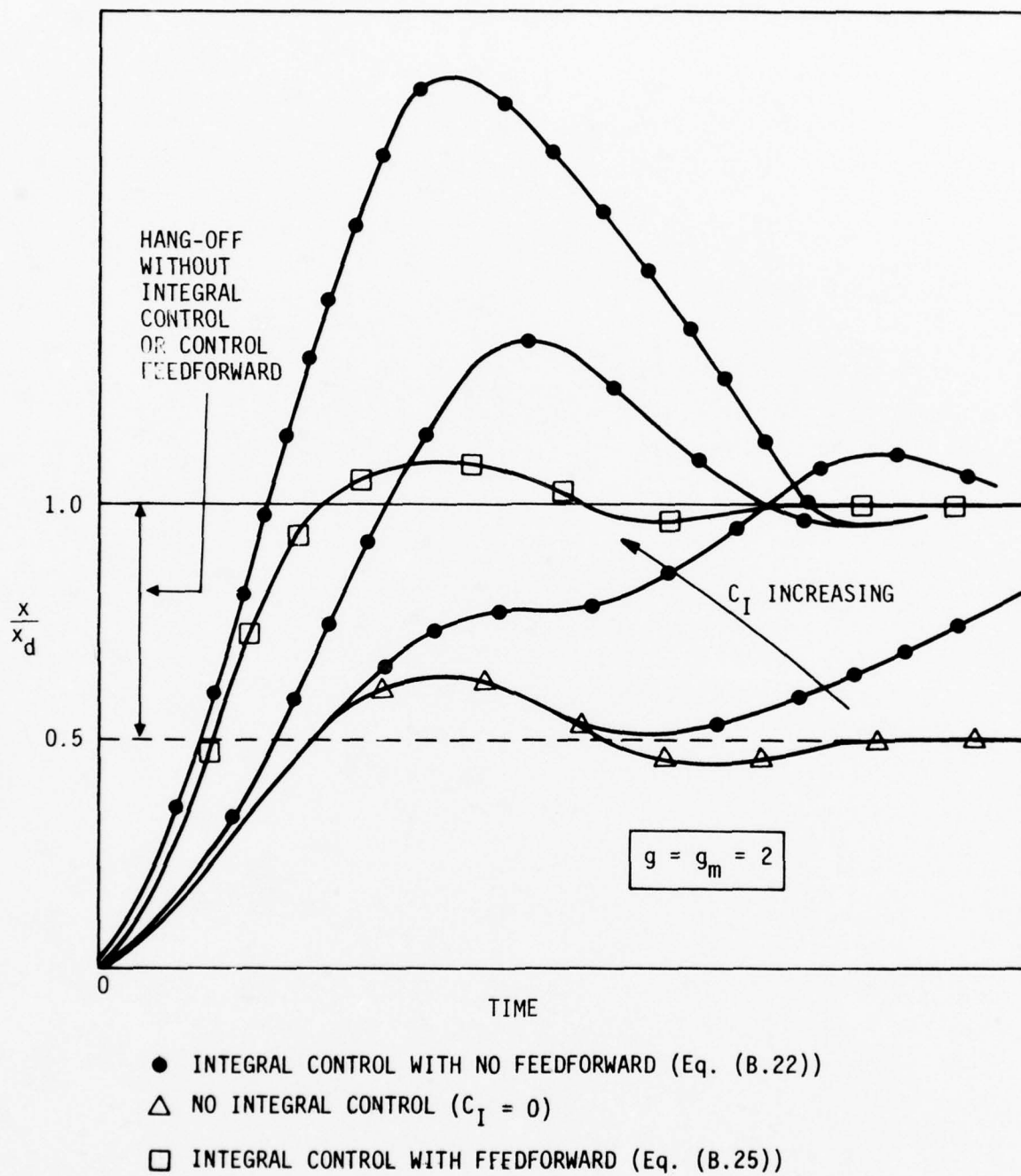


Figure B.5 Comparison of Step Response of Systems With and Without Control Reference Feedforwards

APPENDIX C STEADY-STATE REFERENCE SCHEDULES

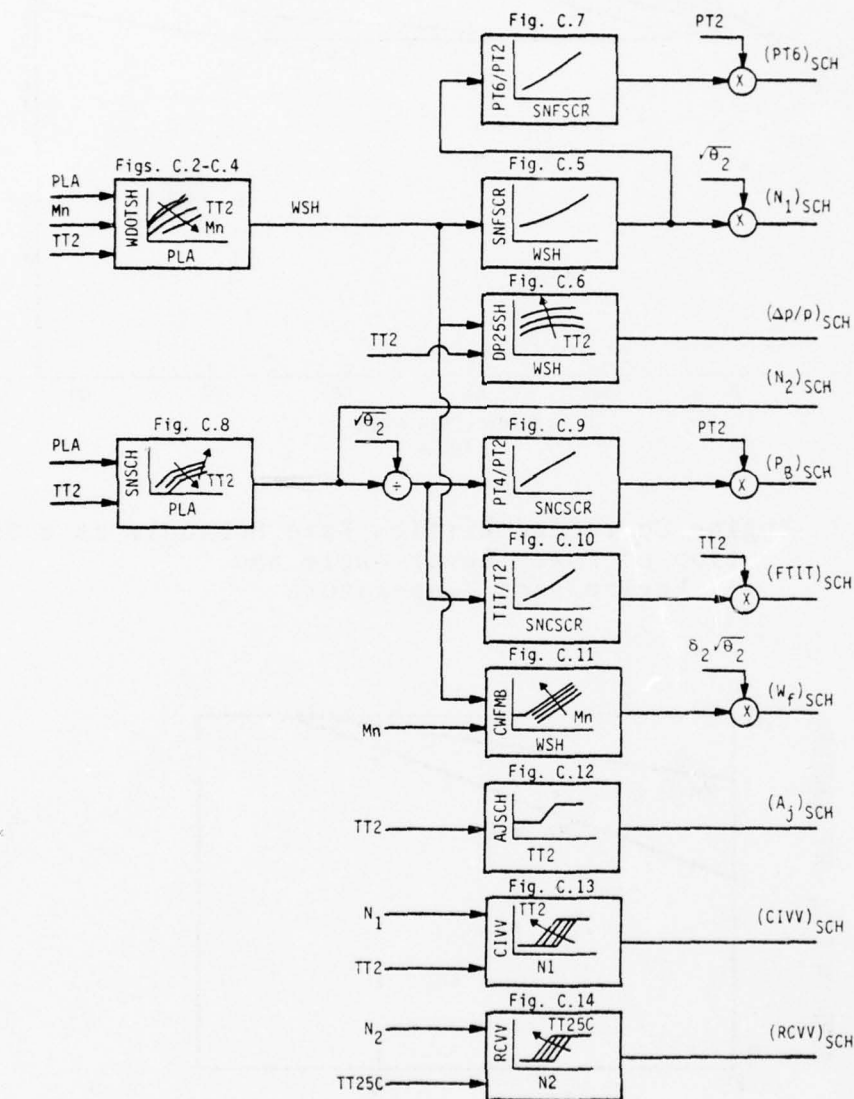


Figure C.1 Reference Schedule Algorithm Figure Index

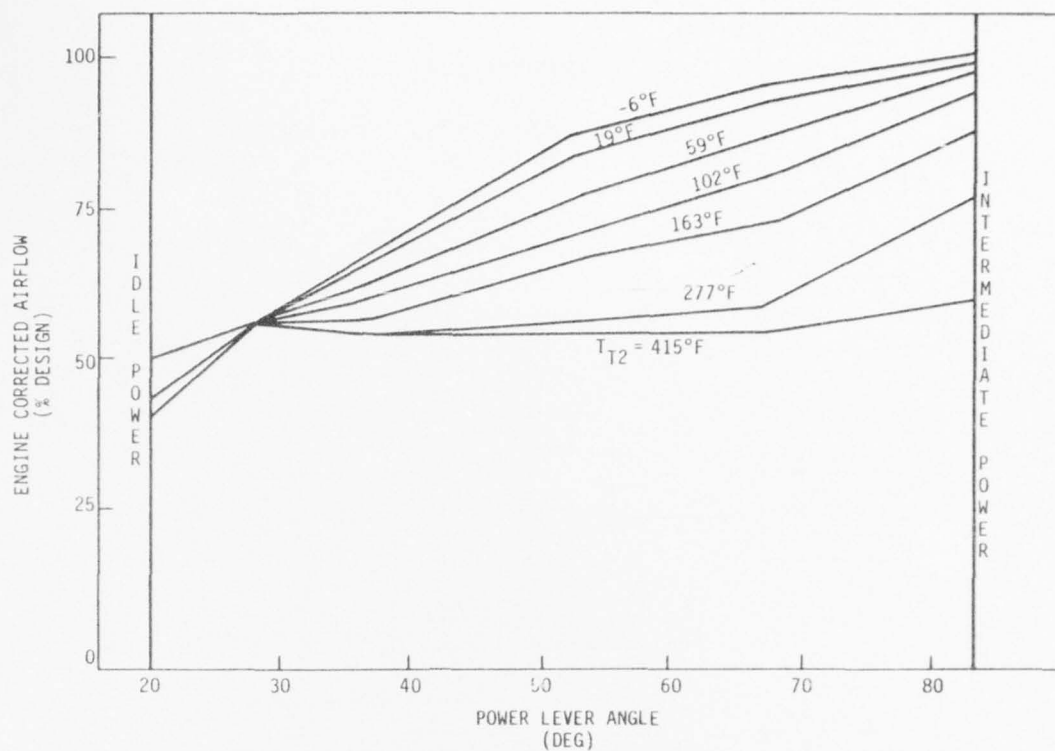


Figure C.2 Engine Corrected Airflow Base Schedule as a Function of Power Lever Angle and Engine Face Temperature

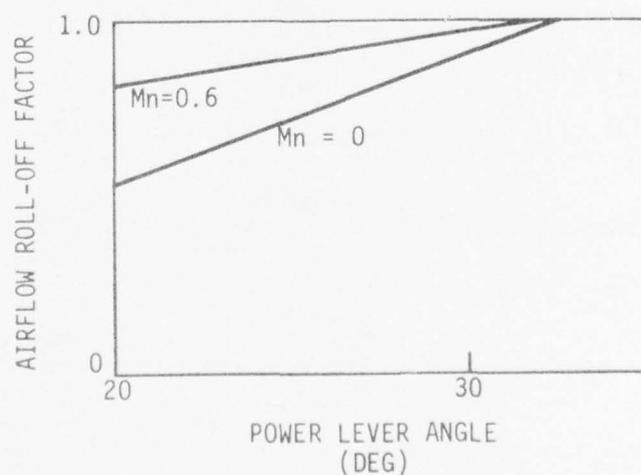


Figure C.3 Airflow Roll-off Factor Schedule for Low Speed, Low Power Modification of Scheduled Engine Airflow

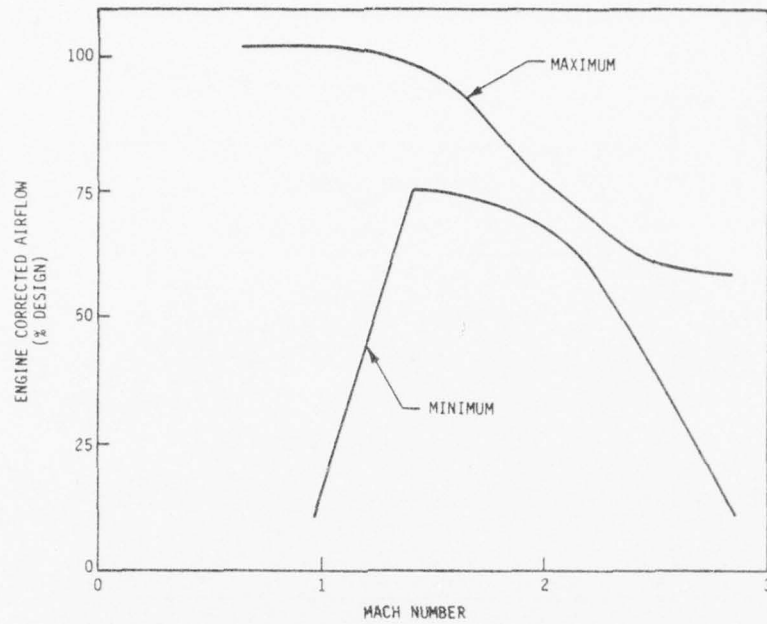


Figure C.4 Airflow Corridor Required for Inlet Compatibility at All Power Conditions

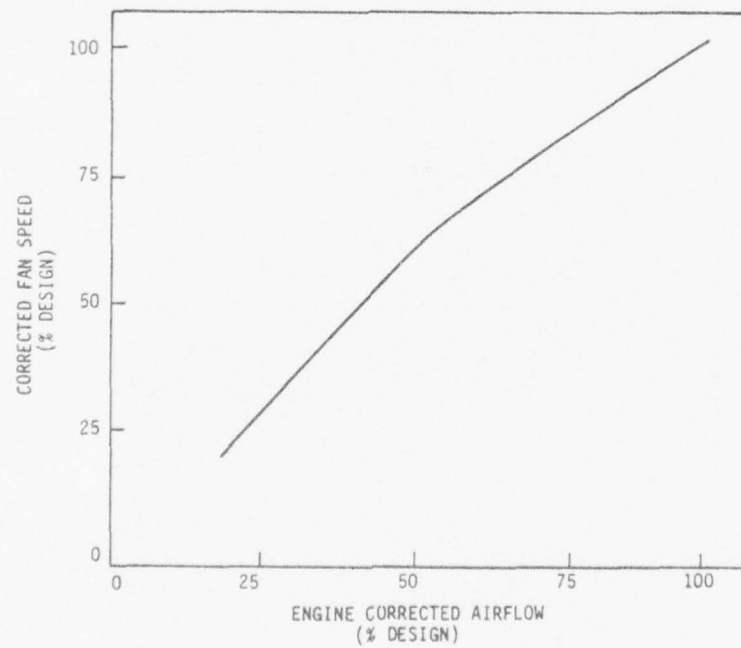


Figure C.5 Fan Speed Schedule as a Function of Scheduled Engine Airflow

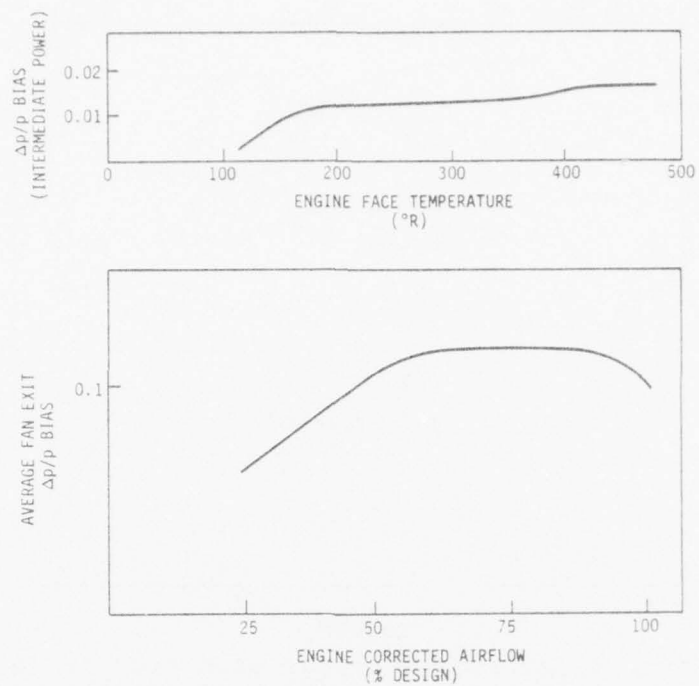


Figure C.6 Fan Match Point Schedule Consisting of a Base Schedule as a Function of Engine Airflow and an Additive Bias Shift for Supersonic Operation

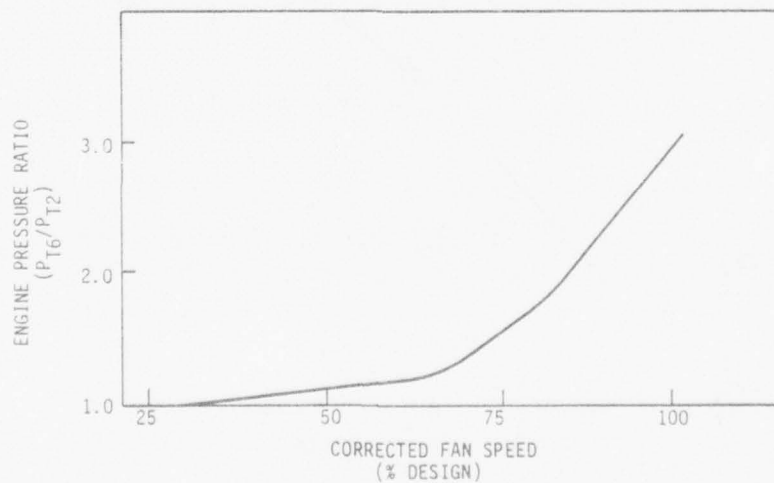


Figure C.7 Engine Pressure Ratio Schedule as a Function of Scheduled Fan Speed

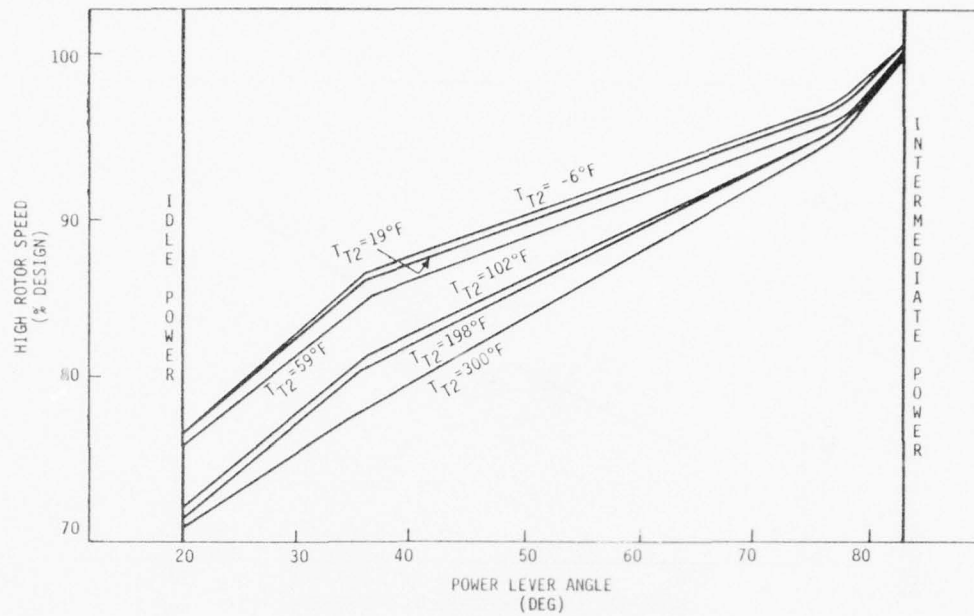


Figure C.8 Scheduled High Rotor Speed as a Function of Power Lever and Engine Face Total Temperature

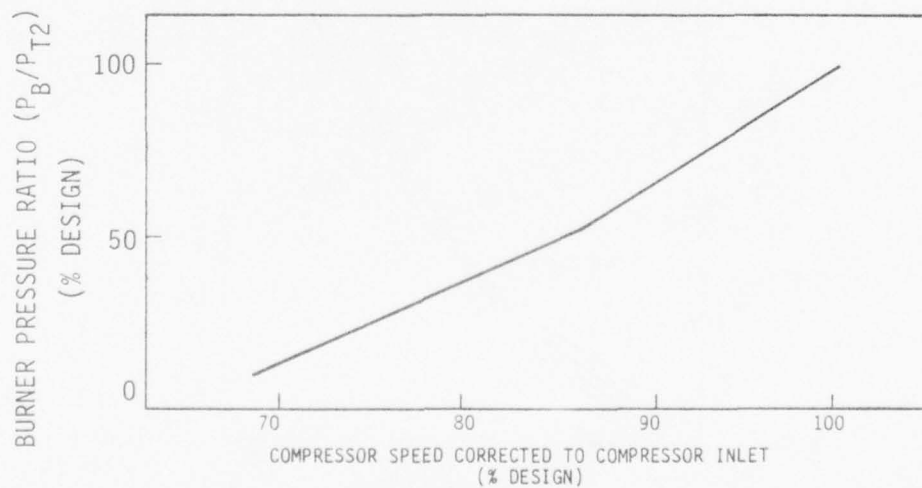


Figure C.9 Burner Pressure Ratio Schedule as a Function of Scheduled, Corrected Compressor Speed

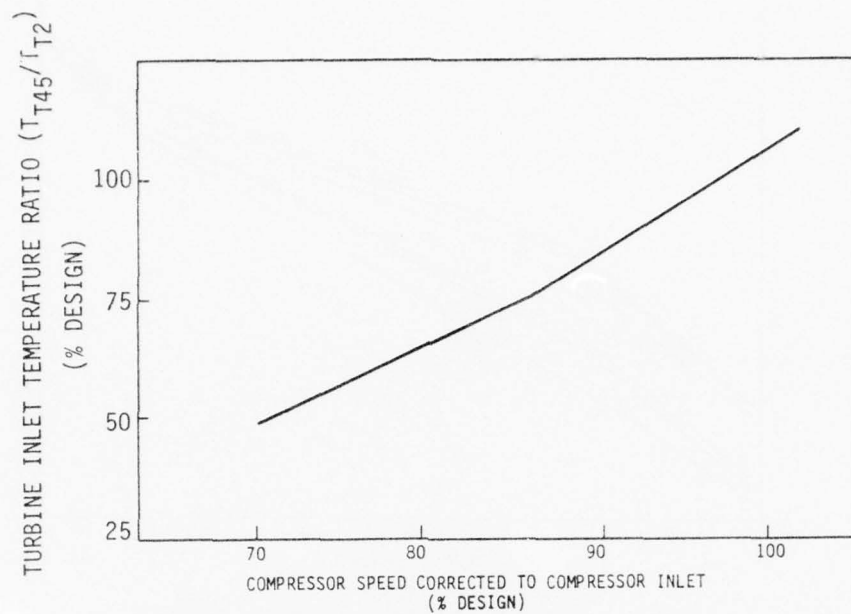


Figure C.10 Scheduled Turbine Inlet Temperature Ratio as a Function of Scheduled, Corrected Compressor Speed

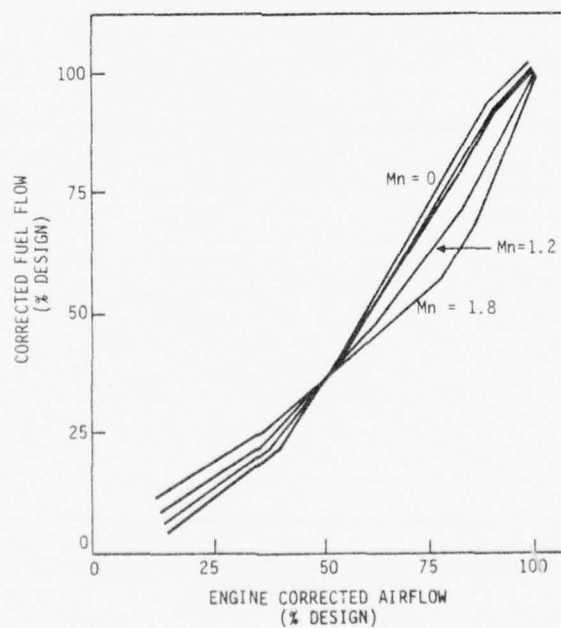


Figure C.11 Scheduled Fuel Flow as a Function of Scheduled, Corrected Airflow and Mach Number

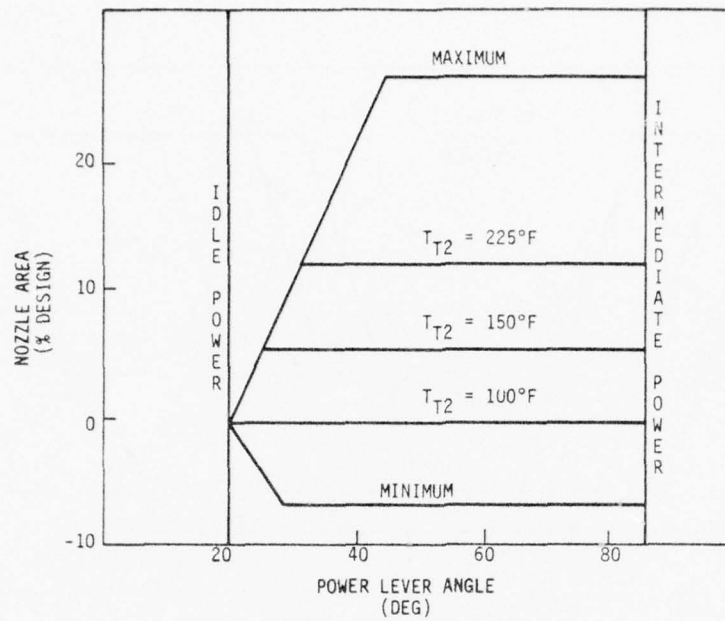


Figure C.12 Nozzle Area Scheduled as a Function of Power Lever Angle and Engine Face Total Temperature

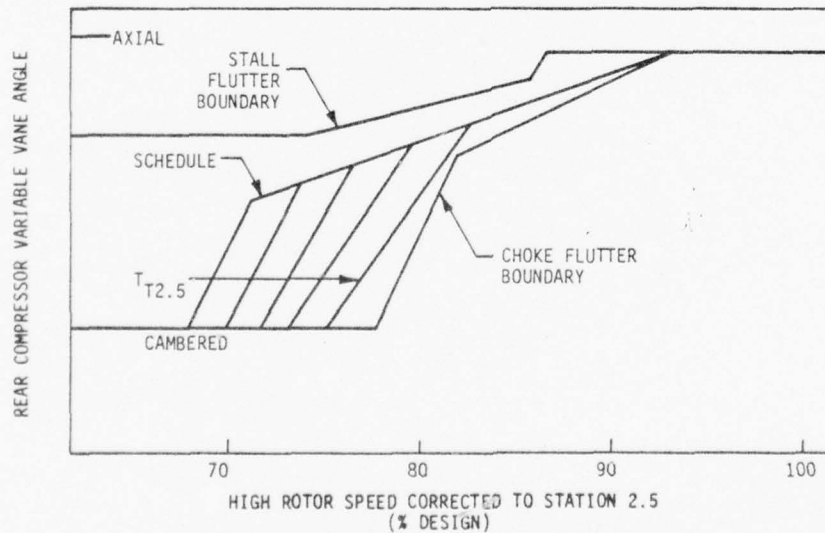


Figure C.13 Rear Compressor Variable Vane Angle Schedule as a Function of Corrected Compressor Speed and Flutter Boundary Curves

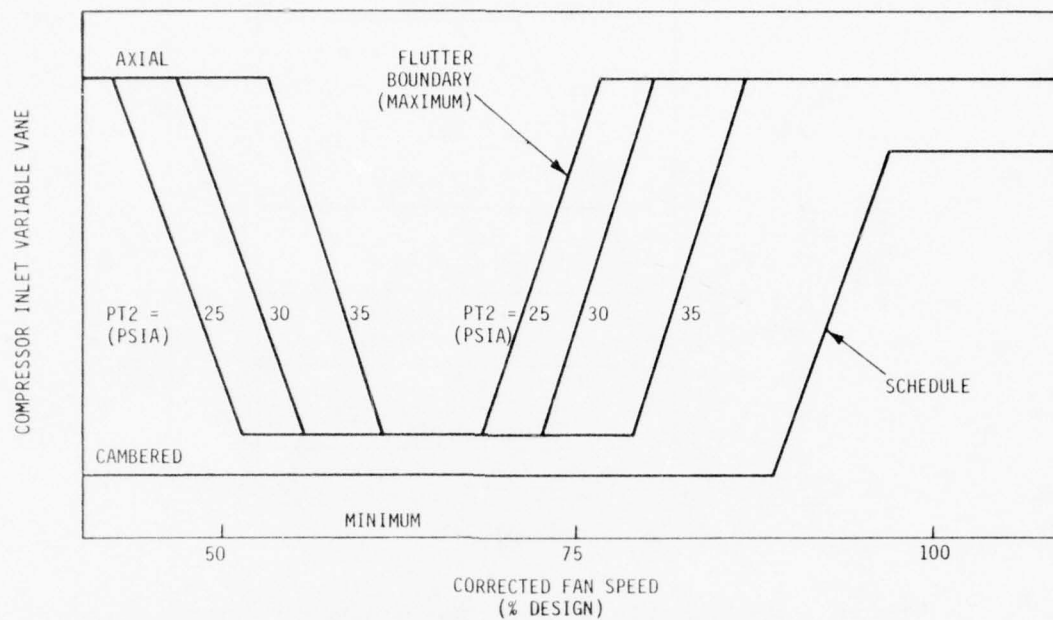


Figure C.14 Compressor Inlet Variable Vane Schedule as a Function of Corrected Fan Speed with Flutter Boundary on Maximum Deflection as a Function of Engine Face Total Pressure

APPENDIX D

LINEAR MODELS

D.1 DETAILED LINEAR MODEL ANALYSIS

Linear models were generated at a group of operating conditions throughout the flight envelope [1]. Operating conditions were specified sequentially in groups. Operating point specification was determined by insight into the behavior resulting from the dynamic analysis of the previous groups of models. The 42 operating points chosen are shown in Table D.1. The analysis of the dynamic behavior coupled with the detailed steady-state analysis contained in Chapter V produced the choice of design and evaluation points for regulator synthesis. The details of the linear model analysis of the matrices, generated by Pratt & Whitney Aircraft and included in their report [1], are presented below.

Sea Level Static Intermediate Power Models

Linear models were generated at a series of operating points at sea level static conditions. For intermediate power, the root locations of the model are shown in Table D.2. It is possible to associate a state variable with each root by inspection of the eigenvectors of the system. A correspondence can then be found to the models of pressure, temperature and flow time constants included in the nonlinear simulation. In this way, the structure of the response can be determined in terms of predominant response variables.

The modeled state response to initial conditions for five of the engine variables has been calculated to illustrate the correspondence of eigenvector components and modal responses in the linear system. In Figure D.1, the time history of the

Table D.1
Operating Points Chosen for Dynamic/Static Analysis

CODE	POINT NO.	MACH NO.	ALTITUDE FT. (000)	PLA (DEG)	COMMENTS
Basic Set	1	0	0.0	20	} Sea Level Static Operating Line
	2	0	0.0	36	
	3	0	0.0	52	
	4	0	0.0	67	
	5	0	0.0	83	
Group I	1	0	0.0	24	Additional Unchoked Model
	2	0.9	10.0	83	Performance at Max. TT4
	3	0.3	20.0	24	PB Lower Limit
	4	0.6	10.0	20	Unchoked Model Behavior
	5	0.6	30.0	24	Unchoked Model Behavior
Group II	6	1.2	0.0	83	Maximum q, PB, N1, N2, TT4
	7	2.2	40.0	83	TT3, TT4 Limit, Compressor Stab.
	8	0.9	45.0	130	Low Augmentor Pressure
	9	0.9	65.0	83	Fan Stability
	10	2.5	65.0	130	Maximum Augmentation
Extra (E)	1	0.9	10.0	36	} Additional Operating Line Data for Engine Test
	2	0.9	10.0	52	
	3	0.9	10.0	67	
	4	0.9	10.0	83	
	5	0.9	30.0	36	
	6	0.9	30.0	52	
	7	0.9	30.0	67	
Group III	1	0.0	0.0	20	Minor Deck Modification
	2	0.0	0.0	20	With BLD/HPX Extraction
	3	0.0	0.0	83	Minor Deck Modification
	4	0.9	10.0	20	} Additional Operating Line Data for Engine Test
	5	0.9	30.0	20	
	6	0.9	30.0	83	
Group IV	1	0.9	45.0	83	Rating Point
	2	0.9	45.0	52	Altitude Part Power Point
	3	0.9	45.0	40	Minimum Burner Pressure
	4	1.8	75.0	83	Low Density, Reynolds Index
	5	1.8	20.0	83	Maximum N1, TT3, TT4
	6	0.3	20.0	83	Fan Stability
	7	1.8	40.0	83	TT4 Limit, Compressor Stab.
	8	2.5	65.0	83	Compressor Stability
	9	2.15	58.5	83	PT2, TT2 Coverage

five states is calculated for unit initial conditions in each state. In the first column, fan speed is initially one unit away from the trim speed. As the system returns to equilibrium, it is observed that the augmentor pressure lags the fan speed. The compressor speed is nearly unaffected. The increase in fan discharge pressure is transmitted into the burner because

Table D.2
Eigenvector Association of Dynamic Roots of 16th Order
Linear System

ROOT LOCATION	DOMINANT VARIABLES	COMMENTS
-501	PT45	Pressure/Volume Dynamics
-181	PT3	
-42	TT4PHI	
-56, -47 ± 4.8j	TT45HI	Temperature Dynamics Uncoupled Time Constants of S = -50.0
	TT4	Temperature/Flow Dynamics - Modified from Original Time Constants of S = -50.0
	TT7M	
	TT5	
-16, -22, -20 ± 4.2j	TT6C	Temperature/Flow Dynamics - Modified from Original Time Constants of S = -20.0
	TT3	
	TT2.5C	
-2.0	TT45LO	Uncoupled Subsystem Original Time Constant of S = -2
-0.72	TT4PLO	Uncoupled Subsystem Original Time Constant of S = -0.67
-2.7	SNCOM	Rotor Inertia/Torque Balance of Core Stream
-4.03 ± 3.1j	SNFAN	Pressure/Flow work Balance for Fan Rotor
	PT7M	

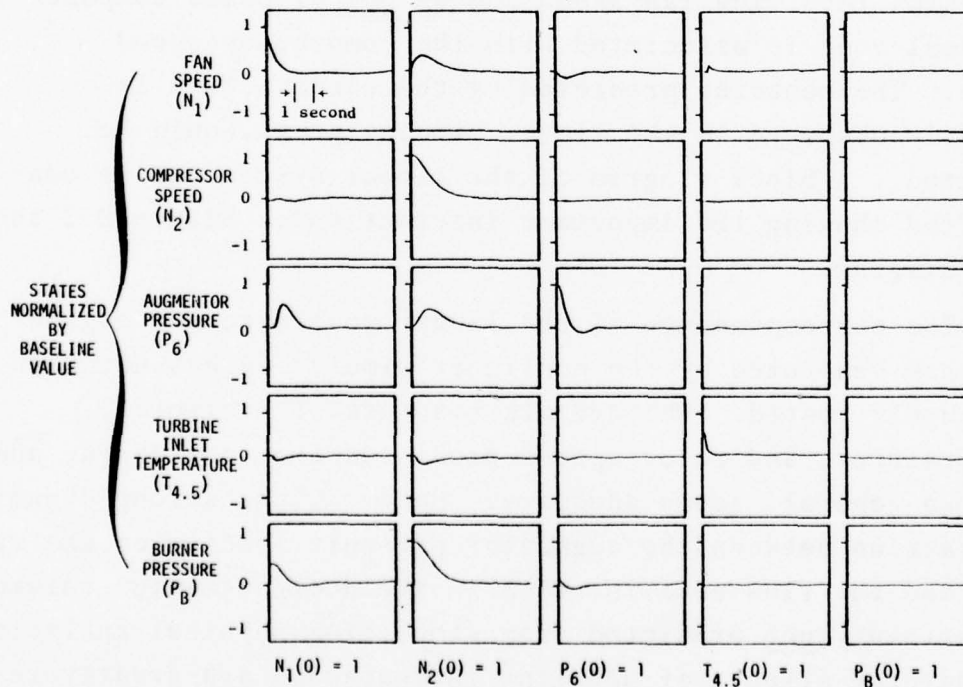


Figure D.1 Indicial Response of Fifth Order Linear Model, Intermediate Power, Sea Level Static

of the nearly constant compressor pressure ratio. As the fan speed moves to equilibrium, the burner pressure follows. For an initial condition in compressor speed, the response is nearly a simple exponential decay. The fan speed and augmentor pressure move in phase in response to the compressor speed. Burner pressure follows the compressor speed decay. For a temperature and burner pressure initial condition, the decay to equilibrium does not excite any motion in the fan, compressor speed and augmentor pressure states.

The dynamic character of the linear system is evident from the eigensystem analysis and the indicial response plots. The eigensystem shows a root with a 7 msec time constant. This root represents the flow equilibration in the burner as illustrated in the 5th column of Figure D.1. Similarly, the gas temperature response of the system at the turbine inlet also has a fast time constant relative to the rotor speed roots. The complex root near $|s| = 5$ rad/sec has response characteristics involving fan speed and an out-of-phase component. The real root is associated with the compressor speed state. The behavior predicted by the eigenvectors is directly observed in the linear simulation as would be expected. A block diagram of the linear system can be constructed showing the important interactions. Figure D.2 shows this diagram.

The correspondence of the linear models to the engine response generated by the nonlinear simulation has not been thoroughly tested. The dynamic response of pressures, temperatures, and rotor speeds predicted from the linear analysis, in general, seems adequate. However, the strong dynamic interaction between the augmentor pressure loading on the fan disc and the flow equilibration in the duct/augmentor volume is certainly not predicted from simplified physical analysis. The adverse effects of modeling inaccuracies are greatly reduced within a closed-loop feedback system such as the linear quadratic regulator. Thus, precise models in closed-loop

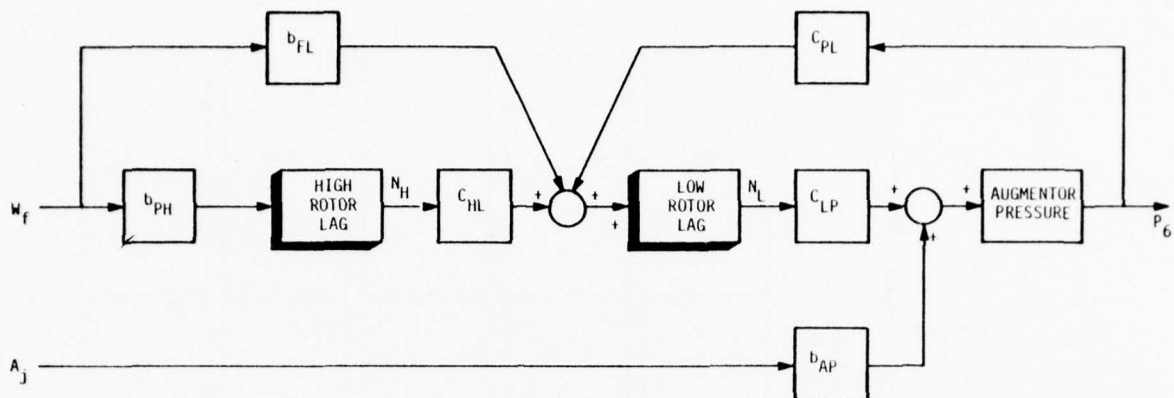


Figure D.2 Linear System Block Diagram

design are not necessary to achieve excellent performance as long as the synthesis procedure is undertaken with a recognition of the approximate nature of the representation. The linear models are used in LQR design in this spirit and with the firm understanding that they are merely a means to an end, namely, a practical controller for a real engine,

The analysis can be used on the output response of the system. Figure D.3 shows the indicial output response (i.e., the response to unit initial conditions in each state). The primary components of the thrust are the fan speed, compressor speed, and augmentor pressure.

Extension of Results to the Sea Level Static Operating Line

The applicability of the linear model to variation in power level is the next issue. In Figure D.4, the frequency response at idle and intermediate power is shown for the fuel flow to low rotor speed transfer function. At intermediate power, the low rotor is driven by the fuel flow through the cascaded high rotor speed lag. As a result, the transfer function is nearly first order with a response showing only the high rotor dynamics.

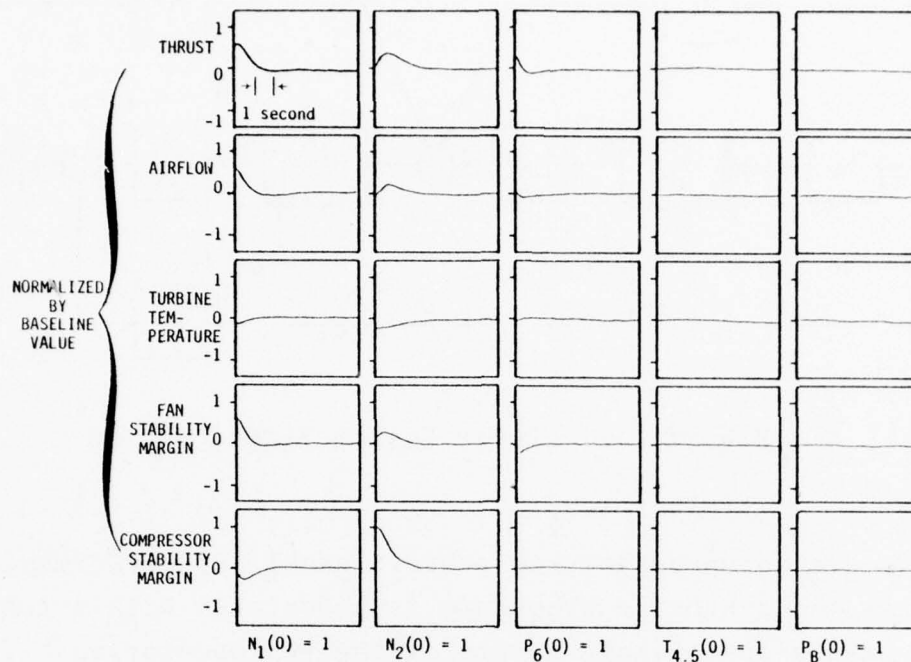


Figure D.3 Output Indicial Response

At idle, the response of low rotor speed to fuel flow shows the effects of the compressor lag. This indicates that a mode of independent low and high rotor motion, suppressed at high power, can be excited at low power. Also, the high rotor root has only one-third the response time at idle.

An intuitive explanation of this behavior is suggested from engine operation. At high power, the fan turbine operates at a constant flow parameter. Changes in high turbine inlet temperature are reflected as excess work at both turbines instantly (or nearly so). Fuel energy is converted to torque for both spools and the response of the system to fuel flow is a characteristic lag of the combined rotor system accelerating (i.e., the two spools act as a single rotor system). Pressure disturbances in the augmentor appear only at the compressor inlet because the choked turbine eliminates any back pressure sensitivity.

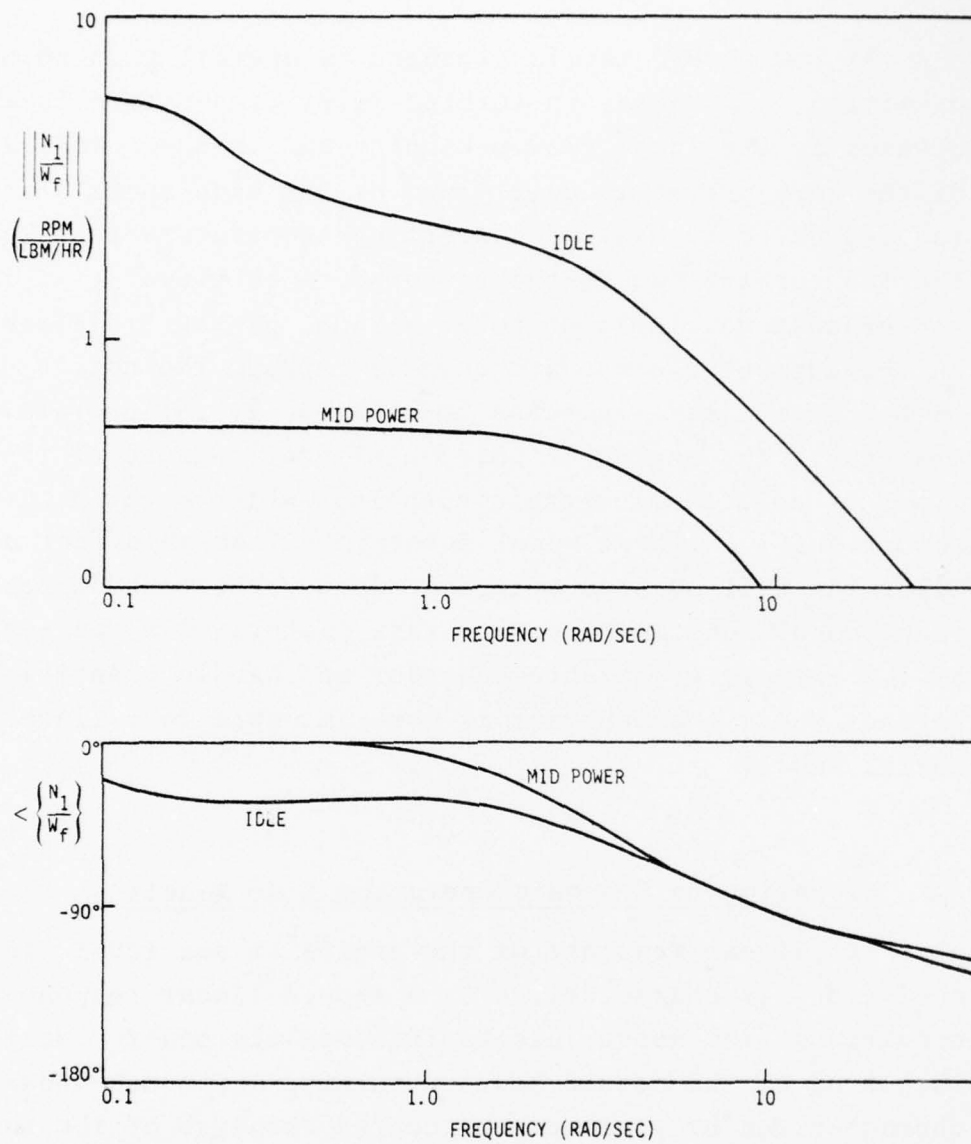


Figure D.4 Frequency Response of Linear Models at Idle and Intermediate Power at Sea Level Static Conditions

At low power, the fan turbine is operating in an unchoked condition. Increases in turbine inlet temperature cause increases in the inlet flow parameter and torque. The response of the core engine is determined by the high spool alone. The reduced effectiveness of converting temperature to torque in the fan turbine causes the response to be slower. At idle, the exhaust nozzle is unchoked. Thus, pressure disturbances in the augmentor dissipate quickly through the nozzle discharge with a significant increase in flow equilibration rate. At low power, the engine is quite nonlinear because of the many types of aero-thermodynamic couplings which occur at low flow conditions. A linear model determined from an offset derivative algorithm will be step size dependent. The control design at these conditions must operate satisfactorily in the presence of the extremely variable behavior and handle transitions to regimes where the behavior is more amenable to a linear differential model.

Extension to Subsonic Operating Line Models

The linear response of the engine at sea level static power conditions is characterized by a simple linear response at conditions from above idle to intermediate power. Near idle, unchoking of the nozzle and low turbine cause nonlinear behavior characterized by a slower, uncoupled response of the two rotor speeds. The modes of operation at various power conditions and altitude points are related to this behavior. The models can be parameterized with an ambient variable when a correspondence is found.

Figure D.5 shows the engine operating envelope. Transient operation is limited to the left by low pressure constraints and minimum airflow requirements. To the right, operation is restricted by maximum pressure, temperature and airflow requirements. This results in a narrow corridor in which transitions

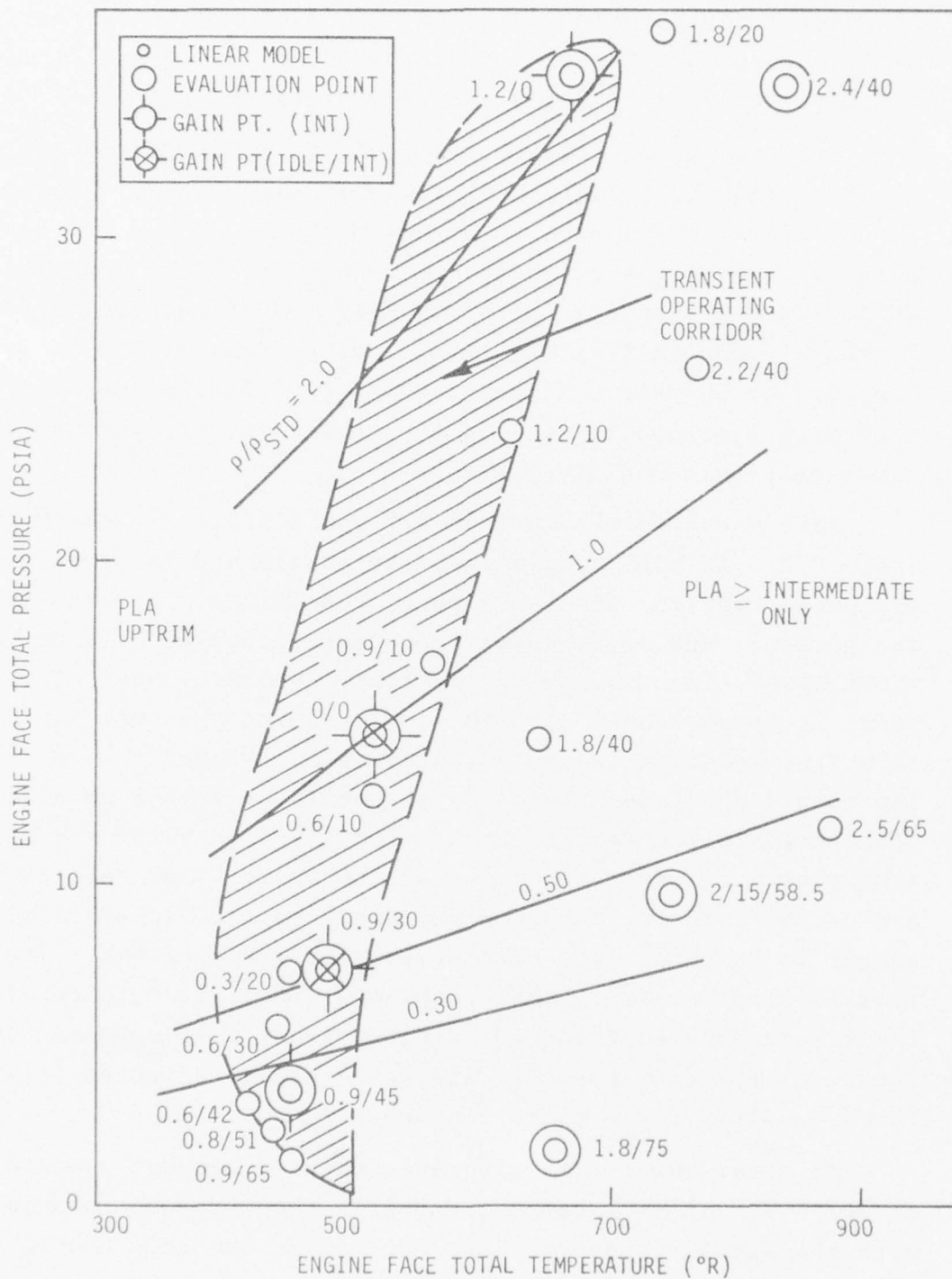


Figure D.5 Linear Model Generation Points

in power condition are permitted. In these regions, the dynamics of the plant must be understood so that practical and minimally complex controls can be implemented.

From sea level static, lower points in the transient corridor correspond to altitude, subsonic conditions. Higher in the corridor corresponds to higher Mach number and low altitude points. Two series of operating line models were generated at subsonic altitude points. At 30K/0.9, the ambient pressure is roughly one-half of sea level static and at 45K/0.9, it is roughly one quarter. Higher than 45,000 ft, the subsonic operating envelope is limited by pressure constraints to include only intermediate power.

Part power models for 45K/0.9 and 30K/0.9 are shown in Table D.3. At both conditions, the nozzle and fan turbine are choked for the series of power conditions. At high power, the pressure and rotor speed roots are uncoupled. Since the rotor speed time constant at a fixed, nondimensional match point is proportional to $8\sqrt{\theta}$ [69] and the pressure equilibration time constant is approximately proportioned to $\sqrt{\theta}$ [70], the coupling between these states should be weaker at higher altitudes and low Mach numbers. For the high rotor speed time constant, these relations are accurate. For the low rotor and pressure roots, the coupling terms in the linear models appear to be important, particularly at low airflows. The root locations reflect this coupling. Thus, at high power, the system has two uncoupled dynamic roots corresponding to the rotor speed response. This behavior is reflected in the 30K/0.9, 45K/0.9 and 65K/0.9 models.

At lower powers, a different behavior becomes apparent at 30K/0.9. In this case, there is a complex root associated with the spool response. The coupling is probably due to the load on the compressor face caused by changes in fan speed and discharge pressure. This effect is not dynamically important at higher pressures or airflows because of the decreased sensitivity of compressor speed to compressor entrance

Table D.3
Eigenvalues of Linear Models at Part Power Conditions at 30,000 Ft and
45,000 Ft, Mach Number = 0.9

83/30K/0.9	67/30K/0.9	52/30K/0.9	36/30K/0.9	20/30K/0.9	83/45K/0.9	52/45K/0.9	40/45K/0.9
-514	-553	-455	-495	-480	-592	-568	-498
-206	-144	-206	-143	-120	-172	-133	-150
-65	-54	-57	-55	-57	-57	-60	-55
-53	-50 + 14j	-52	-50 + 5j	-51	-51	-53	-47
-43	-43 + 1j	-43 + 1j	-44	-44 + 2j	-46	-43 + 2j	-48 + 2j
-36	-43	-44	-44	-44	-45	-45	-45
-22 + .8j	-23	-19 + 7j	-19 + 2j	-21 + .4j	-21 + 3j	-22 + 1j	-18 + 3j
-18 + 8j	-22 + 2j	-22	-22	-20	-22	-17 + 5j	-20
	-18	-20 + .2j	-20	-19	-17	-20	-20
-17	-14	-17	-17	-17	-16	-19	-21
-9.9*	-7.32*	-3.4*	-5.4*	-6.5*	-6.6*	-3.1*	-5.6*
-2.6*	-4.07*	-2.4 + 1j*	-1.9 + .3j*	-1.2 + .5j*	-1.9*	-2.6*	-1.4*
-1.7 + .1j*	-1.29*	-2	-1.7	-2	-0.56*	-2	-2
-0.54	-0.7	-0.7	-0.7	-0.7	-0.7	-0.7 + .1j*	-0.7 + .1j*

* Dominant roots

perturbations. It should be noted that the dynamics of the states are closely coupled at these points. This contrasts with the response of the system at the higher power conditions where the system is more uncoupled.

The conclusions concerning altitude points can be summarized as follows. The high power behavior predominantly corresponds to uncoupled rotor speed dynamics. At low power conditions, moderate altitudes and Mach numbers, the spool responses couple to form a moderately damped complex pair. This behavior is probably produced by the increased sensitivity of the high pressure spool to compressor face disturbances.

Several other subsonic points were investigated. These points were generally low altitude, low Mach number at intermediate and idle power. Figure D.5 shows the low turbine Choking parameter $T_{T4.5}/T_{T2}$ as a function of airflow. The low turbine is observed to run unchoked in a region of the flight envelope at low altitude and Mach number conditions. The eigenvalues of the models generated to investigate this regime are listed in Table D.4. These models demonstrate the response predicted by the unchoked turbine behavior. It can be seen that the character of the roots changes significantly, even at points which are quite close together in the envelope (e.g., 30K/0.9, 30K/0.6 and 20K/0.3). This is indicative of the sensitivity of the linear dynamics to the chosen operating point; or, stated another way, the nonlinearity of the plant in this region.

Extension to Transonic, Low Altitude Points

The behavior of the engine at conditions corresponding to higher inlet pressures and temperatures in the upper half of the transient corridor was investigated with models along the operating line at 10K/0.9 and intermediate power at 0K/1.2. These results are shown in Table D.5.

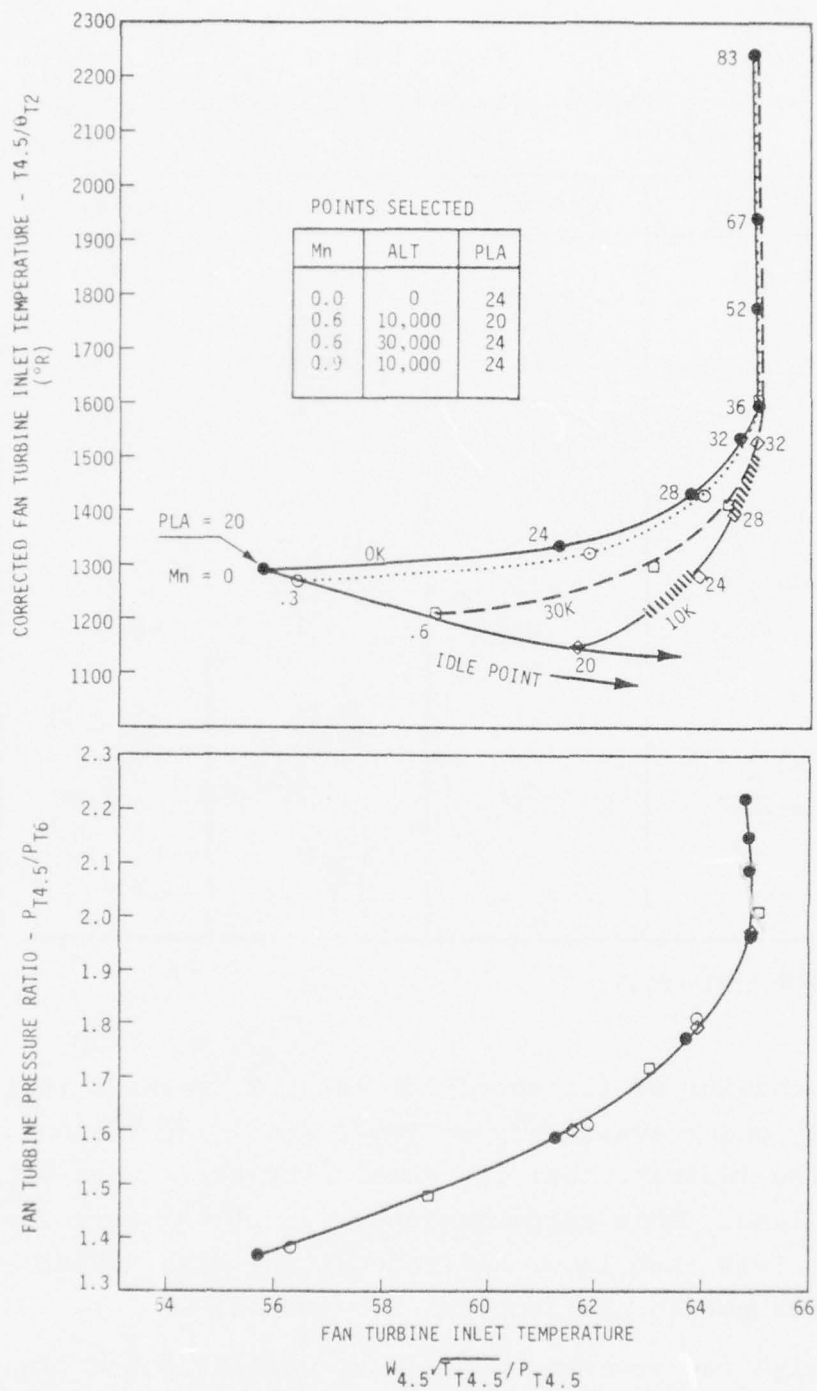


Figure D.5 Fan Inlet Flow Parameter at Low Mach, Low Altitude Flight Points Showing Turbine Choking Characteristics

Table D.4
Eigenvalues of Miscellaneous Subsonic Linear Models

83/20K/0.3	24/20K/0.3	20/10K/0.6	24/30K/0.6
-608	-527	-622	-570
-126	-130	-150	-128
$-50 \pm 20j$	-56	-58	-57
-54	-50	-51	-51
-43	-46	-45	$-46 \pm 1j$
-27	-45	-42	
-21	$-15 \pm 2j$	$-15 \pm 4j$	
$-19 \pm 3j$	-16	$-20 \pm 1j$	-20
-13	-21	-21	$-20 \pm 1j$
	-20		
	-21	-17	$-18 \pm 2j$
$-5 \pm 2j^*$			-5.5
-1.25*	-1.5*	-1.9*	-2.6*
-2	-2	-2	-2
-0.7	$-.7 \pm .2j^*$	$-.7 \pm .2j$	$-.7 \pm .2j^*$

* Dominant roots

The behavior of the models at 10K/0.9 is characteristic of the high power system at sea level static conditions. The results also indicate that the model does not change along the operating line. This condition operates at higher corrected airflow at idle than lower altitude, lower Mach number points and both the nozzle and turbines are choked.

The high ram pressure condition, 0K/1.2, has a limited power level range because of airflow constraints near intermediate power. The response of the engine is similar to the sea level static, intermediate behavior. The response times of the roots are about 30% less than at sea level static.

Table D.5
Eigenvalues of Transonic Operating Points

83/10K/0.9	67/10K/0.9	52/10K/0.9	36/10K/0.9	20/10K/0.9	83/0/1.2
-585	-490	-538	-577	-617	-572
-213	-204	-158	-170	-120	
-67	-56	-58	-62	$-51 \pm 16j$	-61
-53	$-47 \pm 5j$	$-48 \pm 3j$	-52	-52	-46
-45	-41	-42	-44	-43	-35
-32	$-21 \pm 4j$	$-18 \pm 4j$	-38	-20	-23
$-15 \pm 9j$	-23	$-21 \pm .3j$	$-21 \pm .7j$	-26	-19
-22	-20	-19	$-17 \pm 7j$	$-21 \pm .8j$	$-20 \pm 2j$
$-20 \pm 2j$	-17		-20	-12	-14
$-8 \pm 2j^*$	$-3.9 \pm 3j^*$	$-3.8 \pm 4j^*$	$-3 \pm 3j$	$-5.6 \pm 1.7j^*$	$-7 \pm 4j^*$
-3*	-4.4*	-2.9*	-3.4	-1.1*	-5*
-2	-2	-2	-2	-2	-2
-0.7	-0.7	-0.7	-0.7	-0.8	-0.7

* Dominant roots

The conclusions concerning the behavior in this portion of the envelope are summarized below. The eigensystem of the models in this region of the envelope is similar to the sea level static, intermediate power. The response times of the engine decrease as a function of the position in the envelope with the sea level ram point being about 30% faster than the sea level static response.

Extension to Supersonic Conditions

Several supersonic points were chosen to investigate engine dynamic response. These points range from very low to very

high ram pressures and at higher than standard inlet temperatures. Airflow limits constrain the engine to intermediate power (and above). Thus, these points lie to the right of the transient operating corridor. The control requirements at these points are compensation of disturbances due to augmentor lights and inlet distortion.

Three groups of models were chosen. These were low pressure, mid-pressure, and high pressure points in the right side of the envelope. The results from the model analysis for each group is presented below.

The low pressure points consisted of 75K/1.8 and 58.5K/2.15. The model at 75K/1.8 is very similar to that at 65K/0.9 and other subsonic altitude points. The rotor speed responses are coupled. The pressure lag of the augmentor is considerably faster. Control of pressure pulses at this condition due to augmentor lighting can be detected using a pressure measurement. A disturbance in the augmentor propagates quickly to the fan exit station, well before the spool speeds have responded. At 58.5K/2.15, the operating point has the same density as 30K/0.9 but at a higher pressure and temperature. The corrected airflow at this point corresponds to approximately a PLA of 35° at 30K/0.9. The 36°/30K/0.9 model is similar to the model at 83°/58.5K/2.15.

The mid-power supersonic points were 65K/2.5 and 40K/1.8. At 40K/1.8, the model has coupled rotor roots. This point has roughly the same pressure as sea level static and roughly the same temperature as the 0K/1.2 point. The behavior is quite different than either of these points. It lies along a constant density line corresponding to 20K/0.9 conditions at a PLA of approximately 40°. No models were generated at this point but extrapolation of the low power, 30K/0.9 behavior would indicate a system response of the type exhibited by the 40K/1.8 model. At 2.5/65K, the operating point has the same density as 30K/0.9 at extremely high inlet temperatures. The

airflow is low, corresponding to $28^{\circ}/30K/0.9$. The model does not exhibit this type of behavior; rather, it is more typical of the sea level static response at low power.

The high pressure points consisted of $20K/1.8$ and $40K/2.2$ at intermediate power. The $20K/1.8$ corresponds to the density at $0K/1.2$ with higher pressures and temperatures. The behavior of these models is nearly identical. The $40K/2.2$ operating point has the same pressure as $0K/1.2$, and roughly the same temperature as $58.5K/2.15$ at a lower density than $0K/1.2$. The response has a coupled rotor system. This behavior does not correspond to any other high pressure system. It has the same characteristics, however, as $58.5K/2.15$ linear system.

The conclusions important in the analysis of the supersonic operating conditions are as follows. The low pressure supersonic points are similar to the corresponding constant density operating points at subsonic altitude points with the same corrected airflow. Higher temperatures tend to destroy this correspondence.

Supplemental Models

A linear model was generated at the $45K/0.9$ flight point at maximum (full augmented) power. This point is representative of the flight conditions where pressure spike suppression during augmentor ignition is important. The low ambient pressure and fan stability margin at intermediate power make this flight point critical to satisfactory augmentor operation. A comparison of the intermediate and maximum power model roots are shown in Table D.6. During augmentor operation, the engine airflow is nearly constant and the operation of the core engine and fan should be the same throughout augmented operation. It is important to analyze the differences in the transient behavior to assess the impact of differences on performance.

Table D.6
Eigenvalues of Intermediate Power and Maximum
Power Systems at 45,000 Ft,
Mach Number = 0.9

83/45K/0.9	130/45K/0.9
-592	-540
-172	-151
-57	-55
-51	$-49 \pm 6j$
-46	
-45	-44
$-21 \pm 3j$	$-18 \pm 3j$
-22	-22
-20	-21
-16	-19
-6.6*	-6.3*
-1.9*	$-1.2 \pm 0.4j^*$
-0.6*	
-2	-2
-0.7	-0.7

* Dominant roots

Recalling the intermediate model at these flight conditions contained an uncoupled set of real roots, the fully augmented roots exhibited lower frequency, coupled, spool response. Since augmentor control is primarily pressure modulation, the pressure dynamics of both models are similar.

A linear model was generated at sea level static idle conditions with the full specified level of component deterioration, horsepower extraction and bleed flow. It was determined that sea level static idle conditions were the most sensitive to installation and deterioration effects. The results are

shown in Table D.7. Clearly, the impact on the engine dynamics is small while the change of the control effectiveness is more pronounced.

Table D.7
Eigenvalues of Models at Sea Level Static, Idle Power
With and Without Full Installation and
Deterioration Effects

20/OK/0 NONE	20/OK/0 NOMINAL
-831	-827
-144	-146
-87	-52
$-50 \pm 0.1j$	$-50 \pm 2j$
-21	-44
-20	-20
$-25 \pm 8j$	$-25 \pm 3j$
-20	-20
-24	-21
$-5 \pm 2j$	$-4.7 \pm 2j$
$-0.7 \pm .2j$	$-0.7 \pm .2j$
-2	-2

D.2 SELECTED LINEAR MODELS

$$\dot{\delta x} = F\delta x + G\delta u$$

$$\delta y = H\delta x + D\delta u$$

Note 1: For state, control and output ordering, see printout and symbol table.

Note 2: Models are normalized by the baseline operating point (with the exceptions shown below) so that units of all quantities are dimensionless.

$$(\text{DP25QT})_{\text{NOM}} = 1.0$$

$$(\text{DP25SC})_{\text{NOM}} = 1.0$$

Note 3: Table D.8 lists the linear models included.

Table D.8
Index of Linear Model Data

CASE	PLA (DEG)	ALTITUDE (FT)	MACH NO.	COMMENTS
1	83	0	0	Static reduction on T_{T4L0} { Nominal extractions; Static Reduction on T_{T4L0}
2	52	0	0	
3	24	0	0	
4	24	0	0	
5	20	0	0	
6	20	0	0	
7	20	0	0	
8	83	30,000	0.9	
9	20	30,000	0.9	
10	83	0	1.2	
11	83	45,000	0.9	

*** THE MATRICES IN FINAL FORM ***

CASE 1

F-MATRIX

	SNFAN	SNCOM	PT7M	WFCOM	PT3	FTT	PT45	TT25H	TT25C	TT3
SNFAN	-4.3320+000	2.1273+001	-2.9846+000	2.5083+002	1.9326+001	0.0000	3.9498+000	-1.5053+001	7.0752+002	-1.5293+001
SNCOM	-3.5069+001	-5.6480+000	-1.4079+000	1.2613+001	3.7160+000	0.0000	-1.6079+000	1.5526+000	1.1600+001	-3.0490+001
PT7M	2.0431+000	-4.8604+000	-1.0050+001	2.5753+000	4.6087+001	0.0000	3.7445+000	3.5327+000	-1.7035+001	-7.8238+001
WFCOM	0.0000	0.0000	0.0000	-1.0000+001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
PT3	2.8304+001	2.6896+002	1.1641+002	3.1747+000	-1.6450+002	0.0000	-7.2618+001	-1.6532+002	-1.0305+001	2.0637+001
FTT	0.0000	0.0000	0.0000	0.0000	0.0000	-2.5080+001	0.0000	0.0000	0.0000	0.0000
PT45	5.4376+001	-1.3832+001	4.3080+001	3.1199+001	4.9724+002	0.0000	-5.7810+002	-6.9709+001	-8.3385+000	-3.5619+001
TT25H	1.1154+001	-1.9905+001	2.0651+000	2.9313+001	-5.0692+003	0.0000	-6.9713+002	-1.9780+001	-1.6860+001	-4.3082+002
TT25C	8.9975+000	-1.9267+001	4.4071+000	-2.2915+001	3.1481+002	0.0000	-2.3392+002	-5.9180+002	-2.0450+001	-5.2892+002
TT3	-6.6586+001	7.5000+000	-2.8601+000	-4.9780+001	4.2563+000	0.0000	5.9243+002	1.5059+001	2.9443+001	-1.997+001
TT45H	-4.2235+002	9.6136+002	-1.4742+001	2.0841+001	1.9723+002	0.0000	9.3873+004	2.2655+001	1.5463+002	3.8550+000
TT45L	-5.6341+003	-1.2057+002	1.9604+002	2.7754+002	2.5922+003	0.0000	1.1267+004	2.7494+002	2.1408+003	5.1396+001
TT45C	-4.1396+000	-2.9118+001	-1.7747+001	2.0231+001	3.2667+000	0.0000	3.7031+001	2.6114+001	1.8587+000	1.8365+001
TT45H	-1.4346+001	3.0765+000	-6.1005+001	7.8795+001	-1.0342+001	0.0000	1.0283+001	8.4566+001	5.6160+002	7.5427+000
TT45L	-9.1520+001	-1.7871+000	3.3758+000	3.1346+001	-5.0592+000	0.0000	4.1152+000	3.5790+001	2.2497+002	3.0172+000
TT5	-1.6370+001	5.0610+001	3.0847+001	2.5498+002	-5.8760+002	0.0000	-1.2903+000	6.9248+001	4.6555+002	-3.7201+000
TT6C	-1.1916+001	1.6921+001	1.0191+001	1.0969+000	-1.0186+000	0.0000	-7.4982+003	-4.112+001	1.9661+001	2.3986+001
TT7M							8.0663+000	-1.4772+001	-1.0817+000	-6.1727+001

F-MATRIX

	TT4PHI	TT4PLO	TT4	TT45H1	TT45LO	TT5	TT6C	TT7M
SNFAN	2.4645+001	1.6144+002	-1.2005+000	1.6029+000	1.6950+001	-1.3236+001	-1.6144+002	-1.2821+002
SNCOM	2.2318+000	2.3456+001	-9.4684+001	-1.5619+002	-1.3362+002	-1.6728+002	-4.1648+002	-1.5996+002
PT7M	1.0504+001	-3.6678+001	-2.9383+000	-4.2569+001	-4.7324+001	1.4686+000	8.0371+002	-4.3661+001
WFCOM	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
PT3	3.9490+001	4.9882+001	4.5058+001	5.2228+001	5.4776+001	5.7306+001	2.7014+000	5.2234+001
FTT	0.0000	0.0000	0.0000	2.2507+001	2.5008+002	0.0000	0.0000	0.0000
PT45	-7.8480+001	-1.2388+001	1.7144+002	-3.8562+000	-4.0486+000	-3.9045+000	-3.0373+000	-4.0488+000
TT25H	-5.1973+002	-5.0699+002	-1.5211+002	-4.6885+002	-4.4902+002	-4.4362+002	8.8728+002	-4.4906+002
TT25C	8.5630+002	8.0068+002	-1.5111+002	9.3180+002	9.189+002	1.0326+001	1.1456+001	9.1178+002
TT3	3.4122+000	2.9626+002	7.7282+003	2.9627+002	2.6622+002	2.9618+002	-2.6404+002	2.9625+002
TT45H	-5.0000+001	-4.6925+001	4.6016+001	-3.7553+003	3.7553+003	-8.4471+003	-5.6344+003	-4.6447+003
TT45L	-6.0003+000	-6.4720+001	6.1304+000	-4.5068+004	-4.0663+004	-1.1288+003	-7.8862+004	-5.6333+004
TT4	1.9641+001	1.8032+001	-4.7690+001	1.7388+001	1.7147+001	1.6585+001	-1.6420+001	1.7145+001
TT45H	-1.2775+001	1.4236+000	5.9643+001	-5.0000+001	0.0000	-9.9836+003	-1.6217+002	3.7431+003
TT45L	-5.1102+000	-5.613+001	2.3854+001	-1.8000+001	-2.0000+000	-3.5933+003	-6.2698+003	-1.3471+003
TT5	-6.2848+000	-6.9847+001	2.9336+001	3.3525+000	-3.9644+001	-1.9780+001	-2.6881+002	-5.3464+004
TT6C	-2.4993+003	-2.4993+003	7.1222+002	-2.4994+003	-2.4994+003	-2.5000+003	-2.0000+001	-2.5000+003
TT7M	9.4136+001	-1.2002+002	-5.1334+000	-1.4059+001	-1.2002+001	3.9313+001	1.0921+001	-5.0140+001

G-MATRIX

	WFBM	AMIX	CIVV	RCVV	ELC
SNFAN	0.0000	-1.607-001	1.8127-002	5.2331-004	9.5605-002
SNCOM	0.0000	-1.1608-001	1.0613-003	-1.8331-002	2.3521-001
PT7M	0.0000	-6.5882-000	-2.0194-002	-2.0533-002	-2.3878+000
WFCOM	1.0000+001	0.0000	0.0000	0.0000	0.0000
PT3	0.0000	9.5991+000	-7.0012-002	5.3099-001	-1.7362+002
PT1T	0.0000	0.0000	0.0000	0.0000	0.0000
PT6S	0.0000	5.5030+000	4.0991-002	1.2669-001	3.3700-001
TT2SH	0.0000	2.6131+001	-2.1997-002	-2.5740-003	-1.5767-001
TT2SC	0.0000	1.2658-001	-2.0744-002	1.6460-003	9.0357-001
TT3	0.0000	-2.6283-001	1.1570-003	3.0334-002	6.1819-001
TT6PHI	0.0000	-5.9956-003	1.7016-004	-5.8988-004	-2.6339+000
TT6PLO	0.0000	-7.4319-004	2.2658-005	-7.8222-005	-3.4847-001
TT4	0.0000	-1.4389+000	7.2338-003	-6.9514-002	2.8965+001
TT4SHI	0.0000	-1.9040-002	3.0605-004	-2.3993-003	-3.5883+000
TT4SLO	0.0000	-1.6088-002	1.1745-004	-9.5556-004	-1.4337+000
TT5	0.0000	2.7681-002	-2.1122-004	-1.8178-003	-1.4747+000
TT6C	0.0000	3.5957-002	1.8240-003	1.2421-003	-4.3040-002
TT7M	0.0000	8.4772-001	1.0003-001	4.4853-002	-1.0490-001

H-MATRIX

	SNFAN	SNCOM	PT7M	WFCOM	PT3	FT1T	PT4S	TT2SH	TT2SC	TT3
FMX	3.3261-001	-5.6229-001	6.5338-002	-3.5518-002	1.3652-001	0.0000	6.4380-001	5.3928-001	4.0281-002	-4.6488-002
MFAN	6.1767-001	1.7228-004	-1.9746-003	5.9175-003	0.0000	0.0000	0.0000	-1.8555-004	1.7233-004	0.0000
TT6	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
SHAF	3.9581+000	3.4697-001	3.4209+000	1.1445-001	7.4384-004	0.0000	6.8874-002	-2.7053-001	3.4662-001	2.5619-002
SHMC	8.3320-001	8.2255+000	3.5799+000	3.8522-001	-5.1375+000	0.0000	-7.3789-002	-4.2650+000	-3.7470-001	-3.2527-002
DP25Q1	1.6631-001	-3.7048-001	-6.6009-001	-4.8873-002	4.7498-002	0.0000	1.4112-002	3.4185-001	1.7019-001	6.4978-001
DP25SC	9.5302-002	5.7653-002	-1.7076-001	-1.1153-002	-3.4821-003	0.0000	3.6480-003	3.5063-002	6.1063-002	1.8368-003

H-MATRIX

	TT6PHI	TT6PLO	TT4	TT4SHI	TT4SLO	TT5	TT6C	TT7M
FMX	8.8500-002	1.4036-002	-3.7962-001	4.4344-003	5.0607-003	4.1534-001	1.1017-001	5.1659-003
MFAN	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
TT4	0.0000	0.0000	1.0000+000	0.0000	0.0000	0.0000	0.0000	0.0000
SHAF	3.7364-002	3.4020-002	9.2951-003	3.2228-002	3.2228-002	3.0618-002	-2.9685-002	3.2475-002
SHMC	3.8417-002	-3.6815-002	-9.4970-003	-3.5319-002	-3.5008-002	-3.3772-002	3.3771-002	-3.5132-002
DP25Q1	7.8205-003	7.5249-001	2.0507-003	6.8561-003	6.8561-003	6.3679-003	-5.5583-003	6.7009-003
DP25SC	2.1701-003	2.1462-003	5.1268-004	1.8880-003	1.8881-003	1.8609-003	-1.2279-003	1.8488-003

F100 LINEAR MODEL 83/0/0K 2/12/76

D-MATRIX		WPMH	ANIX	CIV	RCVV	BLC
FVX	0.000	-7.9141-002	-3.7765-003	-1.5500-003	7.2050-002	
WPN	0.000	4.1774-003	-5.1350-003	4.6079-006	-5.3411-007	
TTB	0.000	0.000	0.000	0.000	0.000	
SHAF	0.000	-1.7301-001	5.2597-002	2.5801-003	1.6825-001	
SWHC	0.000	3.4194-001	-1.3768-003	-2.3762-002	-4.6623-001	
DB2SGT	0.000	-3.6629-002	-2.3977-003	-7.8320-004	6.0940-002	
DB2SSC	0.000	-7.1980-003	-1.0576-003	2.5100-004	1.3000-002	

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-2.50000-001)+J(0.00000)	0.00000	1.00000	1 (0.00000)+J(0.00000)	0.000000	0.0000
			2 (0.00000)+J(0.00000)	0.000000	0.0000
			3 (0.00000)+J(0.00000)	0.000000	0.0000
			4 (0.00000)+J(0.00000)	0.000000	0.0000
			5 (0.00000)+J(0.00000)	0.000000	0.0000
			6 (1.00000+000)+J(0.00000)	1.000000	0.0000
			7 (0.00000)+J(0.00000)	0.000000	0.0000
			8 (0.00000)+J(0.00000)	0.000000	0.0000
			9 (0.00000)+J(0.00000)	0.000000	0.0000
			10 (0.00000)+J(0.00000)	0.000000	0.0000
			11 (0.00000)+J(0.00000)	0.000000	0.0000
			12 (0.00000)+J(0.00000)	0.000000	0.0000
			13 (0.00000)+J(0.00000)	0.000000	0.0000
			14 (0.00000)+J(0.00000)	0.000000	0.0000
			15 (0.00000)+J(0.00000)	0.000000	0.0000
			16 (0.00000)+J(0.00000)	0.000000	0.0000
			17 (0.00000)+J(0.00000)	0.000000	0.0000
			18 (0.00000)+J(0.00000)	0.000000	0.0000
(-5.77397+002)+J(0.00000)	0.00000	1.00000	1 (-6.86800-003)+J(0.00000)	0.068680	0.0000
			2 (3.11880-003)+J(0.00000)	0.031188	0.0000
			3 (-6.86327-003)+J(0.00000)	0.065833	0.0000
			4 (0.00000)+J(0.00000)	0.000000	0.0000
			5 (2.78685-003)+J(0.00000)	0.027868	0.0000
			6 (7.87631-006)+J(0.00000)	0.000079	0.0000
			7 (1.60000+000)+J(0.00000)	1.000000	0.0000
			8 (2.84443-004)+J(0.00000)	0.002844	0.0000
			9 (2.14720-004)+J(0.00000)	0.002170	0.0000
			10 (-2.16972-004)+J(0.00000)	0.002170	0.0000
			11 (6.82230-005)+J(0.00000)	0.000682	0.0000
			12 (9.05550-006)+J(0.00000)	0.000091	0.0000
			13 (8.12150-004)+J(0.00000)	0.008122	0.0000
			14 (1.03417-002)+J(0.00000)	0.015347	0.0000
			15 (7.69666-003)+J(0.00000)	0.076967	0.0000
			16 (2.32697-003)+J(0.00000)	0.023270	0.0000
			17 (5.19150-006)+J(0.00000)	0.000052	0.0000
			18 (-1.52547-002)+J(0.00000)	0.0152547	0.0000

```
(=i.74625+002)+J( 0.0000 ) h.00000
1 1.00000 (2.4106+002)+J( 0.00000 ) -.028106 .00000
2 (6.10456+003)+J( 0.00000 ) -.0081046 .00000
3 (-2.61547+02)+J( 0.00000 ) -.0261547 .00000
4 (0.0000 )+J( 0.00000 ) .000000 .00000
5 (8.2827+01)+J( 0.00000 ) -.828274 .00000
6 (-1.87602+006)+J( 0.00000 ) .000000 .00000
7 (1.0000+00)+J( 0.00000 ) 1.000000 .00000
8 (2.5144+003)+J( 0.00000 ) .025914 .00000
9 (-2.5147+003)+J( 0.00000 ) -.025145 .00000
10 (1.5599+002)+J( 0.00000 ) -.025599 .00000
11 (1.0304+002)+J( 0.00000 ) .017404 .00000
12 (1.3676+003)+J( 0.00000 ) .013968 .00000
13 (-2.7625+002)+J( 0.00000 ) -.027625 .00000
14 (1.3321+003)+J( 0.00000 ) .013932 .00000
15 (5.4217+004)+J( 0.00000 ) .005422 .00000
16 (2.5399+002)+J( 0.00000 ) .025399 .00000
17 (1.51308+004)+J( 0.00000 ) .001513 .00000
18 (-6.61622+002)+J( 0.00000 ) -.0661622 .00000
```

```
(=5.89420+001)+J( 0.00000 ) h.00000
1 1.00000 (-2.59231+002)+J( 0.00000 ) -.0259231 .00000
2 (-1.57144+002)+J( 0.00000 ) -.0157144 .00000
3 (6.0302+003)+J( 0.00000 ) .060730 .00000
4 (0.0000 )+J( 0.00000 ) .000000 .00000
5 (-6.4443+002)+J( 0.00000 ) -.064443 .00000
6 (-3.9583+003)+J( 0.00000 ) -.039958 .00000
7 (-1.41021+001)+J( 0.00000 ) -.141021 .00000
8 (8.1827+003)+J( 0.00000 ) .081563 .00000
9 (2.29491+003)+J( 0.00000 ) .022949 .00000
10 (6.18726+003)+J( 0.00000 ) .061873 .00000
11 (3.3307+001)+J( 0.00000 ) .333068 .00000
12 (4.1618+002)+J( 0.00000 ) .041618 .00000
13 (-6.5443+002)+J( 0.00000 ) -.065443 .00000
14 (1.0000+000)+J( 0.00000 ) 1.000000 .00000
15 (3.7929+001)+J( 0.00000 ) .379289 .00000
16 (1.8451+001)+J( 0.00000 ) .184514 .00000
17 (-9.8660+004)+J( 0.00000 ) -.009863 .00000
18 (-7.5604+001)+J( 0.00000 ) -.756040 .00000
```

(-5.00462+001)+J(0.00000	1.00000	1	(8.05030-004)+J(0.00000)	.008050	.00000
		2	(8.40310-005)+J(0.00000)	.000840	.00000
		3	(9.76127-003)+J(0.00000)	.0097613	.00000
		4	(0.00000)+J(0.00000)	.000000	.00000
		5	(1.41316-002)+J(0.00000)	.0141316	.00000
		6	(6.70620-005)+J(0.00000)	.006671	.00000
		7	(7.79117-003)+J(0.00000)	.0077912	.00000
		8	(5.26858-004)+J(0.00000)	.005269	.00000
		9	(4.75243-003)+J(0.00000)	.0047526	.00000
		10	(2.25920-003)+J(0.00000)	.0022592	.00000
		11	(5.75279-003)+J(0.00000)	.0057528	.00000
		12	(7.01005-004)+J(0.00000)	.007010	.00000
		13	(3.20675-004)+J(0.00000)	.003207	.00000
		14	(1.42034-002)+J(0.00000)	.0142434	.00000
		15	(5.34473-003)+J(0.00000)	.0053447	.00000
		16	(1.90029-003)+J(0.00000)	.0019003	.00000
		17	(3.14805-003)+J(0.00000)	.0031480	.00000
		18	(1.00000+000)+J(0.00000)	1.000000	.00000
(-3.88570+001)+J(0.00000	1.00000	1	(4.70347-003)+J(0.00000)	.0047635	.00000
		2	(6.43748-002)+J(0.00000)	.0643748	.00000
		3	(1.92562-002)+J(0.00000)	.0192562	.00000
		4	(0.00000)+J(0.00000)	.000000	.00000
		5	(1.10533-002)+J(0.00000)	.0110533	.00000
		6	(5.62227-004)+J(0.00000)	.0056222	.00000
		7	(5.64354-002)+J(0.00000)	.0564354	.00000
		8	(2.90106-003)+J(0.00000)	.0029011	.00000
		9	(1.20577-002)+J(0.00000)	.0120577	.00000
		10	(2.69731-002)+J(0.00000)	.0269731	.00000
		11	(1.00000+000)+J(0.00000)	1.000000	.00000
		12	(1.18208-001)+J(0.00000)	.1182082	.00000
		13	(2.39846-001)+J(0.00000)	.2398465	.00000
		14	(9.25542-002)+J(0.00000)	.0925542	.00000
		15	(3.40720-002)+J(0.00000)	.0340720	.00000
		16	(2.55567-002)+J(0.00000)	.0255567	.00000
		17	(1.28514-002)+J(0.00000)	.0128514	.00000
		18	(2.27430-001)+J(0.00000)	.2274300	.00000

```
(-4.76710+001)+J( 0.00000 ) 0.00000 1.00000
1 (-2.7219=-002)+J( 0.00000 ) -.0272619 .00000
2 (-8.29645=-003)+J( 0.00000 ) .0089665 .00000
3 (-1.88001=-002)+J( 0.00000 ) .0180001 .00000
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 (-1.26851=-002)+J( 0.00000 ) .0126851 .00000
6 (-2.2075=-003)+J( 0.00000 ) .0033207 .00000
7 (-1.59987=-002)+J( 0.00000 ) .0159987 .00000
8 (-1.2565=-002)+J( 0.00000 ) .012565 .00000
9 (-8.8528=-005)+J( 0.00000 ) .0000686 .00000
10 (-1.1622=-002)+J( 0.00000 ) .0116222 .00000
11 (-1.5446=-001)+J( 0.00000 ) .154464 .00000
12 (-1.8691=-002)+J( 0.00000 ) .018691 .00000
13 (-2.6503=-003)+J( 0.00000 ) .0066506 .00000
14 (-6.5135=-001)+J( 0.00000 ) .6513349 .00000
15 (-2.4390=-001)+J( 0.00000 ) .243901 .00000
16 (-5.3537=-002)+J( 0.00000 ) .0535376 .00000
17 (-4.9463=-005)+J( 0.00000 ) .0000495 .00000
18 ( 1.0000+000)+J( 0.00000 ) 1.0000000 .00000
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(-1.79165+001)+J( 4.39010+000 ) 1.84465+001 .97127
1 (-2.03358=-002)+J( -1.00562=-002 ) .0226863 .153.68728
2 (-1.46225=-002)+J( -3.5059=-002 ) .0378664 .112.64000
3 (-4.79146=-002)+J( 1.5612=-002 ) .0503940 .161.95242
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 (-4.6842=-002)+J( -4.1757=-002 ) .0627689 .41.70194
6 (-8.39347=-04)+J( -3.6172=-003 ) .0037133 .103.06389
7 (-2.6463=-002)+J( -4.1427=-002 ) .0491288 .57.4416
8 (-5.85334=-002)+J( 7.2390=-002 ) .093757 128.9377
9 (-8.1566=-003)+J( 3.5266=-002 ) .036001 103.02668
10 (-6.9448=-002)+J( 1.64551=-001 ) .1786046 67.11898
11 (-1.5838=-001)+J( 2.5776=-001 ) .302652 58.33979
12 (-1.6221=-002)+J( 2.4966=-002 ) .030251 53.6752
13 (-8.05181=-002)+J( 1.8078=-001 ) .197087 65.92323
14 (-1.3160=-001)+J( 2.5836=-001 ) .2897102 63.0890
15 (-4.8201=-002)+J( 8.2735=-002 ) .0951622 59.7555
16 (-7.8113=-001)+J( 1.5201=-001 ) .795640 11.01027
17 (-1.18466=-001)+J( 8.7971=-002 ) .147572 36.59725
18 ( 1.0000+000)+J( 0.00000 ) 1.0000000 .00000
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(-6.71900+000)+J( 1.29305+000) 6.84229+000 .98198
1 ( 3.2227-001)+J( 5.6113+001) .6471061
2 ( 5.2799-003)+J(-1.20625-001) .1207401
3 ( 1.0000+000)+J( 0.00000 ) 1.0000000
4 ( 0.0000 )+J( 0.00000 ) .0000000
5 ( 3.8747-001)+J(-3.72815-001) .5377067
6 (-2.7377-003)+J(-1.74618-002) .0176748
7 ( 3.4375-001)+J(-2.9482-001) .4526651
8 ( 4.6062-001)+J( 4.2494+001) .626697
9 ( 5.7583-001)+J( 3.2987-001) .6636262
10 ( 4.57915-001)+J( 2.32068-001) .5133634
11 ( 1.63172-001)+J( 4.3174+001) .461511
12 ( 1.52791-002)+J( 1.49455-002) .021733
13 ( 1.04328-001)+J( 3.89895-001) .4036118
14 ( 1.7250-001)+J( 4.7925-001) .5093790
15 ( 5.90553-002)+J( 6.72495-002) .089091
16 ( 4.50199-001)+J( 6.79128-001) .810774
17 ( 9.00504-001)+J( 3.82765-001) .978766
18 ( 6.57427-001)+J( 2.50000-001) .7033580
```

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(-1.84161+001)+J( 0.00000 ) 1.00000
1 (-1.81328-003)+J( 0.00000 ) .0018133
2 (-2.74681-004)+J( 0.00000 ) .0002747
3 ( 1.25082-002)+J( 0.00000 ) .0125082
4 ( 0.00000 )+J( 0.00000 ) .0000000
5 ( 2.77915-002)+J( 0.00000 ) .0277915
6 ( 9.36736-005)+J( 0.00000 ) .000937
7 ( 1.75955-002)+J( 0.00000 ) .017955
8 ( 4.8752-003)+J( 0.00000 ) .004795
9 ( 6.02856-002)+J( 0.00000 ) .080856
10 ( 6.82392-003)+J( 0.00000 ) .006239
11 ( 4.55160-003)+J( 0.00000 ) .004536
12 ( 4.57604-004)+J( 0.00000 ) .000576
13 ( 3.54870-003)+J( 0.00000 ) .003587
14 ( 7.29399-003)+J( 0.00000 ) .007290
15 ( 2.39969-003)+J( 0.00000 ) .002397
16 ( 9.28307-002)+J( 0.00000 ) .0928307
17 ( 1.00000+000)+J( 0.00000 ) .0000000
18 ( 2.37226-001)+J( 0.00000 ) .2372260
```



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(=6.48252-001)+J( 0.00000 ) 0.00000 1.00000
1 ( 1.2050-001)+J( 0.00000 ) .120499 .00000
2 ( 1.36041-001)+J( 0.00000 ) .1360408 .00000
3 (-4.49684-002)+J( 0.00000 ) -.0449684 .00000
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 ( 1.25629-001)+J( 0.00000 ) .1256289 .00000
6 ( 4.13980-003)+J( 0.00000 ) .0041398 .00000
7 ( 7.78638-002)+J( 0.00000 ) .0778638 .00000
8 ( 6.23816-002)+J( 0.00000 ) .0623816 .00000
9 ( 4.87333-002)+J( 0.00000 ) .0487333 .00000
10 ( 1.34673-001)+J( 0.00000 ) .1346733 .00000
11 ( 3.16131-002)+J( 0.00000 ) .0316131 .00000
12 ( 1.00000-000)+J( 0.00000 ) 1.0000000 .00000
13 ( 2.26083-002)+J( 0.00000 ) .0226083 .00000
14 (-6.43778-003)+J( 0.00000 ) -.064378 .00000
15 (-7.98632-003)+J( 0.00000 ) -.079863 .00000
16 (-3.71893-002)+J( 0.00000 ) -.0371893 .00000
17 ( 5.11502-002)+J( 0.00000 ) .0511502 .00000
18 (-2.33920-002)+J( 0.00000 ) -.0233920 .00000
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(=2.06903+001)+J( 0.00000 ) 0.00000 1.00000
1 ( 1.94517-002)+J( 0.00000 ) .0194517 .00000
2 ( 1.00695-002)+J( 0.00000 ) .0100695 .00000
3 (-7.1105-002)+J( 0.00000 ) -.071105 .00000
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 (-7.51108-002)+J( 0.00000 ) -.0751108 .00000
6 ( 8.55131-004)+J( 0.00000 ) .008551 .00000
7 (-7.5256-002)+J( 0.00000 ) -.075256 .00000
8 ( 5.23998-003)+J( 0.00000 ) .0052400 .00000
9 ( 1.54517-002)+J( 0.00000 ) .0154517 .00000
10 (-1.17747-001)+J( 0.00000 ) -.117747 .00000
11 (-7.58199-002)+J( 0.00000 ) -.0758199 .00000
12 (-7.92522-003)+J( 0.00000 ) -.079252 .00000
13 (-3.84043-002)+J( 0.00000 ) -.0384043 .00000
14 (-7.48644-002)+J( 0.00000 ) -.0748644 .00000
15 (-2.51656-002)+J( 0.00000 ) -.0251656 .00000
16 ( 8.80808-001)+J( 0.00000 ) .8808077 .00000
17 (-3.63883-001)+J( 0.00000 ) -.3638827 .00000
18 ( 1.00000-000)+J( 0.00000 ) 1.0000000 .00000
```

(-2.62888+000)+J(0.00000)	0.00000	1.00000	(1.00000+000)+J(0.00000)	.00000000	.00000
(6.78541-001)+J(0.00000)			(6.78541-001)+J(0.00000)	.00000000	.00000
(3.86668-001)+J(0.00000)			(3.86668-001)+J(0.00000)	.3866685	.00000
(0.00000)+J(0.00000)			(0.00000)+J(0.00000)	.00000000	.00000
(7.88283-001)+J(0.00000)			(7.88283-001)+J(0.00000)	.7882834	.00000
(-2.06219-002)+J(0.00000)			(-2.06219-002)+J(0.00000)	.0208219	.00000
(8.53717-001)+J(0.00000)			(8.53717-001)+J(0.00000)	.6537367	.00000
(6.76907-001)+J(0.00000)			(6.76907-001)+J(0.00000)	.6769067	.00000
(5.92791-001)+J(0.00000)			(5.92791-001)+J(0.00000)	.5927914	.00000
(9.85029-001)+J(0.00000)			(9.85029-001)+J(0.00000)	.9850295	.00000
(2.72106-001)+J(0.00000)			(2.72106-001)+J(0.00000)	.2721057	.00000
(-4.37957-002)+J(0.00000)			(-4.37957-002)+J(0.00000)	.0437957	.00000
(1.97620-001)+J(0.00000)			(1.97620-001)+J(0.00000)	.1976202	.00000
(2.64526-001)+J(0.00000)			(2.64526-001)+J(0.00000)	.2645262	.00000
(-4.00854-001)+J(0.00000)			(-4.00854-001)+J(0.00000)	.4009538	.00000
(2.07153-001)+J(0.00000)			(2.07153-001)+J(0.00000)	.2071526	.00000
(6.82336-001)+J(0.00000)			(6.82336-001)+J(0.00000)	.6823357	.00000
(2.43677-001)+J(0.00000)			(2.43677-001)+J(0.00000)	.2436768	.00000

(-2.20014+001)+J(0.00000)	0.00000	1.00000	(6.28471-003)+J(0.00000)	.0062847	.00000
(6.06074-003)+J(0.00000)			(6.06074-003)+J(0.00000)	.0060607	.00000
(-2.54321-002)+J(0.00000)			(-2.54321-002)+J(0.00000)	.0254321	.00000
(0.00000)+J(0.00000)			(0.00000)+J(0.00000)	.00000000	.00000
(2.44656-003)+J(0.00000)			(2.44656-003)+J(0.00000)	.0024466	.00000
(6.24645-004)+J(0.00000)			(6.24645-004)+J(0.00000)	.0006246	.00000
(-9.07196-005)+J(0.00000)			(-9.07196-005)+J(0.00000)	.0090720	.00000
(6.66601-005)+J(0.00000)			(6.66601-005)+J(0.00000)	.0006667	.00000
(-1.00676-001)+J(0.00000)			(-1.00676-001)+J(0.00000)	.1006757	.00000
(-4.77783-002)+J(0.00000)			(-4.77783-002)+J(0.00000)	.0477783	.00000
(-5.86317-002)+J(0.00000)			(-5.86317-002)+J(0.00000)	.0586317	.00000
(-6.23004-003)+J(0.00000)			(-6.23004-003)+J(0.00000)	.0062300	.00000
(-3.14466-002)+J(0.00000)			(-3.14466-002)+J(0.00000)	.0314466	.00000
(-5.81671-002)+J(0.00000)			(-5.81671-002)+J(0.00000)	.0581671	.00000
(-1.98013-002)+J(0.00000)			(-1.98013-002)+J(0.00000)	.0198013	.00000
(3.08627-001)+J(0.00000)			(3.08627-001)+J(0.00000)	.3086266	.00000
(1.00000+000)+J(0.00000)			(1.00000+000)+J(0.00000)	.0000000	.00000
(8.17426-001)+J(0.00000)			(8.17426-001)+J(0.00000)	.8174259	.00000

(-1.90745+000)+J(0.00000)	0.00000	1.00000	1	(1.66761+001)+J(0.00000)	1.667606	0.0000
			2	(6.57972+002)+J(0.00000)	.0657972	0.0000
			3	(-2.68818+002)+J(0.00000)	-.0268818	0.0000
			4	(0.00000)+J(0.00000)	.0000000	0.0000
			5	(2.92382+002)+J(0.00000)	.0292382	0.0000
			6	(-2.52502+002)+J(0.00000)	-.025502	0.0000
			7	(1.91554+002)+J(0.00000)	.0191554	0.0000
			8	(9.60330+002)+J(0.00000)	.0960330	0.0000
			9	(7.95169+002)+J(0.00000)	.0795169	0.0000
			10	(1.15570+001)+J(0.00000)	.1155701	0.0000
			11	(7.07222+002)+J(0.00000)	.0707222	0.0000
			12	(-2.35639+002)+J(0.00000)	-.0235639	0.0000
			13	(6.41236+002)+J(0.00000)	.0641236	0.0000
			14	(7.48346+002)+J(0.00000)	.0748346	0.0000
			15	(1.00000+000)+J(0.00000)	1.0000000	0.0000
			16	(4.73601+002)+J(0.00000)	.0473601	0.0000
			17	(8.54648+002)+J(0.00000)	.0854648	0.0000
			18	(-4.02946+003)+J(0.00000)	-.0040295	0.0000

(-1.00000+001)+J(0.00000)	0.00000	1.00000	1	(3.16248+001)+J(0.00000)	.3162483	0.0000
			2	(2.08761+002)+J(0.00000)	.0208761	0.0000
			3	(4.96976+001)+J(0.00000)	.4969759	0.0000
			4	(-6.52085+001)+J(0.00000)	-.6520851	0.0000
			5	(3.55694+002)+J(0.00000)	.0355694	0.0000
			6	(-4.53331+004)+J(0.00000)	-.0004533	0.0000
			7	(-5.44931+002)+J(0.00000)	-.0544931	0.0000
			8	(4.34007+001)+J(0.00000)	.4340089	0.0000
			9	(5.05835+001)+J(0.00000)	.5068354	0.0000
			10	(5.69055+001)+J(0.00000)	.5690546	0.0000
			11	(1.53714+002)+J(0.00000)	.0153714	0.0000
			12	(1.10056+003)+J(0.00000)	.0011007	0.0000
			13	(-3.13748+002)+J(0.00000)	-.0313748	0.0000
			14	(1.91337+002)+J(0.00000)	.0191337	0.0000
			15	(4.55954+003)+J(0.00000)	.0045596	0.0000
			16	(2.18296+001)+J(0.00000)	.2182962	0.0000
			17	(1.00000+000)+J(0.00000)	1.0000000	0.0000
			18	(3.19464+001)+J(0.00000)	.3194645	0.0000

T-MATRIX

	1	2	3	4	5	6	7	8	9	10
1	0.0000	-5.8680-003	-2.4811-002	-2.5923-002	8.0503-004	4.7635-003	-2.7268-002	8.4327-002	-4.8422-002	1.2774+000
2	0.0000	3.1188-003	-8.1045-003	1.5714-002	8.4031-005	-6.4335-002	8.2965-003	1.5953-001	3.1102-002	-2.0373-001
3	0.0000	-6.5833-003	-2.6155-002	6.0730-003	9.7613-003	1.9266-002	1.8800-002	5.9000-002	-2.058-001	9.5055-001
4	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	2.7845-003	8.2583-001	-6.4444-002	1.4132-002	1.1035-002	1.2688-002	3.4424-002	2.6232-001	-2.7685-001
6	0.0000	7.6743-004	-1.8740-005	3.9958-003	6.7442-005	5.6233-004	-3.2200-003	1.4860-002	5.698-003	-2.2855-002
7	0.0000	1.0000+000	1.0000+000	-1.4410-001	7.742-003	5.8455-002	1.5999-002	8.1128-002	1.983-001	-1.8315-001
8	0.0000	2.6444-003	2.5141-003	9.1583-003	5.2866-004	-2.4011-003	1.2521-002	-1.1748-001	-3.8888-001	1.1716+000
9	0.0000	2.1472-004	2.5141-003	2.2949-003	-4.7526-003	1.2098-002	-8.8581-005	-1.0584-001	-1.1327-001	1.1182+000
10	0.0000	-2.1637-004	-2.3356-002	6.1873-003	-2.2928-003	2.6973-002	-1.1623-002	-7.5071-001	-1.437-001	8.3687-001
11	0.0000	6.8233-005	1.0740-002	3.3431-001	5.7328-003	1.0000+000	-1.5405-001	1.2951-000	-5.201-002	9.0225-001
12	0.0000	9.0585-006	1.3968-003	4.1262-002	-7.0101-004	1.1811-001	-1.8644-002	1.1234-001	5.073-003	4.0387-002
13	0.0000	-8.1216-004	-2.7624-002	6.1509-004	3.2666-004	2.3985-001	-6.6501-003	-8.3488-001	-1.4982-001	7.7389-001
14	0.0000	-1.9332-002	1.3933-003	1.0000+000	-1.4443-002	9.2654-002	6.5151-001	1.2314+000	-1.5147-001	9.9340-001
15	0.0000	-7.6947-003	5.4222-004	3.7893-001	-5.3447-003	3.4022-002	2.4344-001	-4.0924-001	-2.618-002	1.7251-001
16	0.0000	-2.3270-003	2.5240-002	1.8643-001	-1.9003-003	-2.5571-002	3.5533-002	-2.0711-000	2.4134+000	1.6032+000
17	0.0000	5.1915-004	1.5131-004	-9.5626-004	3.1480-003	1.2831-002	4.9463-005	-5.9569-001	-2.1831-001	1.5184+000
18	0.0000	-1.5255-002	-6.6116-002	-7.5660-001	1.0000+000	-2.2733-001	1.0000+000	-2.3893+000	3.5538+000	1.0576+000

T-MATRIX

	11	12	13	14	15	16	17	18
1	-2.462-002	-1.8133-003	1.2405-001	1.9452-002	1.0000+000	6.2837-003	1.6671-001	3.1625-001
2	-1.2840-001	-2.7448-002	1.3800-001	1.0070-002	6.7854-001	6.0607-003	6.5797-002	2.0876-002
3	-1.7305+000	1.2598-002	-4.4968-002	-7.1111-002	3.6667-001	-2.5432-002	-2.6682-002	4.9698-001
4	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-6.5309-001
5	-1.0244+000	2.7742-002	1.2563-001	-7.5111-002	7.8288-001	2.4486-003	2.9238-002	3.5569-002
6	-1.1879-002	9.3634-005	4.1398-003	8.3513-003	-2.0822-002	6.2455-004	-2.5250-002	-4.5333-004
7	-8.7312-001	1.7556-002	7.7864-002	-7.5926-002	6.5374-001	9.0720-003	1.9155-002	5.4393-002
8	-3.9483-001	4.8755-003	6.2382-002	5.2400-003	6.791-001	6.660-005	9.6033-002	4.3401-001
9	-6.8944-001	8.0246-002	4.8733-002	1.5452-002	5.9799-001	-1.0088-001	7.9511-002	5.0684-001
10	-5.7455-001	6.6249-003	1.3467-001	-1.1774-001	9.8303-001	-4.7778-002	1.1557-001	5.9050-001
11	-1.2002-001	4.5546-003	3.1611-002	-7.5820-002	2.7311-001	-5.8632-002	7.0782-002	1.5371-002
12	-1.2355-002	-4.5740-004	1.0000+000	-7.9252-003	-4.3796-002	6.2300-003	-2.3564-002	1.1007-003
13	1.9007-001	-5.5447-003	2.2600-002	-3.8404-002	1.9462-001	-5.1447-002	6.4124-002	-3.1375-002
14	1.5664-001	7.2940-003	-6.4378-003	-7.4864-002	2.6463-001	-5.8187-002	7.4835-002	1.9134-002
15	-3.8373-002	-2.3937-003	-7.9663-003	-2.5166-002	-4.0095-001	-1.9801-002	1.0000+000	4.5396-003
16	-1.3554-001	-9.2811-002	-3.7189-002	8.8081-001	2.015-001	3.0883-001	4.7366-002	2.1830-001
17	-1.1525+000	1.0000+000	5.1150-002	-3.6388-001	6.8234-001	1.0000+000	8.5463-002	1.0000+000
18	-9.0006-001	2.3733-001	-2.3392-002	1.0000+000	2.4468-001	8.1743-001	-4.0295-003	3.1946-001

T INVERSE

1	2	3	4	5	6	7	8	9	10
1.679-002	4.7575-004	-1.2476-002	1.1595-002	4.2622-004	1.000+000	1.4313-004	9.3493-003	5.414-004	8.638-003
-2.2473-002	4.5358-001	-4.0742-002	-4.0742-002	-1.2112+000	0.0000	1.0031+000	-2.2798-001	-7.1603-003	1.1587-001
-2.8406-001	-1.5063-000	-6.9396-001	4.5707-002	1.1419+000	0.0000	-7.3153-003	1.3380+000	8.5881-002	-1.1025-001
-6.460-001	-2.5672-000	-1.5149+000	2.3359+000	-2.1601-001	0.0000	-5.7058-003	1.9779+000	2.0174-001	2.4453+000
-1.9533-000	-8.3005+000	-4.6849+000	6.4475+000	-3.7335-001	0.0000	3.0976-002	6.0385+000	9.0479-001	7.3550+000
6.2050-001	2.8211+000	1.4532+000	2.2326+000	9.4532-002	0.0000	8.4440+003	1.3176+000	-2.3298-001	-2.9228+000
1.2585+000	5.2491+000	2.8751+000	-4.4073+000	2.719-001	0.0000	3.6686-002	3.355+000	-4.0533-001	-5.1403+000
9.4710-001	-2.0329-001	4.0133-001	-4.4669-001	1.1900-002	0.0000	8.9850+003	-6.0317-001	-3.0009-002	-8.3233-001
1.8684+000	-6.0944-001	6.1103-001	-4.4522-001	6.3575-002	0.0000	2.1659+002	-2.8964+000	-8.2988-002	2.1464-001
7.9104-001	-9.9846-001	1.1107-001	2.6521-001	6.8157-003	0.0000	9.9067-003	-2.2723-001	-1.4419-002	-9.0465-003
4.1522-001	-3.3296-001	-5.5004+000	-2.4822-001	-5.1103-003	0.0000	8.6493-004	-6.0729-002	1.2284-002	4.3285-002
-7.7198+000	1.6506+000	-2.2276+000	1.1906+000	-1.2988-001	0.0000	-4.0753-002	3.7748-001	5.8843+000	-1.0718+000
-3.2272+000	2.5496-002	-3.0331-002	2.7561-002	1.4101-003	0.0000	4.2291+005	2.1730-002	1.4301-003	2.0305-002
-6.5006-002	1.1166+000	-1.2604+000	-3.3321-002	1.8697-001	0.0000	-5.7416-002	5.3778+000	2.4987+000	-3.0491+000
5.4943-001	3.9669-001	-1.0612-001	8.7444-002	1.6644-002	0.0000	-3.7228-003	5.6599-002	6.005-003	6.8991-002
1.4519-001	3.4758-001	-1.1329+000	5.8124-001	2.6501-002	0.0000	9.1756-003	2.7889+000	-4.9431+000	-5.5061-001
0.0000	0.0000	0.0000	-1.5335+000	7.9958-003	0.0000	-2.6641-004	6.4290-002	4.9741-003	7.0716-002
				0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

T INVERSE

1	2	3	4	5	6	7	8	9	10
-5.2686-004	-8.6920-003	6.7425-003	-1.8328-003	1.9722-002	-7.8115-004	-2.7327-005	1.1787-004		
1.4897-001	-2.2603-002	-2.3490-001	9.1824-003	8.4119-003	7.2418-003	1.1111-002	9.1068-003		
2.0930-002	-2.8214-003	-4.3747-001	-3.6562-003	-8.1013-003	6.3280-003	-2.0220-002	-7.3311-003		
1.0905+000	2.4080-002	-5.3874+000	2.0551-001	8.2156-003	4.3761-002	1.7025-002	3.5151-002		
2.5624+000	3.6798-003	-1.9226-001	-8.9395-001	6.8717-004	-1.1165+000	-4.2582-001	1.0763+000		
5.1328-001	-1.2233-002	2.8913+000	1.0703-001	1.6082-003	-8.7023-002	2.3217-002	-2.0028-002		
-1.5459+000	8.3197-003	7.9955+000	1.1900+000	-9.9062-003	-1.2928-001	3.7059-002	4.0203-002		
1.5411-002	1.6455-002	-1.4465-002	4.3007-002	-3.0973-003	-8.6841-002	4.8721-003	-6.0322-003		
-1.3133-001	2.9609-002	1.7331-001	1.0442-001	-1.0639-002	7.9857-002	-5.3882-003	-6.0334-003		
-1.1888-002	6.1701-002	4.5049+003	4.4884-002	-3.6255-002	3.2763-003	1.1211-004	-1.7583-003		
-1.6610-002	-3.2882-002	1.6163-002	5.4050-002	-6.2612-002	4.6498-002	3.0078-004	5.5073-003		
3.0227-001	-1.1250-001	-8.4336-002	-4.5055-002	-6.7713-002	-2.2081-001	5.2884-001	5.078-002		
-1.1941-001	9.8941-001	1.1008-002	-4.5551-003	1.7594-002	-1.8271-003	1.9421-006	3.1068-004		
4.5943-001	-9.6293-002	1.4561-001	3.2622-001	2.6360-002	5.3497-001	-9.3153-002	2.019-002		
8.3164-002	1.8641-001	4.2111-002	4.8937-002	-1.1787-001	-6.2073-003	3.4665-004	-1.2453-003		
-5.9719-002	5.1069-002	6.6817-002	7.5339-002	5.5842-002	2.9371-001	4.3662-001	-4.0101-002		
2.0212-002	-8.2639-002	4.8836-002	-3.5023-001	9.5849-001	-7.6710-003	8.3055-006	1.1773-003		
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		

F100 LINEAR MODEL 020K S2 1/5/76

*** THE MATRICES IN FINAL FORM ***

CASE 2

F-MATRIX

	SNEAN	SACCM	PT3	PT45	PT7M	TT25H	TT25C	TT3	TT4PHI	TT4PLC
SNEAN	-1.510+00	8.1643+001	-2.1093+000	1.1334+001	2.9951+000	-5.7839+001	-1.1721+001	-6.6334+002	2.2310+001	6.1351+002
SACCM	-2.5900+001	-1.1800+000	-1.1599+001	2.5122+000	-1.0859+000	9.3035+001	2.2299+002	-5.4882+002	1.7323+000	3.2918+001
PT3	4.5559+000	3.6915+000	-7.9970+000	4.2541+001	3.6730+000	2.8871+000	-7.5933+001	-5.0486+001	3.3246+001	-1.3040+001
PT45	1.2133+002	2.1242+002	3.5035+001	-1.6150+002	-1.0255+001	-1.7361+002	7.5943+000	6.2333+000	-1.0027+001	-9.9423+000
PT7M	1.0929+002	1.9280+001	5.9543+001	0.7368+002	-5.1300+002	-3.8871+001	2.7413+001	-6.5582+000	-5.0697+001	1.3114+001
TT25H	7.3333+000	-1.8446+000	1.0448+000	2.8440+001	8.6200+002	-1.8390+001	6.3241+001	8.9124+002	6.7660+002	8.9102+002
TT25C	2.8405+000	3.5878+000	2.4437+000	5.5808+001	1.6710+001	3.2301+000	-1.8790+001	1.8895+001	1.8000+001	1.7863+001
TT3	-0.7715+000	2.4207+000	-1.4847+000	5.1568+001	-5.7970+002	1.7974+001	-7.2567+001	-2.0110+001	-1.0637+001	-1.1019+001
TT4PHI	-0.2802+001	0.2648+002	0.9338+002	2.1334+002	0.0000	1.5410+001	-1.7779+002	3.8720+000	-5.0000+001	1.1856+003
TT4PLC	-1.7000+002	-5.4680+003	-5.0737+003	2.8444+003	0.0000	2.0620+002	-2.1790+003	5.1630+001	-6.6650+001	-6.6650+001
TT4	-0.2049+001	-1.0410+001	-7.9558+000	2.8423+001	-0.6745+001	2.6740+001	3.0213+000	2.0264+001	-0.9878+001	-5.1605+001
TT5H	-0.5778+001	-1.0513+002	-1.0513+002	-1.1136+001	1.0812+001	3.0580+001	2.6705+002	7.2623+000	-1.3585+001	-1.4524+000
TT5L	-0.3055+002	-9.4878+001	-5.7336+003	0.4841+000	4.3246+000	1.2260+001	8.0007+003	3.1651+000	-5.4333+000	-5.8074+001
TT5	-0.7339+001	-1.1527+000	4.1879+000	-5.3814+000	1.1134+000	4.4728+001	-9.4886+003	3.8512+000	-6.6110+000	-6.5803+001
TT6	-0.4033+002	3.1108+001	1.0441+001	-2.1599+002	8.5953+003	-2.4798+001	1.9829+001	1.8058+001	8.5978+003	8.5992+003
TT7	-1.7044+001	1.4295+001	0.8698+000	0.5135+001	9.1457+000	-9.6317+000	2.7374+000	3.1510+001	1.9380+000	9.5412+001

F-MATRIX

	TTU	TTUENT	TTUFLC	TT5	TT6	TT7M
SNEAN	-0.7627+001	1.2611+000	1.3347+001	-5.4105+002	2.5059+002	4.0712+002
SACCM	-0.0238+001	1.5444+000	1.4486+001	1.5466+001	1.4432+001	1.5358+001
PT3	-0.0909+000	-1.0787+001	-1.1596+001	2.2100+000	7.5818+001	-1.9333+001
PT45	2.6780+001	-9.9203+000	-1.0070+001	-9.7797+000	-8.3947+000	-9.6450+000
PT7M	1.8566+002	2.1174+001	2.0462+001	2.2530+001	2.1448+001	2.0450+001
TT25H	9.4287+002	8.6127+002	8.4203+002	9.6255+002	1.3509+001	8.9112+002
TT25C	1.9303+001	1.7842+001	1.4569+001	1.9303+001	2.7366+001	1.7858+001
TT3	-0.1328+001	-1.1020+001	-1.4070+001	-1.1260+001	-0.4310+001	-1.1026+001
TT4PHI	0.6008+001	1.1856+001	1.6500+003	-1.1651+003	-0.9246+003	1.1850+003
TT4PLC	5.1370+000	1.0220+000	1.0222+000	-1.4223+000	-0.1121+000	1.0222+000
TT4	-0.8430+001	-5.1607+001	-4.9571+001	-5.0466+001	-0.74959+001	-5.1902+001
TT5H	0.0973+001	-0.9800+001	6.8476+002	3.8210+002	3.9815+002	6.8481+002
TT5L	2.0314+001	-1.7473+001	-1.0720+000	-1.5482+002	1.6053+002	2.7510+002
TT5	2.0700+001	-3.1712+000	-3.1583+001	-1.9740+001	3.1173+002	4.8792+002
TT6	5.7133+002	2.5902+002	8.5967+003	1.1445+002	-1.9960+001	8.5987+003
TT7	-0.1804+000	0.8448+001	8.1680+001	3.6546+001	1.5770+001	-4.9150+001

FIG 00 LINEAR MODEL 070K 52 1/5/76

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-5.01201+0.021+J) 0.00000	0.00000	1.00000	1 (-5.99454-0.03)+J(0.00000) 2 (-2.03144-0.03)+J(0.00000) 3 (-7.42245-0.03)+J(0.00000) 4 (-3.01830-0.02)+J(0.00000) 5 (-1.00000+0.00)+J(0.00000) 6 (-4.99233-0.04)+J(0.00000) 7 (-2.69233-0.04)+J(0.00000) 8 (-2.26655-0.03)+J(0.00000) 9 (-5.43525-0.05)+J(0.00000) 10 (-7.18530-0.06)+J(0.00000) 11 (-5.17414-0.04)+J(0.00000) 12 (-2.32666-0.02)+J(0.00000) 13 (-9.25146-0.03)+J(0.00000) 14 (-2.10649-0.03)+J(0.00000) 15 (-5.54727-0.06)+J(0.00000) 16 (-2.02473-0.02)+J(0.00000)	- .0059945 - .0020314 - .0074225 - .0301834 1.0000000 - .0000649 - .0002662 - .0002367 - .0000544 - .0000072 - .0005174 - .0232666 - .0092514 - .0021065 - .0000055 - .0202473	.0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000
(-1.80994+0.021+J) 0.00000	0.00000	1.00000	1 (-1.75642-0.02)+J(0.00000) 2 (-4.34180-0.03)+J(0.00000) 3 (-2.41269-0.02)+J(0.00000) 4 (-7.16023-0.01)+J(0.00000) 5 (-1.00000+0.00)+J(0.00000) 6 (-7.60527-0.04)+J(0.00000) 7 (-2.72244-0.03)+J(0.00000) 8 (-2.32309-0.02)+J(0.00000) 9 (-5.49783-0.03)+J(0.00000) 10 (-7.15424-0.04)+J(0.00000) 11 (-1.40958-0.02)+J(0.00000) 12 (-1.30180-0.02)+J(0.00000) 13 (-5.12178-0.03)+J(0.00000) 14 (-2.06949-0.02)+J(0.00000) 15 (-4.25266-0.04)+J(0.00000) 16 (-7.90093-0.02)+J(0.00000)	- .0175642 - .004318 - .0241269 - .716023 1.0000000 - .0007406 - .0027269 - .0232309 - .0054978 - .0007154 - .0140958 - .0130180 - .0051218 - .0206949 - .0000253 - .0790093	.0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000

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(-5.43031+001)+J( 0.00000 ) 0.00000 1.00000
1 (-1.73632-002)+J( 0.00000 )
2 (-4.9243-003)+J( 0.00000 )
3 (-4.6584-003)+J( 0.00000 )
4 (-1.2296-001)+J( 0.00000 )
5 (-1.4965-001)+J( 0.00000 )
6 (-1.8899-003)+J( 0.00000 )
7 (-1.9950-003)+J( 0.00000 )
8 (-1.78278-002)+J( 0.00000 )
9 (-2.79501-001)+J( 0.00000 )
10 (-3.4657-002)+J( 0.00000 )
11 (-3.9184-002)+J( 0.00000 )
12 (-1.0000+000)+J( 0.00000 )
13 (-3.7236-001)+J( 0.00000 )
14 (-1.5719-001)+J( 0.00000 )
15 (-7.76185-004)+J( 0.00000 )
16 (-9.01071-001)+J( 0.00000 )
-0.173832
-0.092224
-0.06838
-0.122958
-0.149651
-0.018990
-0.019098
-0.178278
-0.275012
-0.334657
-0.391844
-1.000000
-3772341
-1577191
-907762
-9010711
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(-4.72615+001)+J( 0.00000 ) 0.75000+001 .99999
1 (-2.3108-002)+J( -8.6715-001 )
2 (-4.15459-003)+J( -1.5590-002 )
3 (-1.4777-002)+J( -4.4035-003 )
4 (-1.3241-001)+J( -1.0987-001 )
5 (-5.9422-002)+J( -1.1526-001 )
6 (-5.7082-004)+J( -6.0885-003 )
7 (-6.11410-003)+J( -6.8933-003 )
8 (-3.3498-002)+J( -2.7013-002 )
9 (-9.5512-002)+J( -2.2871-001 )
10 (-1.1033-002)+J( -5.2032-002 )
11 (-4.7601-002)+J( -1.3272-002 )
12 (-1.0000+000)+J( 0.00000 )
13 (-3.722-001)+J( -2.7926-003 )
14 (-6.8913-002)+J( -5.4615-002 )
15 (-5.5820-003)+J( -3.5132-003 )
16 (-1.9981-002)+J( -7.3070-001 )
-0.294653
-0.111399
-0.180516
-178220
-134626
-0.01153
-0.10472
-0.433061
-433060
-0.51905
-0.044945
-1.000000
-377323
-066766
-005500
-739830
-159.67476
-104.31647
-20.77220
-141.32225
-121.01008
-20.43342
-139.64820
-38.58904
-77.42678
-78.02605
-15.56171
-0.00000
-4.2817
-38.52635
-32.3464
-91.53632
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(-4.24824+001)+J( 0.00000 ) 0.00000 1.00000
1 (-2.4966-002)+J( 0.00000 )
2 (-4.0666-002)+J( 0.00000 )
3 (-1.9030-003)+J( 0.00000 )
4 (-4.7462-003)+J( 0.00000 )
5 (-7.5078-002)+J( 0.00000 )
6 (-1.1549-002)+J( 0.00000 )
7 (-9.6930-003)+J( 0.00000 )
8 (-1.8523-002)+J( 0.00000 )
9 (-1.0000+000)+J( 0.00000 )
10 (-1.1523-001)+J( 0.00000 )
11 (-1.4182-001)+J( 0.00000 )
12 (-6.0920-001)+J( 0.00000 )
13 (-2.2819-001)+J( 0.00000 )
14 (-8.7155-003)+J( 0.00000 )
15 (-8.5422-003)+J( 0.00000 )
16 (-1.5332-001)+J( 0.00000 )
-0.29966
-0.49666
-0.019047
-0.007466
-0.79078
-0.11549
-0.06693
-0.17523
-1.000000
-1.000000
-115233
-168416
-609203
-228165
-0.08716
-0.05412
-1534823
*00000
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	$(2.0 \times 10^3 + 0.1 \times 10^4 + 1.0 \times 10^5 + 2.0 \times 10^6)$	$100 \times 10^3 + 0.1 \times 10^4$	$100 \times 10^3 + 0.1 \times 10^4$
1	6.5012(-03)	1.4232(+002)	0.17487
2	7.9335(-03)	1.4553(+002)	0.20068
3	1.0160(-01)	1.4553(+002)	0.06023
4	1.7978(-01)	1.4553(+002)	0.41022
5	7.4271(-02)	1.4553(+002)	0.74830
6	5.5044(-03)	1.4553(+002)	0.03362
7	3.9779(-02)	1.4553(+002)	0.17346
8	6.4327(-02)	1.4545(+001)	0.10380
9	6.763(-02)	1.4030(+001)	0.11973
10	4.350(-03)	1.3530(+002)	0.26685
11	6.935(-02)	1.3530(+002)	0.35407
12	7.0946(-02)	1.2780(+001)	0.26742
13	1.7939(-02)	1.0120(+001)	0.15122
14	7.9775(-01)	1.6208(+001)	0.54552
15	3.9327(-02)	1.6208(+001)	0.35337
16	1.0000(+00)	1.0000(+00)	0.00000

[illegible]

	$(-1.915-3+0i)+j$	0.00000	0.00000	1.00000	
1	(9.74448-003)+j	0.00000			* 0057435
2	(1.58292-004)+j	0.00000			* 0001533
3	(-1.19375-011)+j	0.00000			* 19479
4	(-1.9342-011)+j	0.00000			* 194246
5	(-1.25373-011)+j	0.00000			* 125373
6	(5.4257-002)+j	0.00000			* 54257
7	(-1.54379-02)+j	0.00000			* 153379
8	(-2.1446-02)+j	0.00000			* 21446
9	(2.4335-02)+j	0.00000			* 24335
10	(2.4600-03)+j	0.00000			* 24600
11	(1.7506-02)+j	0.00000			* 17506
12	(3.7642-02)+j	0.00000			* 37642
13	(1.5450-02)+j	0.00000			* 15450
14	(1.0000-00)+j	0.00000			* 100000
15	(-3.7658-01)+j	0.00000			* 37658
16	(5.3521-01)+j	0.00000			* 53521

(-1.3-543+000)+JC	0.00000	0.00000	1.00000	1	(-1.32259-002)+JC	0.00000)	-0.13259	0.0000
(-5.3654-002)+JC	0.00000	0.00000	0.00000	2	(-5.3654-002)+JC	0.00000)	-0.52854	0.0000
(-8.5189-002)+JC	0.00000	0.00000	0.00000	3	(-8.5189-002)+JC	0.00000)	-0.85189	0.0000
(-1.5954-001)+JC	0.00000	0.00000	0.00000	4	(-1.5954-001)+JC	0.00000)	-1.59549	0.0000
(-1.1483-001)+JC	0.00000	0.00000	0.00000	5	(-1.1483-001)+JC	0.00000)	-1.14824	0.0000
(-3.3185-003)+JC	0.00000	0.00000	0.00000	6	(-3.3185-003)+JC	0.00000)	-0.04916	0.0000
(-1.2760-003)+JC	0.00000	0.00000	0.00000	7	(-1.2760-003)+JC	0.00000)	-0.01263	0.0000
(-5.3022-002)+JC	0.00000	0.00000	0.00000	8	(-5.3022-002)+JC	0.00000)	-0.53022	0.0000
(-1.4046-002)+JC	0.00000	0.00000	0.00000	9	(-1.4046-002)+JC	0.00000)	-0.14040	0.0000
(-4.3481-003)+JC	0.00000	0.00000	0.00000	10	(-4.3481-003)+JC	0.00000)	-0.04348	0.0000
(-1.9004-002)+JC	0.00000	0.00000	0.00000	11	(-1.9004-002)+JC	0.00000)	-0.19046	0.0000
(-2.7248-002)+JC	0.00000	0.00000	0.00000	12	(-2.7248-002)+JC	0.00000)	-0.27288	0.0000
(-1.0000-000)+JC	0.00000	0.00000	0.00000	13	(-1.0000-000)+JC	0.00000)	1.0000000	0.0000
(-1.2226-002)+JC	0.00000	0.00000	0.00000	14	(-1.2226-002)+JC	0.00000)	-0.12229	0.0000
(-2.6794-003)+JC	0.00000	0.00000	0.00000	15	(-2.6794-003)+JC	0.00000)	-0.02679	0.0000
(-1.3570-002)+JC	0.00000	0.00000	0.00000	16	(-1.3570-002)+JC	0.00000)	-0.13550	0.0000

(-7.15714-001)+JC	0.00000	0.00000	1.00000	1	(-7.15714-001)+JC	0.00000)	-0.105628	0.0000
(-1.1681-001)+JC	0.00000	0.00000	0.00000	2	(-1.1681-001)+JC	0.00000)	-0.116808	0.0000
(-8.7681-002)+JC	0.00000	0.00000	0.00000	3	(-8.7681-002)+JC	0.00000)	-0.87681	0.0000
(-1.5921-001)+JC	0.00000	0.00000	0.00000	4	(-1.5921-001)+JC	0.00000)	-1.59204	0.0000
(-4.7210-002)+JC	0.00000	0.00000	0.00000	5	(-4.7210-002)+JC	0.00000)	-0.47210	0.0000
(-2.6552-002)+JC	0.00000	0.00000	0.00000	6	(-2.6552-002)+JC	0.00000)	-0.26552	0.0000
(-2.5971-002)+JC	0.00000	0.00000	0.00000	7	(-2.5971-002)+JC	0.00000)	-0.25977	0.0000
(-1.0000-000)+JC	0.00000	0.00000	0.00000	8	(-1.0000-000)+JC	0.00000)	-0.85751	0.0000
(-7.70621-002)+JC	0.00000	0.00000	0.00000	9	(-7.70621-002)+JC	0.00000)	-0.97621	0.0000
(-1.2237-001)+JC	0.00000	0.00000	0.00000	10	(-1.2237-001)+JC	0.00000)	-1.22366	0.0000
(-1.6394-001)+JC	0.00000	0.00000	0.00000	11	(-1.6394-001)+JC	0.00000)	-1.63944	0.0000
(-5.129-001)+JC	0.00000	0.00000	0.00000	12	(-5.129-001)+JC	0.00000)	-1.51293	0.0000
(-2.9404-002)+JC	0.00000	0.00000	0.00000	13	(-2.9404-002)+JC	0.00000)	-0.294096	0.0000
(-5.65013-002)+JC	0.00000	0.00000	0.00000	14	(-5.65013-002)+JC	0.00000)	-0.56013	0.0000

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*** THE VALUES IN FINAL FORM ***

CASE 3

E-MATRIX

	SPAN	SACCM	PT2V	PT3	PT4E	TT25H	TT25C	TT3	TT4PI	TT4PLQ
SPAN	-1.0020+000	1.0495+000	-2.0000+000	-0.8331+002	2.8070+000	-1.0874+000	-2.8541+001	-1.3887+001	6.3830+002	-0.2330+002
SPAN	-2.0000+000	-3.2420+000	-2.0000+000	1.2276+000	-0.7532+001	1.3555+000	-7.0857+002	-1.3887+001	7.6322+001	4.2895+002
SPAN	-2.0000+000	-5.0000+000	-1.0000+000	9.2097+001	-0.0047+000	1.0808+000	2.0020+002	1.1046+001	7.0448+001	3.6638+001
PT2V	0.0000+000	0.0000+000	0.0000+000	1.3020+002	3.0912+000	-2.7181+000	1.8334+001	2.1457+001	4.5916+000	4.7782+000
PT2V	1.0000+000	0.0000+000	2.0000+000	3.5971+002	-0.7100+000	-7.0857+002	-1.2392+001	3.0489+001	-1.7382+001	-2.0820+001
PT2V	2.0000+000	0.0000+000	0.0000+000	0.0000+000	1.2588+001	-1.0808+000	8.0170+001	3.2588+001	1.9375+001	2.0820+001
PT2V	3.0000+000	0.0000+000	0.0000+000	0.0000+000	1.6722+001	4.0804+000	-1.0860+001	3.0043+001	2.8055+001	2.0820+001
PT2V	4.0000+000	0.0000+000	0.0000+000	0.0000+000	1.7522+001	1.9651+001	-5.1644+001	-2.0040+001	-2.8888+001	-1.2663+001
PT2V	5.0000+000	0.0000+000	0.0000+000	0.0000+000	-0.0511+003	1.3200+001	-9.0628+003	3.9273+001	-0.0000+000	-1.6100+003
PT2V	6.0000+000	0.0000+000	0.0000+000	1.3823+003	-0.6630+004	1.7585+002	-1.0594+003	5.2640+001	-0.0000+000	-0.6650+001
PT2V	7.0000+000	0.0000+000	0.0000+000	2.7740+000	-0.0372+001	4.0633+001	-2.0489+000	2.3015+001	-0.0000+000	-0.7042+001
PT2V	8.0000+000	0.0000+000	0.0000+000	1.2205+001	1.1411+001	-8.2701+001	5.1443+002	6.1085+000	-1.3612+001	-1.9991+000
PT2V	9.0000+000	0.0000+000	0.0000+000	0.0000+000	4.5645+000	-3.3111+001	2.3545+002	3.2334+000	-1.4472+000	-5.9934+001
PT2V	1.0000+000	0.0000+000	0.0000+000	0.0000+000	1.1663+000	1.0273+001	-2.3556+002	3.6886+000	-0.1764+000	-0.9770+001
PT2V	2.0000+000	0.0000+000	0.0000+000	0.0000+000	3.3332+003	-2.0499+001	1.0662+001	1.3666+001	6.3334+003	6.3323+003
PT2V	3.0000+000	0.0000+000	0.0000+000	0.0000+000	1.1663+001	-1.1663+001	2.0771+000	1.9694+001	1.7702+000	6.1556+001

E-MATRIX

	TT4SH	TT4SLQ	TT5	TT6C	TT7M
TT4SH	7.1013+001	2.1011+002	7.0220+002	-1.3318+001	-4.3830+002
TT4SH	-2.0000+000	-2.0000+000	-2.1064+002	-1.2407+002	-2.0405+002
TT4SH	0.0000+000	0.0000+000	0.0000+000	1.0842+000	3.2474+001
TT4SH	0.0000+000	0.0000+000	0.0000+000	6.7017+000	4.2257+000
TT4SH	1.0000+000	1.0000+000	1.1264+001	-9.3355+000	-1.3411+001
TT4SH	2.0000+000	2.0000+000	1.7588+001	3.0314+001	2.0868+001
TT4SH	3.0000+000	3.0000+000	2.0000+000	4.3649+001	3.0264+001
TT4SH	4.0000+000	4.0000+000	1.1527+001	-2.0046+001	-1.3760+001
TT4SH	5.0000+000	5.0000+000	0.0000+000	3.2200+003	-1.6103+003
TT4SH	6.0000+000	6.0000+000	5.7077+004	-1.8644+000	-1.9322+004
TT4SH	7.0000+000	7.0000+000	5.9431+001	-1.0324+000	-7.0724+001
TT4SH	8.0000+000	8.0000+000	-2.1527+003	1.2957+002	6.4781+003
TT4SH	9.0000+000	9.0000+000	-1.5550+003	0.0000+000	2.3321+003
TT4SH	1.0000+000	1.0000+000	1.9970+001	5.4502+002	-1.7299+003
TT4SH	2.0000+000	2.0000+000	1.1667+002	-1.1667+002	6.3326+003
TT4SH	3.0000+000	3.0000+000	1.3217+001	1.8619+001	-4.9310+001

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G-MATRIX

	MEMPH	AMTX	CIVV	RCVV	BLC
SFAN	3.4480-001	-1.0500-002	4.523-002	-2.7537-002	-3.6047-001
SFCV	-6.1680-003	-2.6429-002	8.8433-003	1.1030-001	2.2567-001
PTW	-1.4156-000	4.5944-000	-1.3231-001	1.1578-001	1.9268-000
PT3	-1.5814-001	1.9009-000	-2.0750-000	-1.0518-001	-1.1464-002
PT5	5.7686-001	-5.6714-000	-1.3877-001	-1.4543-000	-4.1189-001
TT25H	-1.6889-000	3.7419-002	-5.6877-003	4.5063-002	1.2941-000
TT25C	-1.9520-000	1.0474-001	-5.0423-002	1.2565-001	1.4401-000
TT3	1.2154-000	1.0308-001	7.5519-002	-2.0615-001	-2.1698-000
TT4PHI	9.0953-002	-3.7663-001	1.6577-003	4.8436-003	-2.2459-000
TT4ELO	1.2455-002	-5.1274-000	1.3684-000	4.1887-004	-2.9869-001
TT4	2.2116-001	-3.4215-001	3.5096-001	1.7356-000	2.2243-001
TT4ST	2.4669-001	-2.8201-001	6.3431-003	-4.9042-002	-3.6797-000
TT4SLO	1.6815-001	-1.0121-001	-2.5599-003	-1.0513-002	-1.4732-000
TT5	1.2570-001	-1.7204-002	-1.1629-002	-2.5134-002	-1.4853-000
TT6C	-4.9251-002	-2.1607-001	2.1044-003	-1.2361-002	5.9806-002
TT7	-2.6230-000	3.1484-001	4.2593-001	-6.6461-001	4.0382-000

H-MATRIX

	SFAN	SFCV	PTW	PT3	TT25H	TT25C	TT3	TT4PHI	TT4SLO
FMV	5.7070-001	-1.5946-000	2.0853-000	1.2084-001	8.1175-001	-2.1101-002	-6.3457-002	6.8862-002	1.3063-003
MFAN	9.5875-001	2.7127-001	-1.6836-001	-2.6624-002	-2.0298-001	-5.2779-002	-1.4406-002	-1.3370-002	-1.013-002
TT4	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
SWAF	2.2106-000	1.0059-001	-5.7824-000	-3.2713-001	-2.7900-001	-7.0718-000	-1.8394-000	-5.0410-001	-4.8816-001
SMC	2.2414-000	3.1200-001	1.2494-000	-5.1382-000	9.1172-002	-1.6189-001	6.0066-001	1.6545-001	1.5964-001

H-MATRIX

	TT4	TT25H	TT4SLO	TT5	TT6C	TT7
FMV	-3.5751-001	-1.2619-002	-1.1459-002	1.0644-001	1.4627-001	-8.7263-003
MFAN	-1.6767-002	-1.0004-003	-1.4003-002	-1.1782-002	-2.0591-002	-1.0340-002
TT4	1.0000-000	0.0000	0.0000	0.0000	0.0000	0.0000
SWAF	-5.8490-001	-4.5100-001	-4.8924-001	-4.1068-001	-7.1667-001	-4.8925-001
SMC	1.0119-001	1.0055-001	1.5965-001	1.3503-001	2.3506-001	1.5995-001

G-MATRIX

	MEMPH	AMTX	CIVV	RCVV	BLC
FMV	5.1741-002	-2.7787-002	-2.3274-002	3.3847-002	-5.6173-002
MFAN	4.7214-002	-3.2648-001	-3.5785-002	-3.7877-003	-7.9740-002
TT4	0.0000	0.0000	0.0000	0.0000	0.0000
SWAF	2.0943-000	1.1227-001	7.6716-001	-5.0302-001	3.7231-000
SMC	-3.5763-001	1.1092-001	-7.8432-002	6.9091-001	3.3595-001

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EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-6.739e+002)+j(0.00000)	0.00000	1.00000	1 (-4.16827-003)+j(0.00000)	-.0041893	.00000
			2 (1.01187-003)+j(0.00000)	.0010119	.00000
			3 (-4.08339-003)+j(0.00000)	-.0060864	.00000
			4 (-5.22647-003)+j(0.00000)	-.0052255	.00000
			5 (1.00000+000)+j(0.00000)	1.0000000	.00000
			6 (-1.26565-004)+j(0.00000)	-.0001270	.00000
			7 (-1.66517-004)+j(0.00000)	-.0001669	.00000
			8 (1.27710-004)+j(0.00000)	.0001277	.00000
			9 (-3.20189-005)+j(0.00000)	-.0003200	.00000
			10 (-4.39556-004)+j(0.00000)	-.0000044	.00000
			11 (-5.93273-004)+j(0.00000)	-.0005933	.00000
			12 (-1.84455-002)+j(0.00000)	-.0184455	.00000
			13 (-7.34931-003)+j(0.00000)	-.0073492	.00000
			14 (-1.87551-003)+j(0.00000)	-.0016745	.00000
			15 (-1.36536-007)+j(0.00000)	.0000001	.00000
			16 (-1.86358-002)+j(0.00000)	-.0186358	.00000
(-1.3453e+002)+j(0.00000)	0.00000	1.00000	1 (-1.46473-002)+j(0.00000)	-.0146473	.00000
			2 (-4.42525-003)+j(0.00000)	-.0044253	.00000
			3 (-3.09851-002)+j(0.00000)	-.0309851	.00000
			4 (1.00000+000)+j(0.00000)	1.0000000	.00000
			5 (-4.44554-001)+j(0.00000)	.6445544	.00000
			6 (-3.27685-003)+j(0.00000)	-.0032769	.00000
			7 (-5.18832-003)+j(0.00000)	-.0051833	.00000
			8 (-4.01960-002)+j(0.00000)	-.0401960	.00000
			9 (-1.66237-002)+j(0.00000)	-.0166237	.00000
			10 (-2.14360-003)+j(0.00000)	-.0021436	.00000
			11 (-2.72332-002)+j(0.00000)	-.0272332	.00000
			12 (-8.30535-002)+j(0.00000)	-.0830535	.00000
			13 (-3.24923-002)+j(0.00000)	-.0324923	.00000
			14 (-5.26622-002)+j(0.00000)	-.0526622	.00000
			15 (-1.06255-003)+j(0.00000)	-.0010665	.00000
			16 (-1.17559-001)+j(0.00000)	-.1175593	.00000

(-5.0687+001)+JC 7.16237+000	5.11724+001	.00016	1	(-1.5024+002)+JC (-4.64373+003)	.0157428	-162.84399
			2	(-0.78416+003)+JC 5.44683+003	.0072522	131.31778
			3	(1.8734+002)+JC 9.0628+003	.026647	154.5517
			4	(6.30217+002)+JC (-2.36447+003)	.0673911	-20.72146
			5	(-6.31335+003)+JC 4.97111+003	.0501112	97.24467
			6	(-7.05715+003)+JC 4.33576+003	.0082827	148.41434
			7	(-1.10895+002)+JC 6.22221+003	.0168896	150.63803
			8	(-1.82507+003)+JC (-2.0997+003)	.0010231	-127.13658
			9	(1.89601+001)+JC (-3.07724+003)	.3614452	-58.36119
			10	(2.26349+002)+JC (-3.7859+003)	.0441059	-19.12311
			11	(4.5327+002)+JC 3.41715+003	.0567657	37.01906
			12	(1.00000+000)+JC 0.00000	1.0000000	.00000
			13	(3.75339+001)+JC (-3.56270+003)	.3759560	-54.294
			14	(9.67634+002)+JC (-7.78355+003)	.1241367	-38.83020
			15	(7.24356+003)+JC (-2.1648+003)	.005687	-16.5531
			16	(-0.67103+001)+JC (-5.42017+003)	.715195	-130.75434

(-5.3254+001)+JC 0.00000	0.00000	1.00000	1	(1.25624+002)+JC 0.00000	.0135624	.00000
			2	(2.57302+003)+JC 0.00000	.0025730	.00000
			3	(6.32466+003)+JC 0.00000	.0063247	.00000
			4	(2.84700+003)+JC 0.00000	.0028470	.00000
			5	(3.33244+002)+JC 0.00000	.033244	.00000
			6	(1.33078+003)+JC 0.00000	.0013308	.00000
			7	(2.47430+003)+JC 0.00000	.0024743	.00000
			8	(1.4653+003)+JC 0.00000	.0014255	.00000
			9	(-1.43840+001)+JC 0.00000	.143840	.00000
			10	(-1.76180+002)+JC 0.00000	.0176180	.00000
			11	(1.03559+002)+JC 0.00000	.0103059	.00000
			12	(2.59778+001)+JC 0.00000	.8997784	.00000
			13	(-3.3603+001)+JC 0.00000	.336034	.00000
			14	(-5.2181+002)+JC 0.00000	.052181	.00000
			15	(-1.29177+003)+JC 0.00000	.0012918	.00000
			16	(1.00000+000)+JC 0.00000	1.0000000	.00000

(-0.2486+001)+JC 0.00000	0.00000	1.00000	1	(1.7348+002)+JC 0.00000	.0173248	.00000
			2	(1.92840+002)+JC 0.00000	.0192840	.00000
			3	(4.64130+003)+JC 0.00000	.046413	.00000
			4	(1.15420+002)+JC 0.00000	.0115420	.00000
			5	(-6.90478+002)+JC 0.00000	.0690478	.00000
			6	(-7.39708+003)+JC 0.00000	.073971	.00000
			7	(-1.1073+002)+JC 0.00000	.0110773	.00000
			8	(3.25624+003)+JC 0.00000	.0032592	.00000
			9	(1.00000+000)+JC 0.00000	1.0000000	.00000
			10	(1.14224+001)+JC 0.00000	.114224	.00000
			11	(1.4221+001)+JC 0.00000	.142214	.00000
			12	(-5.25899+001)+JC 0.00000	.625899	.00000
			13	(-2.3302+001)+JC 0.00000	.233024	.00000
			14	(-2.4886+002)+JC 0.00000	.024886	.00000
			15	(9.89535+003)+JC 0.00000	.0089535	.00000
			16	(3.1720+002)+JC 0.00000	.0317220	.00000

(-1.0375+001)+J(4.00175+000)	1.07280+001	.97034	1	(-2.06813+002)+J(-1.1067+002)	.0236184	-151.12119
(-1.0618+002)+J(-1.3180+002)			2	(-1.0618+002)+J(-1.3180+002)	.0169317	-128.80315
(-2.3205+001)+J(-2.31765+001)			3	(-2.3205+001)+J(-2.31765+001)	.3279665	-135.05226
(1.06856+001)+J(-1.46889+001)			4	(1.06856+001)+J(-1.46889+001)	.1766678	-52.76266
(-6.62463+002)+J(-1.73837+001)			5	(-6.62463+002)+J(-1.73837+001)	.1803315	-110.84103
(-0.76148+002)+J(4.61337+002)			6	(-0.76148+002)+J(4.61337+002)	.0644023	136.03517
(-4.44600+002)+J(5.50060+002)			7	(-4.44600+002)+J(5.50060+002)	.0720142	130.19773
(1.15491+001)+J(9.19752+002)			8	(1.15491+001)+J(9.19752+002)	.1476401	38.53325
(1.99404+001)+J(2.82462+001)			9	(1.99404+001)+J(2.82462+001)	.3457554	54.77369
(2.24885+002)+J(2.86444+002)			10	(2.24885+002)+J(2.86444+002)	.0359581	51.30415
(9.23586+002)+J(1.97243+001)			11	(9.23586+002)+J(1.97243+001)	.224071	63.49610
(1.05313+001)+J(2.65968+001)			12	(1.05313+001)+J(2.65968+001)	.2669889	68.47194
(3.93476+002)+J(8.78881+002)			13	(3.93476+002)+J(8.78881+002)	.0942292	65.8154
(7.88730+001)+J(7.93905+002)			14	(7.88730+001)+J(7.93905+002)	.7927157	5.79781
(2.30979+001)+J(2.58650+001)			15	(2.30979+001)+J(2.58650+001)	.3467723	48.23462
(1.00000+000)+J(0.00000)			16	(1.00000+000)+J(0.00000)	1.0000000	.00000
(-4.5548+000)+J(2.43750+001)	4.29175+000	.99876	1	(1.00000+000)+J(0.00000)	1.0000000	.00000
(-3.61827+002)+J(2.21191+003)			2	(-3.61827+002)+J(2.21191+003)	.0322502	176.50177
(7.75331+001)+J(-5.3170+002)			3	(7.75331+001)+J(-5.3170+002)	.7773216	-4.00052
(-5.43556+002)+J(2.1106+002)			4	(-5.43556+002)+J(2.1106+002)	.0583111	156.77481
(1.44719+001)+J(2.31851+003)			5	(1.44719+001)+J(2.31851+003)	.147372	.91785
(5.16146+001)+J(-3.35027+002)			6	(5.16146+001)+J(-3.35027+002)	.5172317	-3.71582
(6.79557+001)+J(-4.75742+002)			7	(6.79557+001)+J(-4.75742+002)	.6812199	-4.00461
(3.73774+001)+J(-3.20467+002)			8	(3.73774+001)+J(-3.20467+002)	.3751454	-4.90245
(1.47646+001)+J(4.2005+002)			9	(1.47646+001)+J(4.2005+002)	.3762944	-6.89953
(-1.33749+003)+J(-2.7526+003)			10	(-1.33749+003)+J(-2.7526+003)	.001589	-19.18369
(3.26742+001)+J(-1.87116+002)			11	(3.26742+001)+J(-1.87116+002)	.3310032	-6.71324
(4.52524+001)+J(-5.20360+002)			12	(4.52524+001)+J(-5.20360+002)	.4555028	-6.5216
(-5.39518+003)+J(-1.5029+002)			13	(-5.39518+003)+J(-1.5029+002)	.0160389	-109.3165
(7.19731+001)+J(-8.70554+002)			14	(7.19731+001)+J(-8.70554+002)	.7249770	-6.26673
(8.83336+001)+J(-7.70701+002)			15	(8.83336+001)+J(-7.70701+002)	.8916727	-4.95844
(5.67107+001)+J(-4.12433+002)			16	(5.67107+001)+J(-4.12433+002)	.5744001	-9.14013
(-1.84233+001)+J(0.00000)		1.00000	1	(-1.84233+001)+J(0.00000)	.1842327	.00000
(-8.26186+003)+J(0.00000)			2	(-8.26186+003)+J(0.00000)	.0082619	.00000
(-4.3702+002)+J(0.00000)			3	(-4.3702+002)+J(0.00000)	.0437025	.00000
(-5.04520+002)+J(0.00000)			4	(-5.04520+002)+J(0.00000)	.054520	.00000
(-6.16576+002)+J(0.00000)			5	(-6.16576+002)+J(0.00000)	.0616576	.00000
(-2.41534+002)+J(0.00000)			6	(-2.41534+002)+J(0.00000)	.0241534	.00000
(-2.90114+002)+J(0.00000)			7	(-2.90114+002)+J(0.00000)	.0290119	.00000
(-2.04455+002)+J(0.00000)			8	(-2.04455+002)+J(0.00000)	.026455	.00000
(-2.8311+003)+J(0.00000)			9	(-2.8311+003)+J(0.00000)	.008321	.00000
(-2.96081+003)+J(0.00000)			10	(-2.96081+003)+J(0.00000)	.0029608	.00000
(1.19934+002)+J(0.00000)			11	(1.19934+002)+J(0.00000)	.0119934	.00000
(6.97674+003)+J(0.00000)			12	(6.97674+003)+J(0.00000)	.009767	.00000
(1.00000+000)+J(0.00000)			13	(1.00000+000)+J(0.00000)	1.0000000	.00000
(-5.89812+003)+J(0.00000)			14	(-5.89812+003)+J(0.00000)	.005898	.00000
(-3.12201+002)+J(0.00000)			15	(-3.12201+002)+J(0.00000)	.0312201	.00000
(-2.84090+002)+J(0.00000)			16	(-2.84090+002)+J(0.00000)	.0284090	.00000

*** THE MATRICES IN FINAL FORM ***

CASE 4

F-MATRIX

SNFAN	SNCOM	PT7M	WFCOM	PT3	FIIT	PT45	TT25H	TT25C	TT3
-1.0017+000	1.9701+000	-2.8997+000	3.4400+001	-4.5429+002	0.0000	2.8070+000	-1.4688+000	-2.8533+001	-1.7382+001
-2.0737+001	-3.2628+000	-2.1994+001	-4.9933+003	1.2477+000	0.0000	-6.7551+001	1.3571+000	-7.4966+002	-8.9381+002
2.0818+000	-5.6875+000	-1.5702+001	-1.4087+000	9.2671+001	0.0000	4.0492+000	4.0903+000	2.1383+002	4.0613+001
0.0000	0.0000	0.0000	-1.0000+001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
6.5249+001	4.7440+002	4.8003+001	-1.5720+001	-1.3019+002	0.0000	3.0842+000	-2.7168+002	1.5926+001	2.5209+001
0.0000	0.0000	0.0000	0.0000	0.0000	-2.5000+001	0.0000	0.0000	0.0000	0.0000
1.8462+001	4.3741+001	2.2235+002	5.7308+001	3.5947+002	0.0000	-6.7137+002	-7.5402+001	-1.2356+001	-5.0683+001
2.0702+000	-3.0246+000	2.5417+000	-1.0850+000	4.0454+001	0.0000	1.2536+001	-1.6884+001	8.0134+001	3.8147+001
2.4232+000	-7.1520+000	3.5013+000	-1.4445+000	6.1597+001	0.0000	1.6651+001	4.8922+000	-1.8881+001	5.3913+001
-2.2312+000	-4.9953+000	-1.6331+000	1.2125+000	4.1598+000	0.0000	-7.7325+002	1.9647+001	-5.1820+001	-2.0247+001
3.0585+002	-6.7591+002	-2.5754+002	9.4923+002	9.6609+003	0.0000	-8.0088+003	1.3200+001	-9.6600+003	3.9261+000
-1.1335+001	-7.0459+001	-8.3020+001	2.2103+001	2.7728+000	0.0000	-4.0270+001	4.8614+001	-2.6377+000	2.2462+001
2.1646+001	-8.0041+001	1.6114+001	2.3670+001	-1.2208+001	0.0000	1.1413+001	-8.4655+001	5.8750+002	6.9316+000
8.4037+002	-3.2086+001	6.4840+002	9.6950+002	-4.8853+000	0.0000	4.5644+000	-3.4695+001	2.3587+002	2.7728+000
5.5221+002	-8.6592+001	3.7834+000	1.1288+001	-5.5011+000	0.0000	1.1673+000	1.2460+001	-2.2160+002	3.1148+000
-4.1710+002	5.2494+001	8.1636+001	-4.4095+002	-1.1640+002	0.0000	3.3211+003	-2.8975+001	1.9862+001	1.4320+001
-1.0861+001	2.7475+001	2.2062+000	-2.6077+000	5.1879+001	0.0000	1.1663+001	-1.5226+001	2.0757+000	8.3930+001

F-MATRIX

TT4PHI	TT4	TT4SHI	TT4SLO	TT5	TT6C	TT7M
4.0867+001	-1.5582+000	7.1414+001	2.4425+002	-7.0186+002	-1.3315+001	-6.3816+002
1.9733+001	-2.2622+001	-2.4971+002	-2.4482+002	-2.1518+002	-3.2484+002	-2.4478+002
-2.4572+000	2.1027+000	3.5582+001	3.4553+001	1.8715+000	1.0830+000	3.2963+001
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
-3.4801+001	8.4985+001	4.6239+000	4.8236+000	4.2126+000	6.5990+000	4.8244+000
0.0000	0.0000	1.3004+001	1.4449+002	0.0000	0.0000	0.0000
1.1024+002	-5.3704+001	-1.4085+001	-1.3742+001	-1.1186+001	-9.3238+000	-1.3405+001
-1.4841+000	2.1701+000	2.0859+001	2.0865+001	1.7540+001	3.0301+001	2.0862+001
-2.1512+000	3.4466+000	3.0233+001	3.0240+001	2.4893+001	4.3632+001	3.0255+001
1.1004+000	-1.4206+000	-1.3762+001	-1.3758+001	-1.1515+001	-2.0052+001	-1.3756+001
-4.9996+001	4.5994+001	-1.4094+003	-1.6095+003	-4.8290+003	-3.2193+003	-1.6099+003
5.6644+000	-5.4449+001	7.0814+001	-1.0685+001	-5.9370+001	-1.0324+000	7.0704+001
-1.2475+001	4.3324+001	-4.9970+001	6.9121+003	-6.5671+004	1.3825+002	6.9125+003
-5.64726+002	1.8937+001	-1.7911+001	-1.9978+000	-1.0333+003	3.4726+004	2.5058+003
1.2919+002	2.1302+001	-1.9638+001	-2.2608+001	-1.0966+001	5.4900+002	-1.5306+003
-4.6636+002	1.4447+001	1.1653+002	8.3393+003	-1.1660+002	-1.9990+001	8.3301+003
-5.5677+000	3.4412+000	7.0446+001	6.9581+001	3.3218+001	1.8619+001	-4.9310+001

G-MATRIX

	WFBH	AMIX	CIVV	RCVV	BLC
SNEAN	0.0000	-1.0466+002	4.5253+002	-2.7581+002	-3.4322+001
SNCOM	0.0000	-2.3477+002	8.6563+003	1.1036+001	1.9750+001
PTM	0.0000	-4.5967+000	-1.3224+001	1.1612+001	1.7657+000
WFCOM	1.0000+001	0.0000	0.0000	0.0000	0.0000
PT3	0.0000	1.0013+000	-2.0740+000	-1.0513+001	-1.1678+002
PT45	0.0000	0.0000	0.0000	0.0000	0.0000
PT5	0.0000	-5.5554+000	-1.4306+001	-1.4737+000	-3.1437+001
TT25H	0.0000	3.2259+002	-5.5008+003	4.5256+002	1.2008+000
TT25C	0.0000	1.0651+001	-5.0363+002	1.2535+001	1.3091+000
TT3	0.0000	1.0059+001	7.5521+002	-2.0626+001	-2.1086+000
TT6H	0.0000	-3.7791+003	1.0373+003	4.8423+003	-2.2452+000
TT6	0.0000	-3.3141+001	3.5082+001	1.7339+000	2.2579+001
TT45	0.0000	-1.4675+003	-6.7056+003	-5.0453+002	-3.0083+000
TT45C	0.0000	-5.5133+004	-2.419+003	-2.0091+002	-1.2048+000
TT5	0.0000	-1.4676+002	-1.1770+002	-2.5772+002	-1.1773+000
TT6C	0.0000	-2.1671+003	2.1081+003	-1.2334+002	5.6072+002
TT7M	0.0000	3.1421+001	4.2609+001	-5.6385+001	3.6727+000

H-MATRIX

	SNEAN	SNCOM	PTM	WFCOM	PT3	PT45	TT25H	TT25C	TT3
FMX	5.7062+001	-1.1988+000	2.0893+000	5.1756+002	1.2085+001	8.0503+001	8.1179+001	-8.1103+002	-6.2431+002
WFAN	0.4588+001	2.7205+001	-1.6831+001	6.6932+002	-2.6652+002	-7.9651+003	-2.0335+001	-5.2755+002	-2.5410+002
TT4	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
SMAF	2.2136+000	1.0045+001	-5.7959+000	2.4851+000	-9.2831+001	-2.7830+001	-7.0846+000	-1.8326+000	-8.8740+001
SMC	2.5805+000	3.1896+001	1.8896+000	-3.4945+001	-5.1377+000	9.0941+002	-1.6184+001	6.0038+001	2.9080+001

H-MATRIX

	TT4H	TT4	TT5HI	TT45LO	TT5	TT6C	TT7M
TT4H	5.7106+002	-3.0549+001	-1.2618+002	-1.1500+002	3.0644+001	1.4627+001	-8.7267+003
FMX	1.1271+001	-1.4547+001	-1.4040+002	-1.4039+002	-1.1770+002	-2.0582+002	-1.4036+002
WFAN	0.0000	1.0000+000	0.0000	0.0000	0.0000	0.0000	0.0000
SMAF	3.9205+000	-5.7754+000	-4.9126+001	-4.8970+001	-4.1025+001	-7.1638+001	-4.8371+001
SMC	-1.2840+000	1.4597+000	1.6050+001	1.5991+001	1.3489+001	2.3497+001	1.5991+001

D-MATRIX

	WFBH	AMIX	CIVV	RCVV	BLC
FMX	0.0000	-8.3748+002	-2.3274+002	3.3846+002	-5.6758+002
WFAN	0.0000	-3.2741+002	-3.5748+002	-3.8007+003	-7.3464+002
TT4	0.0000	0.0000	0.0000	0.0000	0.0000
SMAF	0.0000	1.1244+001	7.4706+001	-5.0387+001	3.9417+000
SMC	0.0000	1.1079+001	-7.6390+002	9.9106+001	2.6445+001

F100 LINEAR MODEL 24/0/OK 2/12/76

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-2.50000-0.00000)+J(0.00000)	0.00000	1.00000	1 (0.00000)+J(0.00000) 2 (0.00000)+J(0.00000) 3 (0.00000)+J(0.00000) 4 (0.00000)+J(0.00000) 5 (0.00000)+J(0.00000) 6 (1.00000+0.00000)+J(0.00000) 7 (0.00000)+J(0.00000) 8 (0.00000)+J(0.00000) 9 (0.00000)+J(0.00000) 10 (0.00000)+J(0.00000) 11 (0.00000)+J(0.00000) 12 (0.00000)+J(0.00000) 13 (0.00000)+J(0.00000) 14 (0.00000)+J(0.00000) 15 (0.00000)+J(0.00000) 16 (0.00000)+J(0.00000) 17 (0.00000)+J(0.00000)	1.0000000 0.0000000 0.0000000 0.0000000 0.0000000 1.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
(-6.74050+0.00200)+J(0.00000)	0.00000	1.00000	1 (-4.18730-0.00300)+J(0.00000) 2 (1.01136+0.00300)+J(0.00000) 3 (-6.08785-0.00300)+J(0.00000) 4 (0.00000)+J(0.00000) 5 (-5.28574+0.00300)+J(0.00000) 6 (3.71477-0.00300)+J(0.00000) 7 (1.00000+0.00000)+J(0.00000) 8 (-1.22356+0.00400)+J(0.00000) 9 (-1.48864-0.00400)+J(0.00000) 10 (1.28946-0.00400)+J(0.00000) 11 (-3.23862+0.00500)+J(0.00000) 12 (5.08422-0.00500)+J(0.00000) 13 (-1.43288+0.00200)+J(0.00000) 14 (-7.35918+0.00300)+J(0.00000) 15 (-1.86993-0.00300)+J(0.00000) 16 (1.36792+0.00700)+J(0.00000) 17 (-1.86384-0.00200)+J(0.00000)	0.0041873 0.010114 0.006879 0.000000 0.002657 0.000037 1.000000 0.001284 0.001689 0.001289 0.000324 0.005984 0.018328 0.007332 0.018700 0.000001 0.018636	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

```

(=1.3687+002)+J( 0.0000 ) 0.0000
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17
( 1.4903-002)+J( 0.0000 ) 0.0000
( -0.0062-003)+J( 0.0000 ) 0.0000
( -2.9589-002)+J( 0.0000 ) 0.0000
( 0.0000 )+J( 0.0000 ) 0.0000
( 1.0000+000)+J( 0.0000 ) 0.0000
( -7.1768-005)+J( 0.0000 ) 0.0000
( 6.6970-001)+J( 0.0000 ) 0.0000
( -2.4072-003)+J( 0.0000 ) 0.0000
( -3.9520-003)+J( 0.0000 ) 0.0000
( -4.0070-002)+J( 0.0000 ) 0.0000
( 1.7703-002)+J( 0.0000 ) 0.0000
( 3.0289-002)+J( 0.0000 ) 0.0000
( 7.2267-002)+J( 0.0000 ) 0.0000
( 2.6287-002)+J( 0.0000 ) 0.0000
( 4.9142-002)+J( 0.0000 ) 0.0000
( 8.7151-004)+J( 0.0000 ) 0.0000
( -1.1602-001)+J( 0.0000 ) 0.0000
( 1.5607-003)+J( 0.0000 ) 0.0000
( 1.3307-002)+J( 0.0000 ) 0.0000
( 9.9479-002)+J( 0.0000 ) 0.0000
( 0.0000 )+J( 0.0000 ) 0.0000
( -0.5666-001)+J( 0.0000 ) 0.0000
( -1.1325-003)+J( 0.0000 ) 0.0000
( -3.5975-001)+J( 0.0000 ) 0.0000
( 4.7353-002)+J( 0.0000 ) 0.0000
( 6.6908-002)+J( 0.0000 ) 0.0000
( 5.0600-002)+J( 0.0000 ) 0.0000
( 1.0000+000)+J( 0.0000 ) 0.0000
( -3.4674-001)+J( 0.0000 ) 0.0000
( 5.4705-001)+J( 0.0000 ) 0.0000
( 2.0609-001)+J( 0.0000 ) 0.0000
( 6.8186-002)+J( 0.0000 ) 0.0000
( -2.7451-002)+J( 0.0000 ) 0.0000
( 5.5652-001)+J( 0.0000 ) 0.0000
( -0.149203 ) 0.0000
( -0.06086 ) 0.0000
( -0.295896 ) 0.0000
( 0.00000 ) 0.0000
( 1.000000 ) 0.0000
( -0.000718 ) 0.0000
( 6.696698 ) 0.0000
( 0.024078 ) 0.0000
( 0.03552 ) 0.0000
( -0.400570 ) 0.0000
( 0.177503 ) 0.0000
( -0.30849 ) 0.0000
( 0.72674 ) 0.0000
( 0.028874 ) 0.0000
( 0.041442 ) 0.0000
( 0.008720 ) 0.0000
( -1.11018 ) 0.0000
( 0.015609 ) 0.0000
( 0.13091 ) 0.0000
( 0.94479 ) 0.0000
( 0.00000 ) 0.0000
( -956460 ) 0.0000
( -0.01323 ) 0.0000
( -3597536 ) 0.0000
( 0.47532 ) 0.0000
( 6.6908 ) 0.0000
( 50600 ) 0.0000
( 1.000000 ) 0.0000
( -346738 ) 0.0000
( 547049 ) 0.0000
( 206089 ) 0.0000
( 681869 ) 0.0000
( -0.27451 ) 0.0000
( 556515 ) 0.0000

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(-4.98915+001)+J( 8.8210+002) 4.88910+001 1.00000
1 (-6.46150+004)+J( 5.8335+004) .0066721 -18.00443
2 (-1.6244+005)+J(-1.00274+005) .000191 -18.31375
3 (-5.52820+004)+J(-1.98204+004) .005873 -100.2758
4 ( 0.00000 )+J( 0.00000 ) .000000 .00000
5 ( 7.14537+004)+J( 2.71244+004) .0007643 20.78718
6 (-1.05953+004)+J(-9.73344+005) .0011439 -17.4198
7 ( 3.94667+004)+J(-1.83261+004) .0004351 -24.9048
8 ( 1.13045+005)+J(-1.70171+005) .000204 -5.4082
9 (-4.06956+004)+J(-6.37343+005) .004119 -11.0909
10 (-1.01375+004)+J(-3.01154+005) .001058 -183.4598
11 ( 1.29574+004)+J( 5.12469+003) .126758 2.26488
12 ( 2.99854+004)+J( 2.64938+004) .004001 41.4630
13 ( 3.88910+002)+J( 3.56159+002) .0527353 42.4807
14 ( 1.46047+002)+J( 1.33551+002) .0197903 42.44074
15 ( 2.63409+003)+J( 2.34154+003) .0035244 41.6350
16 ( 2.60689+004)+J( 3.49944+005) .002430 7.64555
17 ( 1.00000+000)+J( 0.00000 ) 1.000000 .00000
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(-3.62960+001)+J( 0.00000 0 ) 0.00000 1.00000
1 (-2.23430+002)+J( 0.00000 ) .023430 .0000
2 ( 7.01900+005)+J( 0.00000 ) .000702 .0000
3 ( 6.99751+002)+J( 0.00000 ) .089751 .0000
4 ( 0.00000 )+J( 0.00000 ) .000000 .0000
5 (-1.68566+001)+J( 0.00000 ) .165663 .0000
6 (-3.75391+003)+J( 0.00000 ) .0037539 .0000
7 ( 4.57470+002)+J( 0.00000 ) .0457470 .0000
8 ( 3.41857+002)+J( 0.00000 ) .031857 .0000
9 ( 4.56188+002)+J( 0.00000 ) .0456188 .0000
10 (-1.42385+002)+J( 0.00000 ) .012385 .0000
11 ( 6.00058+001)+J( 0.00000 ) .800576 .0000
12 ( 2.59652+001)+J( 0.00000 ) .236554 .0000
13 ( 1.00000+000)+J( 0.00000 ) 1.000000 .0000
14 ( 3.65135+001)+J( 0.00000 ) .3651347 .0000
15 (-2.65438+001)+J( 0.00000 ) .2654380 .0000
16 ( 5.40983+002)+J( 0.00000 ) .0540983 .0000
17 (-9.25691+001)+J( 0.00000 ) .9256905 .0000
```

(-1.99121+000)+J(0.00000)	0.00000	1.00000	(-1.99042-001)+J(0.00000)	-1.990423	0.0000
(-9.52810-003)+J(0.00000)			(-4.60933-002)+J(0.00000)	-0.095281	0.0000
(-4.60933-002)+J(0.00000)			(-0.00000)+J(0.00000)	-0.46033	0.0000
(-5.36392-003)+J(0.00000)			(-4.65155-003)+J(0.00000)	0.000000	0.0000
(-4.65155-003)+J(0.00000)			(-0.46311-002)+J(0.00000)	-0.536392	0.0000
(-2.96499-002)+J(0.00000)			(-3.06980-002)+J(0.00000)	-0.085116	0.0000
(-2.1252-002)+J(0.00000)			(-1.04164-002)+J(0.00000)	-0.46451	0.0000
(-1.04164-002)+J(0.00000)			(-1.27022-002)+J(0.00000)	-0.296499	0.0000
(-7.4121-003)+J(0.00000)			(-3.30734-002)+J(0.00000)	-0.306980	0.0000
(-7.3289-002)+J(0.00000)			(-2.68035-002)+J(0.00000)	-0.21252	0.0000
(-3.30734-002)+J(0.00000)			(-1.04164-002)+J(0.00000)	-0.104164	0.0000
(-2.68035-002)+J(0.00000)			(-1.27022-002)+J(0.00000)	-0.127022	0.0000
			(-7.4121-003)+J(0.00000)	-0.074112	0.0000
			(-7.3289-002)+J(0.00000)	-0.000000	0.0000
			(-3.30734-002)+J(0.00000)	-0.000073	0.0000
			(-2.68035-002)+J(0.00000)	-0.330734	0.0000
				-0.0268035	0.0000

(-6.66577-001)+J(0.00000)	0.00000	1.00000	(-9.11500-001)+J(0.00000)	9.11504	0.0000
(-3.10924-001)+J(0.00000)			(-2.33019-001)+J(0.00000)	-2.330169	0.0000
(-0.00000)+J(0.00000)			(-0.00000)+J(0.00000)	-3.10924	0.0000
(-1.00000+000)+J(0.00000)			(-0.00000)+J(0.00000)	0.000000	0.0000
(-0.49885-001)+J(0.00000)			(-0.00000)+J(0.00000)	1.0000000	0.0000
(-1.59820-001)+J(0.00000)			(-0.00000)+J(0.00000)	-0.926336	0.0000
(-2.17333-001)+J(0.00000)			(-0.00000)+J(0.00000)	-4.98854	0.0000
(-2.81899-001)+J(0.00000)			(-0.00000)+J(0.00000)	-1.59819	0.0000
(-3.19110-001)+J(0.00000)			(-0.00000)+J(0.00000)	-1.626396	0.0000
(-5.75118-001)+J(0.00000)			(-0.00000)+J(0.00000)	-2.17333	0.0000
(-4.66555-001)+J(0.00000)			(-0.00000)+J(0.00000)	-2.81899	0.0000
(-1.71530-001)+J(0.00000)			(-0.00000)+J(0.00000)	-3.19110	0.0000
(-1.69284-001)+J(0.00000)			(-0.00000)+J(0.00000)	-5.75118	0.0000
			(-0.00000)+J(0.00000)	-4.66555	0.0000
			(-0.00000)+J(0.00000)	-1.71530	0.0000
			(-0.00000)+J(0.00000)	-1.69284	0.0000

(-4.97241+000)+J(-2.73287-001) 4.98011+000 .99349

1	(1.00000+000)+J(0.00000)	1.0000000	.00000
2	(-3.70618-002)+J(-1.92887-003)	.0371118	177.01455
3	(7.94678-001)+J(-6.39927-002)	.7972506	-4.60350
4	(0.00000)+J(0.00000)	.0000000	.00000
5	(-6.50846-002)+J(2.23278-002)	.6659775	160.21944
6	(-1.50142-002)+J(9.57135-004)	.0130495	175.78457
7	(1.43544-001)+J(8.2479-004)	.1435485	.32829
8	(5.27945-001)+J(-3.83440-002)	.5293332	-4.15403
9	(6.96318-001)+J(-5.4124-002)	.6984402	-4.46819
10	(3.84915-001)+J(-3.74027-002)	.3867283	-5.55007
11	(3.53218-001)+J(-5.06022-002)	.3865445	-7.52212
12	(3.4239-001)+J(-4.40148-002)	.3452074	-7.32550
13	(4.70635-001)+J(-6.0610-002)	.744777	-7.29655
14	(-1.09941-004)+J(-1.73042-002)	.0173046	-90.36402
15	(7.50034-001)+J(-1.0782-001)	.7567743	-7.65296
16	(9.15335-001)+J(-8.68432-002)	.9196446	-5.54379
17	(5.98767-001)+J(-1.05367-001)	.6081452	-10.07502

(-1.82650+001)+J(4.90258+000) 1.95899+001 .98810

1	(-2.54080-002)+J(-1.73256-002)	.0307530	-145.71008
2	(-5.57360-003)+J(-8.71169-003)	.0103421	-122.61066
3	(-1.82633-001)+J(-2.15657-001)	.2826003	-130.26019
4	(0.00000)+J(0.00000)	.0000000	.00000
5	(1.26139-001)+J(-1.5137-001)	.1972425	-50.24488
6	(-3.97570-004)+J(-2.39448-003)	.0024276	-99.47371
7	(-1.33917-002)+J(-1.5568-001)	.1561430	-94.92005
8	(-5.7716-002)+J(5.35599-002)	.0787339	137.13899
9	(-6.40233-002)+J(7.04655-002)	.0952070	132.25754
10	(1.09003-001)+J(1.05554-001)	.1462997	42.69126
11	(1.78450-001)+J(2.94557-001)	.3444846	58.80007
12	(7.97401-002)+J(2.08956-001)	.2335536	69.1251
13	(1.41931-001)+J(3.17983-001)	.3482209	65.97460
14	(5.26393-002)+J(1.03918-001)	.1169446	62.69845
15	(7.93487-001)+J(8.95909-002)	.7985200	6.44185
16	(2.20431-001)+J(2.93777-001)	.3712915	53.58066
17	(1.00000+000)+J(0.00000)	1.0000000	.00000

(-2.15018+001)+J(0.00000	1.00000	1	(-1.32935+002)+J(0.00000	-0.12935	0.0000
		2	(-4.34377+003)+J(0.00000	-0.043736	0.0000
		3	(-6.20691+003)+J(0.0000	-0.062099	0.0000
		4	(0.0000	0.00000	0.0000
		5	(1.3754+001)+J(0.00000	0.00000	0.0000
		6	(-4.61811+004)+J(0.00000	-0.06181	0.0000
		7	(7.4671+002)+J(0.0000	0.074671	0.0000
		8	(-3.7905+002)+J(0.00000	-0.37905	0.0000
		9	(-6.6687+002)+J(0.00000	-0.66887	0.0000
		10	(1.2369+001)+J(0.00000	0.123693	0.0000
		11	(1.1582+001)+J(0.00000	0.115821	0.0000
		12	(6.0166+002)+J(0.00000	0.60166	0.0000
		13	(1.0935+001)+J(0.00000	0.1093546	0.0000
		14	(3.6134+002)+J(0.00000	0.36134	0.0000
		15	(-6.5842+001)+J(0.00000	-0.658424	0.0000
		16	(1.0000+000)+J(0.00000	0.000000	0.0000
		17	(-6.6993+002)+J(0.00000	-0.669933	0.0000
(-1.92303+001)+J(0.00000	1.00000	1	(-4.03369+003)+J(0.00000	-0.044037	0.0000
		2	(-2.8966+003)+J(0.00000	-0.08899	0.0000
		3	(-1.6992+01)+J(0.00000	-0.139923	0.0000
		4	(0.0000	0.00000	0.0000
		5	(6.2370+003)+J(0.00000	0.00000	0.0000
		6	(-3.0876+005)+J(0.00000	-0.006237	0.0000
		7	(-5.9394+002)+J(0.00000	-0.000309	0.0000
		8	(-1.74743+003)+J(0.00000	-0.050396	0.0000
		9	(-3.8614+002)+J(0.00000	-0.017474	0.0000
		10	(-1.6667+002)+J(0.00000	-0.37614	0.0000
		11	(2.4799+002)+J(0.00000	0.15627	0.0000
		12	(1.67261+002)+J(0.00000	0.247999	0.0000
		13	(4.31541+003)+J(0.00000	0.157261	0.0000
		14	(1.72128+003)+J(0.00000	0.043154	0.0000
		15	(-2.37427+001)+J(0.00000	-0.017213	0.0000
		16	(1.0000+000)+J(0.00000	-0.2374270	0.0000
		17	(3.29949+001)+J(0.00000	0.000000	0.0000

(-2.10817+001)+J(0.00000)	0.00000	1.00000	1	(-9.43879+003)+J(0.00000)	-0.096368	.00000
				2	(-3.76960+003)+J(0.00000)	-0.037896	.00000
				3	(-5.89155+002)+J(0.00000)	-0.058155	.00000
				4	(0.00000)	0.000000	.00000
				5	(8.30378+002)+J(0.00000)	0.030378	.00000
				6	(-4.39903+004)+J(0.00000)	-0.004399	.00000
				7	(2.10316+002)+J(0.00000)	0.210316	.00000
				8	(-2.34083+002)+J(0.00000)	-0.234083	.00000
				9	(-5.53855+002)+J(0.00000)	-0.538555	.00000
				10	(8.42988+002)+J(0.00000)	0.842988	.00000
				11	(8.32685+002)+J(0.00000)	0.832685	.00000
				12	(4.51612+002)+J(0.00000)	0.451612	.00000
				13	(6.78967+002)+J(0.00000)	0.678967	.00000
				14	(2.31710+002)+J(0.00000)	0.231710	.00000
				15	(-4.38735+001)+J(0.00000)	-0.438735	.00000
				16	(1.00000+000)+J(0.00000)	1.000000	.00000
				17	(1.51368+001)+J(0.00000)	1.513683	.00000
(-1.00000+001)+J(0.00000)	0.00000	1.00000	1	(-1.47661+001)+J(0.00000)	-1.476614	.00000
				2	(-2.18736+002)+J(0.00000)	-0.218736	.00000
				3	(4.46440+002)+J(0.00000)	0.446440	.00000
				4	(1.00000+000)+J(0.00000)	1.000000	.00000
				5	(2.09997+001)+J(0.00000)	0.209997	.00000
				6	(-7.46114+003)+J(0.00000)	-0.746114	.00000
				7	(2.43193+001)+J(0.00000)	0.243193	.00000
				8	(-1.24359+001)+J(0.00000)	-0.124359	.00000
				9	(-1.99497+001)+J(0.00000)	-1.99497	.00000
				10	(-9.8209+003)+J(0.00000)	-0.98209	.00000
				11	(5.34380+001)+J(0.00000)	0.534380	.00000
				12	(4.81045+001)+J(0.00000)	0.481045	.00000
				13	(5.79622+001)+J(0.00000)	0.579622	.00000
				14	(1.46830+001)+J(0.00000)	0.146830	.00000
				15	(8.47089+001)+J(0.00000)	0.847089	.00000
				16	(-2.95395+001)+J(0.00000)	-0.295395	.00000
				17	(6.23213+001)+J(0.00000)	0.623213	.00000

F100 LINEAR MODEL 20/0/0K 2/12/75
 *** THE MATRICES IN FINAL FORM ***

CASE 5

F-MATRIX									
SHEAN	SNCOM	PT7M	AFCOM	PT3	FTIT	PT45	TT25H	TT25C	TT3
-2.702+00	2.025+00	4.915+00	1.452+00	-3.694+00	0.000	3.646+00	-1.991+00	-5.015+00	-6.626+00
-2.704+00	4.134+00	-2.653+00	1.360+00	-1.999+00	0.000	-5.652+00	1.646+00	-7.387+00	-1.258+00
1.884+00	-7.061+00	-2.328+00	4.991+00	5.003+00	0.000	3.878+00	3.808+00	-3.112+00	-4.562+00
0.000	0.000	0.000	-1.000+00	0.000	0.000	0.000	0.000	0.000	0.000
6.714+00	6.528+00	7.501+00	-4.875+00	-1.396+00	0.000	1.592+00	-3.412+00	2.075+00	4.101+00
0.000	0.000	0.000	0.000	0.000	-2.500+00	0.000	0.000	0.000	0.000
3.031+00	1.050+00	4.314+00	-5.330+00	3.725+00	0.000	-8.219+00	-6.222+00	-6.358+00	-2.536+00
3.173+00	-1.079+00	3.596+00	-2.904+00	8.539+00	0.000	5.866+00	-1.468+00	1.058+00	1.237+00
2.656+00	5.484+00	4.552+00	-3.542+00	1.291+00	0.000	7.291+00	4.693+00	-1.713+00	1.541+00
-2.107+00	1.245+00	-2.352+00	1.500+00	4.301+00	0.000	-1.783+00	1.758+00	-6.055+00	-2.005+00
-2.099+00	1.173+00	-2.041+00	1.021+00	-3.587+00	0.000	-1.039+00	1.507+00	-1.732+00	3.452+00
-1.295+00	-1.158+00	-1.392+00	2.045+00	3.587+00	0.000	-2.255+00	6.442+00	-3.461+00	1.849+00
3.078+00	3.574+00	-3.431+00	1.026+00	-1.315+00	0.000	1.332+00	-1.449+00	1.271+00	7.046+00
1.272+00	1.817+00	1.365+00	0.925+00	-5.255+00	0.000	5.341+00	-5.792+00	4.127+00	2.858+00
2.673+00	9.467+00	4.285+00	1.010+00	-6.206+00	0.000	1.367+00	-1.553+00	-4.123+00	2.960+00
-3.196+00	6.742+00	1.110+00	-0.202+00	1.551+00	0.000	1.738+00	-3.380+00	1.990+00	1.694+00
-1.112+00	0.267+00	1.610+00	-7.472+00	9.169+00	0.000	1.755+00	-2.085+00	2.891+00	3.157+00

F-MATRIX									
SHEAN	SNCOM	PT7M	AFCOM	PT3	FTIT	PT45	TT25H	TT25C	TT3
2.713+00	3.607+00	3.037+00	-2.552+00	-3.455+00	-4.057+00	-3.367+00	-6.222+00	-6.358+00	-2.536+00
1.237+00	-1.237+00	4.086+00	-4.686+00	-4.728+00	-5.463+00	-4.687+00	1.646+00	-7.387+00	-1.258+00
1.056+00	-2.450+00	-1.727+00	-1.411+00	1.017+00	4.212+00	1.503+00	3.808+00	-3.112+00	-4.562+00
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
-1.113+00	1.775+00	1.341+00	-1.387+00	1.340+00	1.546+00	1.344+00	0.000	0.000	0.000
0.000	0.000	1.235+00	1.370+00	0.000	0.000	0.000	0.000	0.000	0.000
7.038+00	5.659+00	-1.078+00	-1.075+00	1.745+00	3.231+00	-1.075+00	-3.412+00	2.075+00	4.101+00
-5.102+00	6.017+00	6.870+00	6.836+00	5.086+00	7.668+00	6.874+00	3.808+00	-3.112+00	-4.562+00
-6.861+00	8.942+00	8.729+00	8.794+00	8.076+00	9.695+00	8.701+00	3.808+00	-3.112+00	-4.562+00
3.669+00	-4.582+00	-4.024+00	-4.462+00	-4.325+00	-4.959+00	-4.498+00	1.646+00	-7.387+00	-1.258+00
-4.094+00	4.519+00	4.937+00	4.932+00	-8.435+00	-8.454+00	-8.438+00	0.000	0.000	0.000
2.387+00	7.571+00	-2.470+00	-2.665+00	-2.577+00	-2.937+00	-2.676+00	0.000	0.000	0.000
-4.150+00	4.484+00	4.992+00	7.233+00	7.233+00	7.233+00	7.233+00	0.000	0.000	0.000
-2.173+00	1.850+00	-1.792+00	-1.970+00	-2.956+00	3.221+00	2.937+00	0.000	0.000	0.000
-4.508+00	1.258+00	1.573+00	-1.550+00	-1.949+00	3.080+00	-3.549+00	0.000	0.000	0.000
-2.658+00	3.207+00	-2.950+00	-2.951+00	-1.077+00	-1.970+00	1.903+00	0.000	0.000	0.000
-1.685+00	1.430+00	1.683+00	-1.682+00	3.457+00	1.949+00	-4.801+00	0.000	0.000	0.000

G-MATRIX

	WFSH	ANVTX	CTVV	RCVV	BLC
SFAN	0.000	-6.4042-002	6.7373-002	-1.1471-002	-1.3924+000
SFAN	0.000	-1.5236-002	7.9371-003	1.0779-001	-9.0172-002
SFAN	0.000	-1.5801+000	-8.0398-002	2.7102-001	7.4441-001
SFAN	1.000+001	0.000	0.000	0.000	0.000
SFAN	0.000	3.3647+000	-2.2585+000	-2.4551+001	-7.5190+001
SFAN	0.000	0.000	0.000	0.000	0.000
SFAN	0.000	-2.6611+000	-1.1054+000	-3.6731+000	3.6395+001
SFAN	0.000	1.4902-001	-5.4327-002	-2.6449-002	2.6474+000
SFAN	0.000	2.1279-001	-8.4666-002	7.9771-003	3.2767+000
SFAN	0.000	-8.5453-002	7.1968-002	5.1147-001	-1.9852+000
SFAN	0.000	-2.2523+000	1.0248-003	1.3515-002	-2.3511+000
SFAN	0.000	-1.9782-001	4.1924-001	4.8857+000	1.6833+001
SFAN	0.000	0.1095-001	-1.1292-002	-1.0493-001	-2.9553+000
SFAN	0.000	1.3241-003	-0.5267-003	-4.3676-002	-1.1336+000
SFAN	0.000	-2.8752-002	-1.0299-002	-6.0457+003	-1.1266+000
SFAN	0.000	7.4163-003	-1.7442-003	-2.7995+002	1.4276-001
SFAN	0.000	5.4250-001	3.0970-001	-1.8470+000	8.4466+000

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H-MATRIX

	SFAN	SNCOM	PTM	WFCOM	PT3	FTT	PT45	TT25H	TT25C	TT3
SFAN	4.0467-001	-2.1214+000	4.2398+000	3.5081-001	1.1361-001	0.0000	1.0278+000	1.0368+000	-1.2261-001	-1.8866-001
SFAN	9.0297-001	2.3193-001	-2.4958-001	2.1503-001	-6.6778-002	0.0000	-4.3333-002	-2.3344-001	-7.5807-002	-9.2579-002
SFAN	0.000	0.000	0.000	0.000	0.000	0.0000	0.0000	0.0000	0.0000	0.0000
SFAN	-1.4018+000	5.2568+000	-6.1130+000	4.3339-000	-1.5411+000	0.0000	-9.8158-001	-5.9335+000	-1.7189+000	-2.0994+000
SFAN	7.2646+000	1.3064+000	-8.1094+000	-2.9858+000	-1.3783+001	0.0000	1.3071+000	-6.8987+001	2.2853+000	2.7894+000
SFAN	9.2646-002	-1.3131-002	-5.4334-001	0.1666-001	-1.0737-001	0.0000	-8.8413-002	-1.4872-001	-7.5097-002	-1.8807-001
SFAN	5.4395-002	-1.3035-002	-1.1500-001	8.6029-002	-2.1384-002	0.0000	-1.8640-002	2.4514-003	-5.9414-004	-4.0024-002

H-MATRIX

	TT3	TT45H	TT45L	TT5	TT6	TT7
SFAN	4.4854-001	-1.0757+000	-7.9507-002	-8.1457-002	7.9014-002	-8.3993-002
SFAN	4.1662-001	-1.2504+001	-5.1405-002	-5.1190-002	-4.9422-002	-5.1320-002
SFAN	0.000	1.0000+000	0.0000	0.0000	0.0000	0.0000
SFAN	9.3108+000	-1.1914+001	-1.1658+000	-1.1607+000	-1.2923+000	-1.1642+000
SFAN	-1.2779+001	1.6247+001	1.5440+000	1.5421+000	1.7175+000	1.5515+000
SFAN	9.3173-001	-1.0623+000	-1.0368-001	-1.0404-001	-1.1591-001	-1.0367-001
SFAN	1.7591-001	-2.2639-001	-2.2082-002	-2.2060-002	-2.4872-002	-2.2074-002

FIG. LINEAR MODEL 20/0/0K 2/12/76

D-MATRIX	AFVH	AMTX	CIVV	PCVV	BLC
FVWY	0.0000	-5.0453-002	-2.0171-002	8.5833-002	-3.8174-001
WEAN	0.0000	-1.2635-002	-3.4125-002	2.1107-003	-1.9481-001
TTG	0.0000	0.0000	0.0000	0.0000	0.0000
SWF	0.0000	-2.6265-001	1.0040+000	4.7197-002	-4.5238+000
SWC	0.0000	9.6857-001	-2.3103-001	-3.0732+000	9.7159-001
DSFOT	0.0000	-2.5417-002	6.0473-003	2.2971-002	-3.9454-001
DSFSC	0.0000	-5.5184-003	-1.4393-003	5.7833-003	-8.0019-002

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-2.50000-001)+J(0.00000)	0.00000	1.00000	1 (0.00000)+J(0.00000)	.0000000	.00000
			2 (0.00000)+J(0.00000)	.0000000	.00000
			3 (0.00000)+J(0.00000)	.0000000	.00000
			4 (0.00000)+J(0.00000)	.0000000	.00000
			5 (0.00000)+J(0.00000)	.0000000	.00000
			6 (1.00000+000)+J(0.00000)	1.0000000	.00000
			7 (0.00000)+J(0.00000)	.0000000	.00000
			8 (0.00000)+J(0.00000)	.0000000	.00000
			9 (0.00000)+J(0.00000)	.0000000	.00000
			10 (0.00000)+J(0.00000)	.0000000	.00000
			11 (0.00000)+J(0.00000)	.0000000	.00000
			12 (0.00000)+J(0.00000)	.0000000	.00000
			13 (0.00000)+J(0.00000)	.0000000	.00000
			14 (0.00000)+J(0.00000)	.0000000	.00000
			15 (0.00000)+J(0.00000)	.0000000	.00000
			16 (0.00000)+J(0.00000)	.0000000	.00000
			17 (0.00000)+J(0.00000)	.0000000	.00000
(-6.30702+002)+J(0.00000)	0.00000	1.00000	1 (-4.42670-003)+J(0.00000)	-.0044267	.00000
			2 (8.31550-004)+J(0.00000)	.0009315	.00000
			3 (-4.75837-003)+J(0.00000)	-.0047584	.00000
			4 (0.00000)+J(0.00000)	.0000000	.00000
			5 (-2.50006-002)+J(0.00000)	-.0250006	.00000
			6 (2.74946-006)+J(0.00000)	.0000027	.00000
			7 (1.00000+000)+J(0.00000)	1.0000000	.00000
			8 (-6.38887-004)+J(0.00000)	-.0063889	.00000
			9 (-7.94214-004)+J(0.00000)	-.0079421	.00000
			10 (5.60678-004)+J(0.00000)	.0005607	.00000
			11 (-1.63013-004)+J(0.00000)	-.0016301	.00000
			12 (2.92481-003)+J(0.00000)	.0029248	.00000
			13 (-1.77251-002)+J(0.00000)	-.0177251	.00000
			14 (-7.06353-003)+J(0.00000)	-.0070636	.00000
			15 (-1.04262-003)+J(0.00000)	-.0019426	.00000
			16 (-2.53908-006)+J(0.00000)	-.0000025	.00000
			17 (-2.24783-002)+J(0.00000)	-.0224783	.00000

F100 LINEAR MODEL 2010/OK 2/12/76

[illegible][illegible]

```
(-0.98799+001)+J( 1.49795-001) 0.98801+001 1.00000
1 (-9.38231-004)+J(-1.21514-003) .0015332 -127.67243
2 (-2.74071-005)+J(-9.14014-006) .0002899 -161.55721
3 (-6.51566-004)+J(-3.22912-005) .0006524 -177.16278
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 ( 9.00587-004)+J( 3.14823-004) .0009509 19.26834
6 (-1.33144-004)+J(-2.01468-004) .0002443 -124.43783
7 (-1.41784-004)+J( 1.00188-004) .0017336 144.75399
8 (-2.72185-004)+J(-4.57073-005) .0002700 -170.44682
9 ( 1.47816-004)+J(-6.42007-005) .0001612 -23.47312
10 ( 3.33980-005)+J(-1.25417-005) .0000357 -20.36228
11 ( 1.34568-001)+J( 1.36016-002) .1325534 5.77164
12 ( 3.16626-004)+J( 4.49889-004) .0005522 50.84663
13 ( 5.33736-002)+J( 7.76593-002) .0005346 55.39946
14 ( 2.00915-002)+J( 2.91153-002) .0333747 55.39175
15 ( 2.70481-003)+J( 3.50277-003) .0044625 51.71529
16 ( 2.94050-004)+J( 4.22843-005) .0002971 6.18302
17 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
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(-7.54595-001)+J( 0.00000 ) 0.00000 1.00000
1 ( 8.06004-001)+J( 0.00000 ) .8060037 .00000
2 ( 2.19064-001)+J( 0.00000 ) .2190639 .00000
3 ( 1.27380-001)+J( 0.00000 ) .1273802 .00000
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
6 ( 1.06461-001)+J( 0.00000 ) .1064612 .00000
7 ( 4.93547-001)+J( 0.00000 ) .4935470 .00000
8 ( 1.45940-001)+J( 0.00000 ) .1459399 .00000
9 ( 1.31392-001)+J( 0.00000 ) .1313922 .00000
10 ( 2.87425-001)+J( 0.00000 ) .2874255 .00000
11 (-2.57323-001)+J( 0.00000 ) -.2573225 .00000
12 (-2.93399-001)+J( 0.00000 ) -.2933993 .00000
13 (-3.79814-001)+J( 0.00000 ) -.3798145 .00000
14 (-5.16327-001)+J( 0.00000 ) -.5163277 .00000
15 (-4.71657-001)+J( 0.00000 ) -.4716572 .00000
16 ( 1.39234-001)+J( 0.00000 ) .1392343 .00000
17 (-1.46897-001)+J( 0.00000 ) -.1468978 .00000
```



```
(-2.46875+0.01)+J( 8.37918+0.00) 2.60707+0.01 .94694
1 ( 8.07433-0.04)+J(-2.69415-0.02) .0269537 -88.28295
2 ( 1.09503-0.04)+J(-3.73348-0.03) .0037351 -88.32000
3 (-3.62220-0.02)+J(-1.06615-0.01) .1126000 -108.76500
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 ( 2.90510-0.01)+J(-7.62534-0.02) .3003512 -14.70728
6 ( 1.81463-0.03)+J(-1.80831-0.03) .0025618 -44.90007
7 ( 9.61136-0.02)+J(-7.41494-0.02) .1213918 -37.64934
8 (-8.45437-0.02)+J(-4.99905-0.03) .0846855 -176.63559
9 (-1.04082-0.01)+J(-2.34974-0.03) .1041089 -178.70672
10 ( 2.97049-0.02)+J( 5.14306-0.02) .0596286 60.22573
11 (-1.39322-0.01)+J( 4.29440-0.01) .4514743 107.97451
12 (-1.56972-0.01)+J( 2.06369-0.01) .2592840 127.25802
13 (-2.28535-0.01)+J( 4.62848-0.01) .5161944 116.27829
14 (-7.29466-0.02)+J( 1.67590-0.01) .1827775 113.52196
15 ( 5.47108-0.01)+J( 2.30284-0.01) .5935977 22.82681
16 ( 9.80968-0.02)+J( 1.68159-0.01) .2121955 62.44473
17 ( 1.00000+0.00)+J( 0.00000 ) 1.0000000 .00000
```

```
(-2.46875+0.01)+J( 8.37918+0.00) 2.60707+0.01 .94694
1 (-1.38877-0.02)+J( 0.00000 ) -.0138877 .00000
2 (-5.46576-0.03)+J( 0.00000 ) -.0054658 .00000
3 (-2.52413-0.01)+J( 0.00000 ) -.2524132 .00000
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 ( 1.56405-0.01)+J( 0.00000 ) .1564051 .00000
6 ( 7.49534-0.04)+J( 0.00000 ) .007496 .00000
7 (-7.16332-0.02)+J( 0.00000 ) -.0716332 .00000
8 (-5.06457-0.02)+J( 0.00000 ) -.0506457 .00000
9 (-6.51831-0.02)+J( 0.00000 ) -.0651831 .00000
10 ( 9.55800-0.02)+J( 0.00000 ) .0955800 .00000
11 (-3.12137-0.02)+J( 0.00000 ) -.0312137 .00000
12 (-2.55856-0.02)+J( 0.00000 ) -.0255856 .00000
13 (-1.39074-0.01)+J( 0.00000 ) -.1390741 .00000
14 (-4.81079-0.02)+J( 0.00000 ) -.0481079 .00000
15 ( 5.35059-0.01)+J( 0.00000 ) .5350587 .00000
16 ( 3.15078-0.01)+J( 0.00000 ) .3150778 .00000
17 ( 1.00000+0.00)+J( 0.00000 ) 1.0000000 .00000
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AD-A052 346 SYSTEMS CONTROL INC PALO ALTO CALIF AERONAUTICAL AND--ETC F/G 21/5
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JUN 77 R L DE HOFF, W E HALL, R J ADAMS F33615-75-C-2053
UNCLASSIFIED AFAPL-TR-77-35-VOL-2 NL

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AFAPL-TR-77-35-VOL-2 NL

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(-1.95162+001)+J(0.00000	1.00000	1	(-1.05475-003)+J(0.00000)	-0.010547	.00000
		2	(-1.10432-003)+J(0.00000)	-0.011043	.00000
		3	(-9.43474-002)+J(0.00000)	-0.0943474	.00000
		4	(0.00000)+J(0.00000)	.0000000	.00000
		5	(-3.19795-002)+J(0.00000)	-0.319795	.00000
		6	(8.33831-005)+J(0.00000)	.0000831	.00000
		7	(-6.13675-002)+J(0.00000)	-0.0613675	.00000
		8	(7.13475-003)+J(0.00000)	.0713475	.00000
		9	(2.41310-002)+J(0.00000)	.0241310	.00000
		10	(-1.74194-002)+J(0.00000)	-0.174194	.00000
		11	(6.09486-004)+J(0.00000)	.0006095	.00000
		12	(1.87973-003)+J(0.00000)	.0018797	.00000
		13	(-1.33152-002)+J(0.00000)	-0.133152	.00000
		14	(-4.41126-003)+J(0.00000)	-0.044113	.00000
		15	(-5.51690-001)+J(0.00000)	-0.5516902	.00000
		16	(1.00000+000)+J(0.00000)	1.0000000	.00000
		17	(-2.35775-002)+J(0.00000)	-0.235775	.00000
(-2.12357+001)+J(0.00000	1.00000	1	(-2.11206-002)+J(0.00000)	-0.211206	.00000
		2	(-6.64017-003)+J(0.00000)	-0.066402	.00000
		3	(-1.11455-001)+J(0.00000)	-0.1114552	.00000
		4	(0.00000)+J(0.00000)	.0000000	.00000
		5	(1.62155-001)+J(0.00000)	.1621546	.00000
		6	(-6.34317-004)+J(0.00000)	-0.006343	.00000
		7	(1.89486-002)+J(0.00000)	.0189486	.00000
		8	(-4.89548-002)+J(0.00000)	-0.489548	.00000
		9	(-6.43458-002)+J(0.00000)	-0.643458	.00000
		10	(1.78825-001)+J(0.00000)	.178825	.00000
		11	(1.58581-001)+J(0.00000)	.158581	.00000
		12	(8.39561-002)+J(0.00000)	.0839561	.00000
		13	(1.03999-001)+J(0.00000)	.1039991	.00000
		14	(3.51567-002)+J(0.00000)	.0351567	.00000
		15	(-4.82174-001)+J(0.00000)	-0.4821743	.00000
		16	(1.00000+000)+J(0.00000)	1.0000000	.00000
		17	(1.32261-001)+J(0.00000)	.1322610	.00000

F100 LINEAR MODEL 20/0/0K 2/12/76

(-2.04221+001)+J(0.00000	1.00000	1	(-4.69964-003)+J(0.00000)	-0046996	.00000
		2	(-2.43394-003)+J(0.00000)	-0024339	.00000
		3	(-1.15378-001)+J(0.00000)	-1153783	.00000
		4	(0.00000)+J(0.00000)	0000000	.00000
		5	(-2.00580-002)+J(0.00000)	-0200580	.00000
		6	(-2.03537-004)+J(0.00000)	-0002035	.00000
		7	(-6.62148-002)+J(0.00000)	-0662148	.00000
		8	(4.10590-003)+J(0.00000)	0041059	.00000
		9	(-2.05607-002)+J(0.00000)	-0205607	.00000
		10	(1.57606-002)+J(0.00000)	0157606	.00000
		11	(5.14703-002)+J(0.00000)	0514703	.00000
		12	(3.17425-002)+J(0.00000)	0317425	.00000
		13	(3.20546-002)+J(0.00000)	0320546	.00000
		14	(1.07483-002)+J(0.00000)	0107483	.00000
		15	(-4.74330-001)+J(0.00000)	-4743299	.00000
		16	(1.00000+000)+J(0.00000)	1000000	.00000
		17	(6.23153-002)+J(0.00000)	0623153	.00000

(-1.00000+001)+J(0.00000	1.00000	1	(-5.46560-002)+J(0.00000)	-0546560	.00000
		2	(-2.66111-002)+J(0.00000)	-0266111	.00000
		3	(1.01094-001)+J(0.00000)	1010939	.00000
		4	(9.27429-001)+J(0.00000)	9274290	.00000
		5	(1.00261-001)+J(0.00000)	1002608	.00000
		6	(-8.28725-003)+J(0.00000)	-0082872	.00000
		7	(1.29762-001)+J(0.00000)	1297621	.00000
		8	(-2.20674-002)+J(0.00000)	-0220674	.00000
		9	(-5.39321-003)+J(0.00000)	-0053932	.00000
		10	(2.05111-002)+J(0.00000)	0205111	.00000
		11	(6.26001-001)+J(0.00000)	6260009	.00000
		12	(5.43022-001)+J(0.00000)	5430221	.00000
		13	(6.37214-001)+J(0.00000)	6372142	.00000
		14	(1.59889-001)+J(0.00000)	1598891	.00000
		15	(1.00000+000)+J(0.00000)	1000000	.00000
		16	(-1.04872-002)+J(0.00000)	-0104872	.00000
		17	(6.00288-001)+J(0.00000)	6002882	.00000

----- THE MATRICES IN FINAL FORM -----

CASE 6

PARAMETER	SNFAN	SNCOM	PTM	PT3	PT45	TT25H	TT25C	TT3	TT4PHI	TT4PLO
SNFAN	-2.1390+000	-2.4380+000	-5.0974+000	-6.6139+001	-3.7327+000	-2.1297+000	-5.3483+001	-6.3291+001	-2.7063+001	-3.5571+001
SNCOM	-2.4125+001	-3.9330+000	-2.7455+001	1.0675+000	-6.0723+001	1.6520+000	-7.4388+002	-1.3003+001	4.8091+001	9.6296+003
PTM	-2.0214+000	-7.3523+000	-2.4440+001	7.6282+001	4.0757+000	4.1275+000	-1.8152+001	-1.6980+001	2.5876+001	6.8554+003
PT3	7.1388+001	6.2348+002	6.1888+001	-1.4920+002	1.7103+001	-3.6563+002	-2.2129+001	3.1827+001	1.4589+001	1.4659+001
PT45	4.7748+001	9.8361+001	4.5164+002	3.5529+002	-8.1570+002	-6.0555+001	1.5917+001	-4.8620+000	-3.3920+001	9.2808+000
TT25H	2.7817+000	-3.6463+000	3.6177+000	9.5503+001	5.6338+001	-1.6770+001	1.0037+000	6.8118+001	6.6373+001	6.6897+001
TT25C	2.6797+000	-5.6562+000	6.4122+000	1.2705+000	7.1498+001	4.6765+000	-1.8760+001	-8.4402+001	-8.2127+001	-8.2661+001
TT3	-2.0286+000	1.8602+000	-2.3261+000	4.0624+000	-3.6698+001	1.7402+001	-6.4822+001	-2.0430+001	-4.2805+001	-4.3231+001
TT4PHI	-3.8464+002	1.4733+001	5.0186+002	-2.5086+002	-6.6902+003	1.7729+001	-1.6725+002	4.0859+000	-5.0010+001	-1.1711+002
TT4PLO	-5.2183+003	-2.5087+002	-6.6234+003	3.4116+003	-1.0038+003	-2.3682+002	-2.2078+003	5.4467+001	-6.0012+000	-6.6830+001
TT4	-1.3923+001	-1.2664+002	-1.5940+001	5.7783+000	-2.5323+000	7.1849+001	4.4207+000	1.8485+001	-2.9621+000	-2.9707+000
TT45HI	8.7116+002	1.2716+000	8.9285+002	-1.2490+001	1.1893+001	-3.1139+001	3.2667+000	8.1108+000	-1.1631+001	-1.2586+000
TT45LO	3.4488+002	-5.0678+001	3.5277+002	-4.9974+000	4.7578+000	-1.2466+001	1.2542+002	3.2447+000	-4.6520+000	-5.0322+001
TT5	1.4773+001	-1.4390+000	4.1113+000	-5.3870+000	7.3885+001	3.5591+001	3.3582+002	3.4770+000	-5.0694+000	-5.7582+001
TT6C	-3.1368+002	6.8123+001	1.0804+001	-2.4400+002	1.7425+002	-3.4152+001	1.9902+001	1.3765+001	1.9167+002	1.3940+002
TT7M	-1.0702+001	4.7444+001	1.7015+000	-7.4345+002	-1.8772+001	-2.3401+001	-2.8221+000	-1.2611+000	-2.8448+000	-1.9414+000

PARAMETER	TT4	TT45HI	TT45LO	TT5	TT6C	TT7M
SNFAN	-8.4412+001	3.6222+001	-2.4481+001	-3.7123+001	-4.3950+001	-3.6735+001
SNCOM	-2.7847+001	-4.8708+002	-4.9216+002	-4.7081+002	-5.5104+002	-4.9748+002
PTM	-1.2232+000	-1.4649+002	-1.8849+002	1.1890+000	5.6791+001	-3.1630+002
PT3	5.0533+001	1.4728+001	1.4659+001	1.4100+001	1.6473+001	1.4733+001
PT45	1.3685+002	1.4810+001	1.4809+001	1.7021+001	1.9232+001	1.4808+001
TT25H	6.9672+001	6.7931+001	6.6901+001	6.4842+001	7.5048+001	6.8903+001
TT25C	4.7198+001	8.4844+001	8.3708+001	8.0917+001	9.2621+001	8.3701+001
TT3	-4.5168+001	-4.3458+001	-4.3237+001	-4.1731+001	-4.8067+001	-4.3134+001
TT4PHI	4.5867+001	5.0177+003	-1.1709+002	-1.3381+002	-1.0036+002	-1.0037+002
TT4PLO	6.1155+000	-8.0254+004	-1.6052+003	-1.8060+003	-1.4050+003	-1.4051+003
TT4	5.0890+001	-2.8666+000	-2.9662+000	-2.8662+000	-3.3129+000	-2.9811+000
TT45HI	5.4444+001	-4.9950+001	4.1378+002	2.3948+002	2.3955+002	3.4842+002
TT45LO	2.3379+001	-1.7982+001	-1.9840+000	9.4037+003	9.4074+003	1.1113+002
TT5	2.6570+001	-1.5049+000	-1.6031+001	-2.0000+001	-1.8466+002	-1.6786+002
TT6C	5.5757+002	2.0905+002	1.3939+002	2.0902+002	-1.9980+001	1.9165+002
TT7M	-3.2511+000	1.8331+000	1.8442+000	3.4552+001	1.9679+001	-4.8170+001

G-MATRIX

	WFEH	ANIX	CTVV	RCVV	BLC
SFAN	1.439+000	-1.1511-001	6.8480-002	-1.1273-002	-1.8791-002
SNCM	1.1033-001	-2.1507-002	7.7745-003	1.3275-001	-1.1582-004
PTM	-2.6169-002	-3.6185+000	-2.2592-002	3.0341-001	-4.5068-003
PT3	-4.6744+001	5.1241+000	-2.3312+000	-3.0240+001	-1.6715+000
PT5	-5.4340+001	4.5473+000	-2.0718+000	-9.4639+000	1.1161+000
TT25M	-2.5933+000	-2.1246-001	-5.1986-002	-2.5525-002	3.6985-002
TT25C	-3.4692+000	-2.5291-001	-8.3508-002	1.9175-002	4.8145-002
TT3	1.7992+000	-1.1399-001	6.7226-002	4.8802-001	-2.9342-002
TT4PHI	1.2930-001	-5.2849-003	1.3738-003	1.7642-002	-4.8796-002
TT4PLO	1.7539-002	-6.9121-004	1.8940-004	2.5524-003	-6.5120-003
TT4	3.0790+001	-1.1924+000	4.5059-001	5.8652+000	3.7438-001
TT45M	3.2660+001	7.9428+003	-3.5068-003	-3.5865-002	7.4655-002
TT45LO	1.3232-001	3.2119-003	-1.3923-003	-1.8379-002	-2.9918-002
TT5	2.4494+001	-2.3642-003	-6.5145-003	2.9208-002	-3.2811-002
TT6C	-7.1051-002	5.1419-003	-1.2692-003	-3.4575-002	-2.0313-003
TT7M	-4.9763+000	5.8734-001	4.4291-001	-2.2761+000	1.3087-001

H-MATRIX

	SFAN	SNCM	PTM	PT3	PT5	TT25M	TT25C	TT3	TT4PHI	TT4PLO
FNNX	4.6320-001	-2.1210+000	4.4651+000	9.7181-002	1.0098+000	1.0492+000	-1.4761-001	-1.6146-001	-0.3483-002	-9.2540-002
WFAN	8.9334-001	2.1102-001	-2.7159-001	-7.1151-002	-4.2821-002	-2.3863-001	-7.4979-002	-5.0698-002	-5.0063-002	-5.0405-002
TT4	-0.0000	0.0000	-0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
SM4F	-1.3868+000	5.8901+000	-6.1124+000	-1.5998+000	-9.6314-001	-5.3713+000	-1.6853+000	-1.1419+000	-1.1257+000	-1.1323+000
SM4C	1.3040+001	2.3243+002	1.4922+001	-2.5394+001	2.3723+000	-1.1489+002	4.1414+000	2.8047+000	2.7728+000	2.7825+000
	9.9358-002	-1.6839-002	-5.3172-001	-1.0355-001	-8.4268-002	-1.3633-001	-6.9978-002	-1.0041-001	-9.8537-002	-9.8812-002
	5.2218-002	-3.6325-002	-1.1285-001	-2.0072-002	-1.8000-002	7.2250-003	2.4816-004	-2.1375-002	-2.0951-002	-2.0814-002

H-MATRIX

	TT4	TT45M	TT45LO	TT5	TT6C	TT7M
FNNX	-4.3145-001	-1.0147-001	-1.0006-001	-2.2739-001	-6.0308-002	-9.7494-002
WFAN	-5.2600-002	-5.0442-002	-5.0432-002	-4.8522-002	-5.6095-002	-5.0440-002
TT4	1.0000+000	0.0000	0.0000	0.0000	0.0000	0.0000
SM4F	-1.1403+000	-1.1341+000	-1.1337+000	-1.0925+000	-1.2618+000	-1.1338+000
SM4C	2.9115+000	2.7948+000	2.7826+000	2.8841+000	3.1044+000	2.7882+000
	-1.0375-001	-9.8660-002	-9.8632-002	-9.5050-002	-1.1043-001	-9.8809-002
	-2.2073-002	-2.1044-002	-2.0820-002	-2.0129-002	-2.3622-002	-2.0821-002

F100 LINEAR MODEL 20/0/0K HP/BLD 1/30/76

D-MATRIX	RFM9H	INVTX	CIVV	RCVV	BLC
FMY	4.2953-001	-6.1992-002	-1.8984-002	1.0703-001	-7.6925-003
MFAN	2.1940-001	-1.3993-002	-3.4254-002	2.4849-003	-3.4333-003
TTA	0.0000	0.0000	0.0000	0.0000	0.0000
SWAF	4.5792+000	-3.5861-001	1.0314+000	4.4270-002	-6.4241-002
SWHC	-6.5580+000	1.2107+000	-4.2765-001	-6.3393+000	1.6634-001
	3.8345-001	-3.1530-002	5.2450-003	-2.5666-002	-5.3387-003
	8.2378-002	-6.4080-003	-1.8830-003	6.6768-003	-1.1673-003

F100 LINEAR MODEL 20/0/0K HP/BLD 1/30/76

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-8-27027+0.021+J(-0-0.0000	0-00000	1-00000	1 (-4.57838-003)+J(-0-0.00000	0.045784	00000
			2 (7.65932-004)+J(0-0.00000	0.007659	00000
			3 (-5.02808-003)+J(0-0.00000	0.050281	00000
			4 (-2.44377-002)+J(-0-0.00000	0.024437	00000
			5 (1.00000+000)+J(0-0.00000	1.000000	00000
			6 (-5.87166-004)+J(0-0.00000	0.005872	00000
			7 (-7.53298-004)+J(-0-0.00000	0.007533	00000
			8 (5.38518-004)+J(0-0.00000	0.005385	00000
			9 (-1.86922-004)+J(0-0.00000	0.001869	00000
			10 (-2.46638-005)+J(-0-0.00000	0.000247	00000
			11 (3.23790-003)+J(0-0.00000	0.032379	00000
			12 (-1.59454-002)+J(0-0.00000	0.015945	00000
			13 (-6.35578-003)+J(-0-0.00000	0.006358	00000
			14 (-1.18286-003)+J(0-0.00000	0.001182	00000
			15 (-3.33860-006)+J(0-0.00000	0.000033	00000
			16 (-2.30998-002)+J(-0-0.00000	0.024098	00000
(-1-45045+0.02)+J(-0-0.0000	0-00000	1-00000	1 (-1.4799-002)+J(0-0.00000	0.014799	00000
			2 (-5.49950-003)+J(0-0.00000	0.054995	00000
			3 (-2.41487-002)+J(0-0.00000	0.024148	00000
			4 (-1.00000+000)+J(0-0.00000	1.000000	00000
			5 (5.04628-001)+J(0-0.00000	0.504627	00000
			6 (-8.84310-003)+J(0-0.00000	0.008843	00000
			7 (-1.17910-002)+J(0-0.00000	0.011791	00000
			8 (-3.00947-002)+J(0-0.00000	0.030097	00000
			9 (2.32204-002)+J(0-0.00000	0.023220	00000
			10 (-3.00453-003)+J(0-0.00000	0.003005	00000
			11 (-4.52831-002)+J(0-0.00000	0.045283	00000
			12 (1.00512-001)+J(0-0.00000	0.005120	00000
			13 (-3.93758-002)+J(0-0.00000	0.039376	00000
			14 (5.25187-002)+J(0-0.00000	0.052518	00000
			15 (2.04791-003)+J(0-0.00000	0.002047	00000
			16 (-1.19518-001)+J(0-0.00000	0.011951	00000

(-5.05263+001)+J(1.89791+001) 5.39733+001 .93614			
1	(-1.37110-002)+J(-9.61287-003)	.0167452	-144.96554
2	(-9.88474-003)+J(-2.84046-003)	.0102046	163.96754
3	(-4.07724-002)+J(1.61840-004)	.0407727	179.77286
4	(3.75059-001)+J(-1.32081-001)	.3976362	-19.40026
5	(1.74879-001)+J(-2.56138-002)	.1767450	-8.33282
6	(-4.47126-002)+J(6.69160-005)	.0447127	179.91425
7	(-5.62418-002)+J(6.24412-005)	.0562418	179.91639
8	(-1.27542-003)+J(-1.41813-003)	.0019073	131.96712
9	(5.44617-001)+J(-3.62078-001)	.6539940	-33.61714
10	(6.57101-002)+J(-4.67096-002)	.0806201	-35.40688
11	(1.44271-001)+J(-2.29022-001)	.2706756	57.79141
12	(1.00000+000)+J(0.00000)	1.0000000	.00000
13	(3.78594-001)+J(-8.37815-003)	.3786869	-1.26773
14	(-1.83614-001)+J(-1.59564-001)	.2432585	-40.99139
15	(2.54479-002)+J(1.59809-002)	.0300497	32.12823
16	(-4.71763-001)+J(-6.96623-001)	.8413344	-124.10640

(-5.16767+001)+J(0.00000 0.00000 1.00000			
1	(9.89451-003)+J(0.00000)	.0098945	.00000
2	(-9.05364-004)+J(-0.00000)	.0009054	.00000
3	(1.78376-003)+J(0.00000)	.0017838	.00000
4	(2.47551-003)+J(0.00000)	.0024755	.00000
5	(6.84132-003)+J(0.00000)	.0068414	.00000
6	(7.14764-004)+J(0.00000)	.0007148	.00000
7	(7.99637-004)+J(0.00000)	.0007996	.00000
8	(-1.1566-003)+J(-0.00000)	.0011157	.00000
9	(-8.05470-002)+J(0.00000)	.0805470	.00000
10	(-9.82775-003)+J(0.00000)	.0098278	.00000
11	(-3.10117-003)+J(-0.00000)	.0031012	.00000
12	(-6.91790-001)+J(0.00000)	.6917899	.00000
13	(-2.60039-001)+J(0.00000)	.2600387	.00000
14	(-4.46890-002)+J(-0.00000)	.0446890	.00000
15	(-4.64130-004)+J(0.00000)	.0004641	.00000
16	(1.00000+000)+J(0.00000)	1.0000000	.00000

(-4.41886+001)+J(0.00000 0.00000 1.00000			
1	(1.97053-002)+J(0.00000)	.0197053	.00000
2	(-1.30944-002)+J(-0.00000)	.0130944	.00000
3	(-8.77174-003)+J(0.00000)	.0087717	.00000
4	(3.07629-002)+J(0.00000)	.0307629	.00000
5	(-2.89539-002)+J(-0.00000)	.0289539	.00000
6	(-9.35562-003)+J(0.00000)	.0093556	.00000
7	(-1.17432-002)+J(0.00000)	.0117432	.00000
8	(-7.68750-003)+J(-0.00000)	.0768750	.00000
9	(1.00000+000)+J(0.00000)	1.0000000	.00000
10	(1.20052-001)+J(0.00000)	.1200522	.00000
11	(1.26135-001)+J(0.00000)	.1261352	.00000
12	(-8.78545-001)+J(0.00000)	.8785446	.00000
13	(-3.26485-001)+J(0.00000)	.3264854	.00000
14	(-3.85874-002)+J(-0.00000)	.0385874	.00000
15	(9.57024-003)+J(0.00000)	.0095702	.00000
16	(1.95632-001)+J(0.00000)	.1956317	.00000

(-2.46496+001)+J(3.45418+000) 2.48905+001 .99032				.0184379				-121.28454			
1 (-9.57457-003)+J(-1.57570-002)				.0070736				-86.43691			
2 (-1.93061-004)+J(-7.07499-003)				.2603572				-125.01803			
3 (-1.49402-001)+J(-2.13225-001)				.1878165				-23.46873			
4 (1.72280-001)+J(-7.47976-002)				.1350304				-85.00816			
5 (-1.17502-002)+J(-1.34526-001)				.0543587				169.29047			
6 (-5.34119-002)+J(1.01015-002)				.0643402				173.54783			
7 (-6.39327-002)+J(7.23015-003)				.0650609				37.35162			
8 (-5.17186-002)+J(3.94730-002)				.3132288				115.30414			
9 (-1.33881-001)+J(2.83175-001)				.0343869				113.52273			
10 (-1.37243-002)+J(3.15294-002)				.0739499				124.87775			
11 (-9.94693-002)+J(-1.42704-001)				.2906997				133.38422			
12 (-1.99678-001)+J(2.11270-001)				.1012623				132.08856			
13 (-6.78740-002)+J(7.51478-002)				.5657310				10.82570			
14 (-5.56030-001)+J(-1.04316-001)				.2164324				30.12133			
15 (1.87206-001)+J(1.08613-001)				1.0000000				.00000			
16 (1.00000+000)+J(0.00000)											
(-2.73104+000)+J(1.98987+000) 5.13285+000 .92180				1.0000000				.00000			
1 (1.00000+000)+J(0.00000)				.0299274				-163.95471			
2 (-2.87613-002)+J(-8.27176-003)				.2527838				-23.52558			
3 (2.31773-001)+J(-1.00901-001)				.3030110				127.61436			
4 (-1.84941-001)+J(2.40028-001)				.1360918				-3.68528			
5 (-1.35810-001)+J(-8.74743-003)				.4852087				-32.83065			
6 (4.07710-001)+J(-2.63060-001)				.5947211				-34.27411			
7 (4.91449-001)+J(-3.34919-001)				.2016184				-45.12541			
8 (-1.46062-001)+J(-1.46705-001)				.3444859				-53.69720			
9 (2.03953-001)+J(-2.77621-001)				.0203602				-125.20643			
10 (-1.17381-002)+J(-1.66359-002)				.3215264				-51.50195			
11 (-2.00146-001)+J(-2.51636-001)				.4730184				-49.85814			
12 (3.04947-001)+J(-3.61599-001)				.1122764				-111.37324			
13 (-4.09182-002)+J(-1.04555-001)				.6110912				-53.48490			
14 (3.63620-001)+J(-4.91134-001)				.7635784				-41.96601			
15 (5.61752-001)+J(-5.10597-001)				.5490690				-75.45765			
16 (1.37864-001)+J(-5.31478-001)											
(-6.46340-001)+J(2.17310-001) 7.00880-001 .95072				.8696496				-14.61660			
1 (8.41504-001)+J(-2.19456-001)				.2194273				-73441			
2 (-2.19409-001)+J(-2.81252-003)				.1353843				-11.92358			
3 (1.32463-001)+J(-2.79713-002)				1.0000000				.00000			
4 (1.00000+000)+J(0.00000)				.4991265				-2.16568			
5 (-4.88770-001)+J(-1.88614-002)				.1278916				-6.64152			
6 (1.27033-001)+J(-1.47916-002)				.1331414				-5.77462			
7 (1.32466-001)+J(-1.33961-002)				.2725920				-1.44443			
8 (-2.72505-001)+J(-6.87132-003)				.3087453				-179.15747			
9 (-3.08712-001)+J(-4.53989-003)				.8226672				93.80850			
10 (5.46432-002)+J(8.20850-001)				.3548607				-179.08342			
11 (-3.54815-001)+J(-5.67660-003)				.4414095				-176.00477			
12 (-4.40337-001)+J(-3.07545-002)				.5614734				177.58123			
13 (-5.66962-001)+J(2.39490-002)				.5378205				-176.49181			
14 (-5.36813-001)+J(-3.29098-002)				.1400448				-5.86179			
15 (1.39313-001)+J(-1.43027-002)				.1932328				163.61816			
16 (-1.85388-001)+J(5.44989-002)											

	(-1.99516+0i)+j(0.00000)	0.00000	1.00000	
1	(-2.69940-003)+j(0.00000)			-.0029994
2	(-1.24161-002)+j(0.00000)			-.0012416
3	(-7.61393-002)+j(0.00000)			-.0761393
4	(-1.61053-002)+j(0.00000)			-.0161053
5	(-4.05416-002)+j(0.00000)			-.0405416
6	(-3.79727-003)+j(0.00000)			-.0037973
7	(-2.65048-003)+j(0.00000)			-.0026505
8	(-3.32320-004)+j(0.00000)			-.0003323
9	(-1.90220-002)+j(0.00000)			-.0190220
10	(-1.98869-003)+j(0.00000)			-.0019887
11	(-1.23328-002)+j(0.00000)			-.0123328
12	(-7.25764-003)+j(0.00000)			-.0072576
13	(-2.42445-003)+j(0.00000)			-.0024205
14	(-6.25673-001)+j(0.00000)			-.6256734
15	(-1.00000+000)+j(0.00000)			1.0000000
16	(-1.02920-001)+j(0.00000)			-.0292002

1	(-2.01045+001)+J(0.00000	1.000000	1	(-3.45312-003)+J(0.00000	-0.0034531	.000000
2	(-1.60668-003)+J(0.00000		2	(-1.60668-003)+J(0.00000	-0.0016067	.000000
3	(-8.11269-002)+J(0.00000		3	(-8.11269-002)+J(0.00000	-0.0811269	.000000
4	(-1.43008-002)+J(0.00000		4	(-1.43008-002)+J(0.00000	-0.0143008	.000000
5	(-4.18998-002)+J(0.00000		5	(-4.18998-002)+J(0.00000	-0.0418998	.000000
6	(-3.30452-003)+J(0.00000		6	(-3.30452-003)+J(0.00000	-0.0033045	.000000
7	(-5.09444-003)+J(0.00000		7	(-5.09444-003)+J(0.00000	-0.0050944	.000000
8	(-7.72236-003)+J(0.00000		8	(-7.72236-003)+J(0.00000	-0.0077224	.000000
9	(-3.06583-002)+J(0.00000		9	(-3.06583-002)+J(0.00000	-0.0306583	.000000
10	(-3.17884-003)+J(0.00000		10	(-3.17884-003)+J(0.00000	-0.0031789	.000000
11	(-1.91925-002)+J(0.00000		11	(-1.91925-002)+J(0.00000	-0.0191925	.000000
12	(-1.66741-002)+J(0.00000		12	(-1.66741-002)+J(0.00000	-0.0168741	.000000
13	(-5.63376-003)+J(0.00000		13	(-5.63376-003)+J(0.00000	-0.0056338	.000000
14	(-6.25307-001)+J(0.00000		14	(-6.25307-001)+J(0.00000	-0.6253069	.000000
15	(-1.00000+000)+J(0.00000		15	(-1.00000+000)+J(0.00000	-1.0000000	.000000
16	(-1.03300+001)+J(0.00000		16	(-1.03300+001)+J(0.00000	-0.0033004	.000000

1	(-2.94984-001)+j(0.00000)	--2949839	.00000
2	(-3.58763-003)+j(0.00000)	--358763	.00000
3	(-3.79941-002)+j(0.00000)	--379941	.00000
4	(6.10335-004)+j(0.00000)	--008102	.00000
5	(-1.89081-002)+j(0.00000)	--0189081	.00000
6	(-2.30051-002)+j(0.00000)	--0230051	.00000
7	(-2.12910-002)+j(0.00000)	--0212910	.00000
8	(-6.27963-003)+j(0.00000)	--062796	.00000
9	(-7.59232-003)+j(0.00000)	--075923	.00000
10	(-2.2537-003)+j(0.00000)	--0022554	.00000
11	(-7.3209-003)+j(0.00000)	--073221	.00000
12	(-1.27808-002)+j(0.00000)	--0127808	.00000
13	(1.00000+000)+j(0.00000)	1.0000000	.00000
14	(-3.04126-002)+j(0.00000)	--304126	.00000
15	(-2.20121-002)+j(0.00000)	--0220121	.00000
16	(6.06298-002)+j(0.00000)	--0806298	.00000

1	1.00000	(-2.34137*-002)+J(0.00000)	-0.0344137	0.00000
2	2	(-6.19840*-003)+J(0.00000)	-0.0618849	0.00000
3	3	(-1.31866*-001)+J(0.00000)	-0.1318655	0.00000
4	4	(-1.80889*-001)+J(0.00000)	-1.80889	0.00000
5	5	(-7.50888*-003)+J(0.00000)	-0.077609	0.00000
6	6	(-4.64699*-002)+J(0.00000)	-0.0464699	0.00000
7	7	(-6.04876*-002)+J(0.00000)	-0.0404876	0.00000
8	8	(-2.46066*-001)+J(0.00000)	-2.046056	0.00000
9	9	(-1.66667*-001)+J(0.00000)	-1.666672	0.00000
10	10	(-2.06839*-002)+J(0.00000)	-0.068839	0.00000
11	11	(-1.05484*-001)+J(0.00000)	-1.054842	0.00000
12	12	(-1.0822*-001)+J(0.00000)	-1.08222	0.00000
13	13	(-4.1457*-002)+J(0.00000)	-0.041457	0.00000
14	14	(-7.33331*-001)+J(0.00000)	-7.333310	0.00000
15	15	(-1.00000*-000)+J(0.00000)	-1.000000	0.00000
16	16	(-1.54542*-001)+J(0.00000)	-1.545421	0.00000

-----THE MATRICES IN FINAL FORM-----

PARAMETER	SNFAH	SNCOM	PT7M	WFCOM	FTIT	PT3	PT45	TT25H	TT25C	TT3
SNFAH	-2.3362+000	2.4514+000	-5.0339+000	1.4355+000	0.0000	-4.5957+001	3.7333+000	-2.1423+000	-5.3365+001	-7.2282+001
SNCOM	-2.4132+001	-3.9334+000	-2.7645+001	1.1959+001	0.0000	1.0675+000	-6.0724+001	1.6523+000	-7.4419+002	-1.2219+001
PT7M	2.0219+000	-7.1526+000	-2.0440+001	-2.5989+002	0.0000	7.6268+001	4.0757+000	4.1277+000	-1.8154+001	-1.6422+001
WFCOM	0.0000	0.0000	0.0000	-1.0000+001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
FTIT	0.0000	0.0000	0.0000	0.0000	-2.5000+001	0.0000	0.0000	0.0000	0.0000	0.0000
PT3	7.1272+001	6.8293+002	8.1742+001	-4.6160+001	0.0000	-1.4927+002	1.7082+001	-3.6511+002	2.2081+001	4.3774+001
PT45	4.7676+001	4.0322+001	4.155+002	-5.6106+001	0.0000	3.5524+002	-8.1571+002	-6.0226+001	1.5886+001	-2.7019+000
TT25H	2.7762+000	-3.4715+000	3.6711+000	-2.5757+000	0.0000	9.5161+001	5.6236+001	-1.6746+001	1.0015+000	1.2264+000
TT25C	2.7732+000	-5.4773+000	4.0530+000	-3.4675+000	0.0000	1.2663+000	7.1860+001	4.7058+000	-1.8763+001	1.5177+000
TT3	-2.0256+000	1.8745+000	-2.3218+000	1.7841+000	0.0000	4.0546+000	-3.6631+001	1.7387+001	-6.4140+001	-2.0782+001
TT45H	-1.8373+002	-1.8669+001	-5.0070+002	1.2849+001	0.0000	-2.5026+002	-6.6726+003	1.7688+001	-1.6687+002	4.0764+000
TT45C	-1.3972+001	-1.2653+002	-1.5911+001	3.0712+001	0.0000	5.7915+000	-2.5278+000	7.1744+001	-4.4109+000	1.6064+001
TT5	-0.4043+002	-1.2204+000	1.0176+001	-2.9557+001	0.0000	-1.2084+001	1.1894+001	-3.5599+001	3.525+002	7.0851+000
TT6C	3.8417+002	4.8959+001	4.0264+002	1.1012+001	0.0000	-4.9948+000	4.7584+000	-1.4249+001	1.4205+002	2.8346+000
TT7M	1.5222+001	1.04173+000	4.1470+000	2.7862+001	0.0000	-5.3840+000	7.3972+001	3.3550+001	-3.1680+002	3.0077+000
TT6C	-3.1475+002	6.8076+001	1.0790+001	-7.0685+002	0.0000	-2.4471+002	1.7404+002	-3.4103+001	1.9902+001	-1.4901+001
TT7M	-1.0718+001	4.7411+001	1.6823+000	-6.9253+000	0.0000	-8.4250+002	1.8769+001	-2.3332+001	2.6157+000	2.8433+000

F-MATRIX

PARAMETER	TT45H	TT4	TT45H	TT45C	TT5	TT6C	TT7M
SNFAH	2.9236+000	-0.0992+000	3.6264+001	-2.8396+001	-1.7037+001	-4.3675+001	-3.6660+001
SNCOM	3.6444+001	-1.9055+001	-4.0760+002	-0.9239+002	-2.7107+002	-5.5122+002	-4.9769+002
PT7M	1.9720+001	-1.1604+000	-1.4857+002	-1.8666+002	1.1884+000	5.6790+001	-3.1644+002
WFCOM	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
FTIT	0.0000	0.0000	1.2895+001	1.4328+002	0.0000	0.0000	0.0000
PT3	-1.1705+002	1.2467+002	1.4711+001	1.4624+001	1.4080+001	1.6443+001	1.8703+001
PT45	-1.1716+002	2.2378+002	1.4799+001	1.4787+001	1.6935+001	1.9212+001	1.4789+001
TT25H	-5.3435+000	6.8144+000	6.7851+001	6.6740+001	6.4482+001	7.4907+001	6.6762+001
TT25C	-6.6015+000	8.4362+000	8.3785+001	8.3509+001	8.0694+001	9.2447+001	8.3527+001
TT3	3.4540+000	-4.4077+000	-4.3406+001	-4.3133+001	-4.1614+001	-4.7976+001	-4.3043+001
TT45H	-4.9905+001	4.5740+001	-5.0937+003	1.1281+002	-1.3309+002	-1.0012+002	1.0013+002
TT45C	-3.2714+001	-7.4074+001	-2.9830+000	-2.9010+000	-1.8582+000	-3.3067+000	-2.9748+000
TT5	-3.2872+001	4.6927+001	-4.0246+001	4.4001+002	2.7349+002	2.6601+002	3.7488+002
TT6C	-1.3320+001	1.4774+001	-1.7981+001	-1.9828+001	1.0744+002	1.0465+002	1.5171+002
TT7M	1.0130+001	2.0000+001	-1.3042+000	1.5892+001	-1.9998+001	1.9677+002	-1.5575+002
TT6C	-1.0601+001	1.4332+001	-2.0488+002	1.3905+002	-3.0544+002	-1.9980+001	1.9136+002
TT7M	-1.4588+001	1.4513+001	1.8307+000	1.8395+000	3.4546+001	1.9675+001	-4.8174+001

F100 LINEAR MODEL 2070/OK HP/BLD 1/30/76

G-MATPIX

	MEMPH	AMIX	CIVV	RCVV	RLC
SNFAN	0.0000	-1.1474-001	6.8380-002	-1.2525-002	-1.5325-002
SNCOM	0.0000	-2.1557-002	7.7772-003	1.3279-001	-2.0965-004
PT7M	0.0000	-3.4195+000	-9.2590-002	3.0343-001	4.5000-003
WFCOM	1.0000+001	0.0000	0.0000	0.0000	0.0000
FTIT	0.0000	0.0000	0.0000	0.0000	0.0000
PT3	0.0000	5.1089+000	-2.3271+000	-3.0156+001	-1.6144+000
PT45	0.0000	4.5377+000	-2.0692+000	-3.4313+000	1.0257+000
TT25H	0.0000	2.1197-001	-5.3795-002	-2.2171-002	3.0467-002
TT25C	0.0000	2.6208-001	-8.3274-002	-2.2085-002	4.0090-002
TT3	0.0000	-1.1354-001	6.7104-002	4.8650-001	-2.5129-002
TT4PHI	0.0000	-5.2748-003	1.3705-003	1.7601-002	4.8682-002
TT4	0.0000	-1.1893+000	4.4375-001	5.8508+000	4.0333-001
TT45HI	0.0000	9.2457+003	-3.8255-003	-0.0285-002	-4.2391-002
TT45LC	0.0000	3.7328-003	-1.5349-003	-1.6151-002	-2.5015-002
TT5	0.0000	-7.7731-003	-4.6777-003	-2.7161-002	-2.7200-002
TT6C	0.0000	5.1275-003	1.2732-003	-3.4526-002	1.8954-003
TT7M	0.0000	5.2534+001	4.4340-001	-2.2693+000	1.1195-001

H-MATPIX

	SNFAN	SNCOM	PT7M	WFCOM	FTIT	PT3	PT45	TT25H	TT25C	TT3
FNMX	4.4458-001	-2.1182+000	4.4460+000	4.2710-001	0.0000	9.7654+002	1.0099+000	1.0459+000	-1.4730-001	-2.3688-001
MFAN	4.9374-001	2.1291+001	-2.7109-001	2.1708-001	0.0000	-7.0894+002	-4.2745-002	-2.4042-001	-7.4813-002	-9.1778-002
TT4	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
SV4F	-1.3780+000	5.4326+000	-6.1012+000	4.5095+000	0.0000	-1.5941+000	-9.6144-001	-5.4114+000	-1.6815+000	-2.0647+000
SMHC	1.3018+001	2.3232+002	1.4894+001	-6.4609+000	0.0000	-2.5408+001	-2.3681+000	-1.1479+002	4.1322+000	-5.0724+000
DP2GT	1.0013-001	-1.1125+002	-5.5374-001	3.8054-001	0.0000	-1.0304-001	-8.4120-002	-1.3983-001	-6.9652-002	-1.8094-001
DP25C	5.2340-002	-3.8544+002	-1.1244-001	8.1242-002	0.0000	-1.9966-002	-1.7969-002	6.4875+003	3.1692-004	-3.8338-002

H-MATPIX

	TT4PHI	TT4	TT45HI	TT45LC	TT5	TT6C	TT7M
FNMX	7.8750-001	-1.2783+000	-1.0175-001	-9.9834+002	2.2744-001	6.0502-002	-9.7301-002
MFAN	4.0256-001	-5.1345-001	-5.0422-002	-5.0311-002	-4.8386-002	-5.5989-002	-5.0334-002
TT4	0.0000	1.0000+000	0.0000	0.0000	0.0000	0.0000	0.0000
SV4F	9.0420+000	-1.1546+001	-1.1347+000	-1.1304+000	-1.0894+000	-1.2595+000	-1.1314+000
SMHC	-2.2213+001	2.4473+001	2.7915+000	2.7759+000	2.6769+000	3.0985+000	2.7824+000
DP2GT	7.8877-001	-1.1080+000	-9.8541-002	-9.5995-002	-2.4783-002	-1.1022-001	-9.8602-002
DP25C	1.6595-001	-2.1254+001	-2.0779-002	-2.0770-002	-2.0073-002	-2.3579-002	-2.0777-002

FI00 LINEAR MODEL 20/0/0K HP/BLD 1/30/76

DATAPIX	NEVPH	ANIX	CTIV	RCVV	BLC
FMY	0.000	-1.1598-002	-1.4990-002	1.0670-001	-6.7908-003
FEAN	0.000	-1.3641-002	-3.4249-002	2.3074-003	-2.9422-003
FTB	0.000	0.0000	0.0000	0.0000	0.0000
SWAF	0.000	-1.5500-001	1.0311+000	4.0285-002	-5.3208-002
SWUC	0.000	1.2079+000	-4.2686-001	-4.3295+000	1.3233-001
DS25G	0.000	-3.1428-002	5.2170-003	2.5515-002	-4.3759-003
DS25C	0.000	-4.3845-003	-1.6889-003	6.5035-003	-9.6448-004

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-2.50000-001)+J(0.00000	0.00000	1.00000	1 (0.00000)+J(0.00000)	.0000000	.00000
			2 (0.00000)+J(0.00000)	.0000000	.00000
			3 (0.00000)+J(0.00000)	.0000000	.00000
			4 (0.00000)+J(0.00000)	.0000000	.00000
			5 (1.00000+000)+J(0.00000)	1.0000000	.00000
			6 (0.00000)+J(0.00000)	.0000000	.00000
			7 (0.00000)+J(0.00000)	.0000000	.00000
			8 (0.00000)+J(0.00000)	.0000000	.00000
			9 (0.00000)+J(0.00000)	.0000000	.00000
			10 (0.00000)+J(0.00000)	.0000000	.00000
			11 (0.00000)+J(0.00000)	.0000000	.00000
			12 (0.00000)+J(0.00000)	.0000000	.00000
			13 (0.00000)+J(0.00000)	.0000000	.00000
			14 (0.00000)+J(0.00000)	.0000000	.00000
			15 (0.00000)+J(0.00000)	.0000000	.00000
			16 (0.00000)+J(0.00000)	.0000000	.00000
			17 (0.00000)+J(0.00000)	.0000000	.00000
(-8.24967+002)+J(0.00000	0.00000	1.00000	1 (-4.56539-003)+J(0.00000)	.0043654	.00000
			2 (7.66645-004)+J(0.00000)	.0007666	.00000
			3 (-5.02777-003)+J(-0.00000)	-.0050278	.00000
			4 (0.00000)+J(0.00000)	.0000000	.00000
			5 (2.59271-006)+J(0.00000)	.0000026	.00000
			6 (-2.51521-002)+J(-0.00000)	-.0251521	.00000
			7 (1.00000+000)+J(0.00000)	1.0000000	.00000
			8 (-6.12719-004)+J(0.00000)	-.0006127	.00000
			9 (-7.84764-004)+J(-0.00000)	-.0007848	.00000
			10 (5.59808-004)+J(0.00000)	.0003598	.00000
			11 (-1.94212-004)+J(0.00000)	-.0001942	.00000
			12 (-3.36705-003)+J(-0.00000)	-.0033671	.00000
			13 (-1.59167-002)+J(0.00000)	-.0159167	.00000
			14 (-6.34433-003)+J(0.00000)	-.0063433	.00000
			15 (-1.16616-003)+J(-0.00000)	-.0011692	.00000
			16 (-3.15621-006)+J(0.00000)	-.0000032	.00000
			17 (-2.41615-002)+J(0.00000)	-.0241615	.00000

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(-1.60813+002)+J( 0.00000 ) 0.00000 1.00000
1 (-1.21372-002)+J( 0.00000 ) -.0121372 .00000
2 (-5.33031-003)+J( 0.00000 ) -.0050303 .00000
3 (-2.15929-002)+J( 0.00000 ) -.0215929 .00000
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 (-7.33392-005)+J( 0.00000 ) .0000739 .00000
6 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
7 ( 5.00975-001)+J( 0.00000 ) .5009746 .00000
8 (-3.90078-003)+J( 0.00000 ) -.0390068 .00000
9 (-5.61340-003)+J( 0.00000 ) -.0561340 .00000
10 (-3.01923-002)+J( 0.00000 ) -.0301923 .00000
11 ( 2.80368-002)+J( 0.00000 ) .0280368 .00000
12 (-6.46758-002)+J( 0.00000 ) -.0646758 .00000
13 ( 8.82138-002)+J( 0.00000 ) .0882138 .00000
14 ( 3.04628-002)+J( 0.00000 ) .0304628 .00000
15 ( 4.68669-002)+J( 0.00000 ) .0468669 .00000
16 ( 1.05927-003)+J( 0.00000 ) .0010593 .00000
17 (-8.59446-002)+J( 0.00000 ) -.0859446 .00000
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(-8.44642+001)+J( 0.00000 ) 0.00000 1.00000
1 (-8.24416-003)+J( 0.00000 ) -.0024416 .00000
2 (-7.34545-003)+J( 0.00000 ) -.0073455 .00000
3 (-4.39256-002)+J( 0.00000 ) -.0439256 .00000
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 ( 8.93800-005)+J( 0.00000 ) .0000894 .00000
6 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
7 ( 5.38581-001)+J( 0.00000 ) .5385810 .00000
8 (-4.50373-002)+J( 0.00000 ) -.0450373 .00000
9 (-5.69612-002)+J( 0.00000 ) -.0569612 .00000
10 (-2.98701-002)+J( 0.00000 ) -.0298701 .00000
11 (-2.25575-001)+J( 0.00000 ) -.2255758 .00000
12 ( 1.73622-001)+J( 0.00000 ) .1736216 .00000
13 (-5.99738-002)+J( 0.00000 ) -.0599738 .00000
14 (-2.15766-002)+J( 0.00000 ) -.0215766 .00000
15 ( 2.68026-002)+J( 0.00000 ) .0268026 .00000
16 ( 1.70834-002)+J( 0.00000 ) .0170834 .00000
17 (-4.80178-001)+J( 0.00000 ) -.4801783 .00000
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(-4.97729+001)+J(0.00000	1.00000	1.00000	1	(-2.05857-003)+J(0.00000)	-0.0020586	.00000
(-1.01916-006)+J(0.00000			2	(-1.01916-006)+J(0.00000)	-0.0000014	.00000
(4.06970-005)+J(0.00000			3	(4.06970-005)+J(0.00000)	.0000407	.00000
(0.00000			4	(0.00000)	.0000000	.00000
(-3.56219-004)+J(0.00000			5	(-3.56219-004)+J(0.00000)	-0.0003562	.00000
(3.20360-004)+J(0.00000			6	(3.20360-004)+J(0.00000)	.0003504	.00000
(4.27292-004)+J(0.00000			7	(4.27292-004)+J(0.00000)	.0004879	.00000
(-1.31366-005)+J(0.00000			8	(-1.31366-005)+J(0.00000)	-0.000131	.00000
(-3.86436-004)+J(0.00000			9	(-3.86436-004)+J(0.00000)	-0.0003864	.00000
(-1.50560-004)+J(0.00000			10	(-1.50560-004)+J(0.00000)	-0.0001506	.00000
(-1.48382-001)+J(0.00000			11	(-1.48382-001)+J(0.00000)	-1.483815	.00000
(6.87184-004)+J(0.00000			12	(6.87184-004)+J(0.00000)	.0006872	.00000
(1.31329-001)+J(0.00000			13	(1.31329-001)+J(0.00000)	.1313266	.00000
(4.92402-002)+J(0.00000			14	(4.92402-002)+J(0.00000)	.0492402	.00000
(5.44834-003)+J(0.00000			15	(5.44834-003)+J(0.00000)	.005483	.00000
(1.92269-005)+J(0.00000			16	(1.92269-005)+J(0.00000)	.0000192	.00000
(-1.00000+000)+J(0.00000			17	(-1.00000+000)+J(0.00000)	-1.0000000	.00000
(-4.95660+001)+J(0.00000	0.00000	1.00000	1	(-3.01015-004)+J(0.00000)	-0.003010	.00000
(5.48967-006)+J(0.00000			2	(5.48967-006)+J(0.00000)	.0000055	.00000
(1.87623-004)+J(0.00000			3	(1.87623-004)+J(0.00000)	.0001876	.00000
(-0.00000			4	(-0.00000)	.0000000	.00000
(-5.19339-005)+J(0.00000			5	(-5.19339-005)+J(0.00000)	-0.0000516	.00000
(8.47742-005)+J(0.00000			6	(8.47742-005)+J(0.00000)	.0000848	.00000
(2.77445-004)+J(0.00000			7	(2.77445-004)+J(0.00000)	.0002775	.00000
(6.22571-005)+J(0.00000			8	(6.22571-005)+J(0.00000)	.0000623	.00000
(-2.80591-004)+J(0.00000			9	(-2.80591-004)+J(0.00000)	-0.0002806	.00000
(-1.35683-004)+J(0.00000			10	(-1.35683-004)+J(0.00000)	-0.0001367	.00000
(1.26768-001)+J(0.00000			11	(1.26768-001)+J(0.00000)	.1267676	.00000
(6.26109-005)+J(0.00000			12	(6.26109-005)+J(0.00000)	.0000626	.00000
(1.01037-002)+J(0.00000			13	(1.01037-002)+J(0.00000)	.0191097	.00000
(7.16753-003)+J(0.00000			14	(7.16753-003)+J(0.00000)	.0071675	.00000
(9.09183-004)+J(0.00000			15	(9.09183-004)+J(0.00000)	.0009092	.00000
(-1.41442-005)+J(0.00000			16	(-1.41442-005)+J(0.00000)	-0.000142	.00000
(1.00000+000)+J(0.00000			17	(1.00000+000)+J(0.00000)	1.0000000	.00000

(-4.97729+001)+J(0.00000)	0.00000	1.00000	1	(-2.05857-003)+J(0.00000)	-0.0020586	0.00000
			2	(-1.41916-006)+J(0.00000)	-0.0000014	0.00000
			3	(4.06970-005)+J(0.00000)	0.0000047	0.00000
			4	(0.00000)+J(0.00000)	0.0000000	0.00000
			5	(-3.56219-004)+J(0.00000)	-0.0003562	0.00000
			6	(3.80360-004)+J(0.00000)	0.0003804	0.00000
			7	(4.87842-004)+J(0.00000)	0.0004874	0.00000
			8	(1.31366-005)+J(0.00000)	0.0000131	0.00000
			9	(-3.86436-004)+J(0.00000)	-0.0003864	0.00000
			10	(-1.50580-004)+J(0.00000)	-0.0001506	0.00000
			11	(-1.48382-001)+J(0.00000)	-0.0000000	0.00000
			12	(6.87184-004)+J(0.00000)	0.0006872	0.00000
			13	(1.31329-001)+J(0.00000)	0.0000000	0.00000
			14	(4.92402-002)+J(0.00000)	0.0492402	0.00000
			15	(5.44834-003)+J(0.00000)	0.0054833	0.00000
			16	(1.92265-005)+J(0.00000)	0.0000192	0.00000
			17	(1.00000+000)+J(0.00000)	1.0000000	0.00000

(-4.98660+001)+J(0.00000)	0.00000	1.00000	1	(-3.01015-004)+J(0.00000)	-0.0003010	0.00000
			2	(5.48967-006)+J(0.00000)	0.0000055	0.00000
			3	(1.87623-004)+J(0.00000)	0.0001876	0.00000
			4	(0.00000)+J(0.00000)	0.0000000	0.00000
			5	(-5.16329-005)+J(0.00000)	-0.0000516	0.00000
			6	(8.47799-005)+J(0.00000)	0.0000848	0.00000
			7	(-2.77495-004)+J(0.00000)	-0.002775	0.00000
			8	(6.22571-005)+J(0.00000)	0.0000623	0.00000
			9	(-2.80591-004)+J(0.00000)	-0.0002806	0.00000
			10	(-1.36683-004)+J(0.00000)	-0.0001367	0.00000
			11	(1.28768-001)+J(0.00000)	0.0000000	0.00000
			12	(6.26109-005)+J(0.00000)	0.0000628	0.00000
			13	(-1.91097-002)+J(0.00000)	-0.0191097	0.00000
			14	(7.14753-003)+J(0.00000)	0.0071475	0.00000
			15	(9.04183-004)+J(0.00000)	0.0009042	0.00000
			16	(-1.41642-005)+J(0.00000)	-0.0000142	0.00000
			17	(1.00000+000)+J(0.00000)	1.0000000	0.00000

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(-7.19412-001)+J( 0.00000 ) 0.00000 1.00000
1 ( 9.13147-001)+J( 0.00000 ) 9131474 .00000
2 (-2.18544-001)+J( 0.00000 ) 2185436 .00000
3 ( 1.42690-001)+J( 0.00000 ) 1426896 .00000
4 ( 0.00000 )+J( 0.00000 ) 0000000 .00000
5 (-1.35817-001)+J( 0.00000 ) 1358166 .00000
6 ( 1.00000+000)+J( 0.00000 ) 1000000 .00000
7 ( 5.06279-001)+J( 0.00000 ) 5062792 .00000
8 (-1.35462-001)+J( 0.00000 ) 1354617 .00000
9 ( 1.41374-001)+J( 0.00000 ) 1413743 .00000
10 ( 2.75937-001)+J( 0.00000 ) 2759367 .00000
11 (-3.06337-001)+J( 0.00000 ) 3063369 .00000
12 (-3.52246-001)+J( 0.00000 ) 3522455 .00000
13 (-4.30381-001)+J( 0.00000 ) 4303811 .00000
14 (-5.76077-001)+J( 0.00000 ) 5760765 .00000
15 (-5.25689-001)+J( 0.00000 ) 5256891 .00000
16 ( 1.48716-001)+J( 0.00000 ) 1487163 .00000
17 (-1.99575-001)+J( 0.00000 ) 1995750 .00000
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(-2.01574+000)+J( 0.00000 ) 0.00000 1.00000
1 (-2.91327-001)+J( 0.00000 ) 2913268 .00000
2 ( 3.81992-003)+J( 0.00000 ) 0381999 .00000
3 (-3.74032-002)+J( 0.00000 ) 0374032 .00000
4 ( 0.00000 )+J( 0.00000 ) 0000000 .00000
5 (-7.17630-003)+J( 0.00000 ) 0071763 .00000
6 ( 1.98306-003)+J( 0.00000 ) 0198306 .00000
7 (-1.79807-002)+J( 0.00000 ) 0179807 .00000
8 (-2.23738-002)+J( 0.00000 ) 0237338 .00000
9 (-2.05907-002)+J( 0.00000 ) 0205907 .00000
10 (-5.75483-003)+J( 0.00000 ) 0057548 .00000
11 (-7.74554-003)+J( 0.00000 ) 0077455 .00000
12 (-7.58106-003)+J( 0.00000 ) 0075811 .00000
13 (-1.28484-002)+J( 0.00000 ) 0128484 .00000
14 ( 1.00000+000)+J( 0.00000 ) 1000000 .00000
15 (-3.03376-002)+J( 0.00000 ) 0303376 .00000
16 (-2.12462-002)+J( 0.00000 ) 0212462 .00000
17 ( 8.00691-002)+J( 0.00000 ) 0800691 .00000
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CASE 8

G-MATRIX

	ANVX	CIVV	RCVV	ELC
SNFAN	-1.069-001	-6.0036-003	5.0692-004	-6.1482-002
SNCOM	-7.9120-002	4.5182-004	-8.0327-003	-6.0167-001
PT7M	-5.7598+000	4.0296-003	-3.0673-002	-5.1668+000
SNFV	1.0000+001	0.0000	0.0000	0.0000
PT3	1.0000	0.0000	1.6771-001	-2.5908+002
PT7T	0.0000	0.0000	0.0000	0.0000
PT5	-1.7549+001	2.5555-001	8.1839-001	1.8603+002
TT25H	1.1845-001	1.0602-002	-9.9947-003	-1.8875+000
TT25C	1.6912+000	1.2177-002	-1.9459-002	-4.3247+000
TT3	-2.2200-001	3.2202-003	4.3685-002	3.6583+000
TT25H	-5.5204-003	1.2723-004	-4.9786-005	-2.5623+000
TT25C	-1.1786-003	1.7004-005	-5.5367-006	-3.4169-001
TT4	-1.0484+000	1.8483-002	-1.3687-002	4.5346+001
TT5H	-1.4201-002	3.8204-004	-3.2185-004	-3.1511+000
TT5C	-1.5046-003	1.5184-004	-1.3417-004	-1.2812+000
TT5	1.4766-001	3.0039-004	-5.3606-004	-1.0842+000
TT6C	4.3109-002	-1.5189-003	3.3408-004	-2.8728-001
TT7M	1.4450+000	-8.4168-002	-6.2025-003	-1.2951+001

H-MATRIX

	SNFAN	SNCOM	PT7M	WFCOM	PT3	FTIT	PT45	TT25H	TT25C	TT3
FNMY	1.3356-001	-9.4178-001	-2.9354+001	1.5242-001	1.7882-001	0.0000	9.8684-001	8.2433-001	3.2341-002	-1.1159-001
KNAN	4.4261-001	4.7883-004	-2.8635-003	5.9545-003	5.0213-004	0.0000	7.0304-004	3.2642-004	8.7877-004	7.0305-004
TT4	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
SNFV	1.2019+001	1.0189+000	-3.4753+000	-1.4264+000	5.4904-001	0.0000	6.4314-001	1.9417-001	9.9227-001	5.8931-001
SNFV	4.6162-001	8.5207+000	3.5744+000	4.1187+000	-6.3923+000	0.0000	-6.7607-001	-5.7289+000	-1.0511+000	-6.1813-001
DP25T	2.5233-001	-6.6340-001	-5.4935-001	-5.9262-001	1.3313-001	0.0000	1.0343-001	4.2660-001	2.5272-001	5.4249-002
DP25C	1.1754-001	8.3346-002	-1.4205-001	-1.4845-001	1.8636-002	0.0000	2.6376-002	5.2560-002	8.1500-002	2.4190-002

H-MATRIX

	TT45H	TT45L	TT5	TT6C	TT7M
FNMY	1.0458-001	-1.2919-002	-6.1744-001	-2.8185-002	6.1548-001
KNAN	7.0301-004	7.0305-004	5.0218-004	7.0312-004	7.0307-004
TT4	0.0000	0.0000	0.0000	0.0000	0.0000
SNFV	5.9326-001	5.9563-001	5.9359-001	5.9233-001	5.9561-001
SNFV	-6.2486-001	-6.2534-001	-6.2481-001	-6.2446-001	-6.2539-001
DP25T	9.5727-002	9.5370-002	9.5397-002	9.5514-002	9.5368-002
DP25C	2.4539-002	2.4547-002	2.4534-002	2.4535-002	2.4586-002

F100 LINEAR MODEL 83/9/30X 2/18/76

D-MATRIX		ANMIX	CTVV	RCVV	RLC
ENMX	0.0000	6.2582-002	1.1522-003	-2.9477-003	-3.7528-002
WFAN	0.0000	6.1253-003	2.9064-003	9.8651-006	3.8022-003
TYA	0.0000	0.0000	0.0000	0.0000	0.0000
SMF	0.0000	-4.2075-001	2.8443-002	1.4415-002	3.3477+000
SMC	0.0000	4.7943-001	-4.1756-003	-4.1831-002	-4.1033+000
DPSEGT	0.0000	-6.0676-002	2.1110-003	1.2060-003	5.8050-001
DPSSC	0.0000	-7.3145-003	7.7960-004	7.1160-004	1.4300-001

F100 LINEAR MODEL RTA/9/30X 2/18/76

EIGENVALUE		NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR		MAGNITUDE	PHASE (DEG)
-----		-----	-----	-----		-----	-----
(-2.50000-001)+J(0.00000)		0.00000	1.00000	1 (0.00000)	J(0.00000)	.0000000	.00000
				2 (0.00000)	J(0.00000)	.0000000	.00000
				3 (0.00000)	J(0.00000)	.0000000	.00000
				4 (0.00000)	J(0.00000)	.0000000	.00000
				5 (0.00000)	J(0.00000)	.0000000	.00000
				6 (1.00000+000)+J(0.00000)		1.0000000	.00000
				7 (0.00000)	J(0.00000)	.0000000	.00000
				8 (0.00000)	J(0.00000)	.0000000	.00000
				9 (0.00000)	J(0.00000)	.0000000	.00000
				10 (0.00000)	J(0.00000)	.0000000	.00000
				11 (0.00000)	J(0.00000)	.0000000	.00000
				12 (0.00000)	J(0.00000)	.0000000	.00000
				13 (0.00000)	J(0.00000)	.0000000	.00000
				14 (0.00000)	J(0.00000)	.0000000	.00000
				15 (0.00000)	J(0.00000)	.0000000	.00000
				16 (0.00000)	J(0.00000)	.0000000	.00000
				17 (0.00000)	J(0.00000)	.0000000	.00000
				18 (0.00000)	J(0.00000)	.0000000	.00000
(-5.14312+002)+J(0.00000)		0.00000	1.00000	1 (-4.13617-003)+J(0.00000)		-.0041362	.00000
				2 (1.57287-003)+J(0.00000)		.0015729	.00000
				3 (-8.50266-003)+J(0.00000)		-.005027	.00000
				4 (0.00000)	J(0.00000)	.0000000	.00000
				5 (4.51701-002)+J(0.00000)		.0451701	.00000
				6 (9.10761-006)+J(0.00000)		.0000091	.00000
				7 (1.00000+000)+J(0.00000)		1.0000000	.00000
				8 (1.36257-003)+J(0.00000)		.0013626	.00000
				9 (8.38037-004)+J(0.00000)		.0008380	.00000
				10 (-1.50084-003)+J(0.00000)		-.0015408	.00000
				11 (6.19340-004)+J(0.00000)		.0006193	.00000
				12 (8.18446-005)+J(0.00000)		.0000618	.00000
				13 (-5.72103-003)+J(0.00000)		-.0057210	.00000
				14 (-2.06807-002)+J(0.00000)		-.0206807	.00000
				15 (8.28166-003)+J(0.00000)		.0082817	.00000
				16 (-1.62118-003)+J(0.00000)		-.0016232	.00000
				17 (8.51025-005)+J(0.00000)		.0000881	.00000
				18 (-1.27950-002)+J(0.00000)		-.0127959	.00000

1	(-1.9568-002)+J(0.0000)	-0.109568	0.0000
2	(-2.42705-003)+J(0.0000)	-0.024270	0.0000
3	(-1.71745-002)+J(0.0000)	-0.171745	0.0000
4	(0.0000)+J(0.0000)	0.000000	0.0000
5	(6.53856-001)+J(0.0000)	6.538556	0.0000
6	(6.6364-003)+J(0.0000)	0.000066	0.0000
7	(1.0000+000)+J(0.0000)	1.000000	0.0000
8	(5.8734-003)+J(0.0000)	0.058673	0.0000
9	(3.57003-003)+J(0.0000)	0.035700	0.0000
10	(-2.64146-002)+J(0.0000)	-0.026414	0.0000
11	(1.26162-002)+J(0.0000)	0.126162	0.0000
12	(1.6644-003)+J(0.0000)	0.016644	0.0000
13	(-4.2671-002)+J(0.0000)	-0.426710	0.0000
14	(-5.9703-003)+J(0.0000)	-0.059970	0.0000
15	(-2.35639-003)+J(0.0000)	-0.023564	0.0000
16	(1.2117-002)+J(0.0000)	0.182117	0.0000
17	(3.45173-004)+J(0.0000)	0.003652	0.0000
18	(-3.16488-002)+J(0.0000)	-0.031648	0.0000
1	(-7.04941-003)+J(0.0000)	-0.070494	0.0000
2	(-8.31022-003)+J(0.0000)	-0.083102	0.0000
3	(2.42452-002)+J(0.0000)	0.024245	0.0000
4	(0.0000)+J(0.0000)	0.000000	0.0000
5	(-2.39612-001)+J(0.0000)	-0.239612	0.0000
6	(-3.47118-003)+J(0.0000)	-0.034712	0.0000
7	(-2.89934-001)+J(0.0000)	-0.289936	0.0000
8	(1.46297-002)+J(0.0000)	0.146297	0.0000
9	(3.16411-003)+J(0.0000)	0.031641	0.0000
10	(9.5769-003)+J(0.0000)	0.095770	0.0000
11	(4.55064-001)+J(0.0000)	4.550639	0.0000
12	(5.8095-002)+J(0.0000)	0.586095	0.0000
13	(-1.53083-001)+J(0.0000)	-0.153082	0.0000
14	(1.0000+000)+J(0.0000)	1.000000	0.0000
15	(3.81051-001)+J(0.0000)	3.810613	0.0000
16	(2.15644-001)+J(0.0000)	2.156836	0.0000
17	(-1.74653-004)+J(0.0000)	-0.001797	0.0000
18	(-3.23428-001)+J(0.0000)	-0.323428	0.0000

```
(-5.33409+001)+J( 0.00000 ) 0.00000 1.00000
1 ( 1.01808-002)+J( 0.00000 ) .0101808
2 ( 2.72255-003)+J( 0.00000 ) .0027226
3 ( 5.5232-003)+J( 0.00000 ) .005523
4 ( 0.00000 )+J( 0.00000 ) .0000000
5 ( 8.21504-003)+J( 0.00000 ) .0082150
6 ( 2.40182-003)+J( 0.00000 ) .0024018
7 ( 3.17267-002)+J( 0.00000 ) .0317267
8 (-2.5773-003)+J( 0.00000 ) -.0025773
9 (-2.84758-003)+J( 0.00000 ) -.0028476
10 (-1.32364-003)+J( 0.00000 ) -.0013236
11 (-9.65241-002)+J( 0.00000 ) -.0965241
12 (-1.15107-002)+J( 0.00000 ) -.0115107
13 ( 7.11395-003)+J( 0.00000 ) .0071140
14 (-5.64513-001)+J( 0.00000 ) -.5645128
15 (-2.12618-001)+J( 0.00000 ) -.2126181
16 (-8.26582-002)+J( 0.00000 ) -.0826582
17 ( 1.75818-003)+J( 0.00000 ) .0017582
18 ( 1.00000+000)+J( 0.00000 ) 1.0000000
```

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(-4.34117+001)+J( 0.00000 ) 0.00000 1.00000
1 ( 2.16693-002)+J( 0.00000 ) .0216693
2 (-3.11870-002)+J( 0.00000 ) -.0311870
3 (-3.48061-003)+J( 0.00000 ) -.0034806
4 ( 0.00000 )+J( 0.00000 ) .0000000
5 ( 3.34034-002)+J( 0.00000 ) .0334034
6 ( 4.22392-003)+J( 0.00000 ) .0042239
7 (-6.56857-002)+J( 0.00000 ) -.0656857
8 (-1.28638-002)+J( 0.00000 ) -.0128638
9 (-9.29780-003)+J( 0.00000 ) -.0092978
10 ( 1.43801-002)+J( 0.00000 ) .0143801
11 ( 1.00000+000)+J( 0.00000 ) 1.0000000
12 ( 1.19826-001)+J( 0.00000 ) .1198264
13 ( 1.42091-001)+J( 0.00000 ) .1420912
14 (-8.07583-001)+J( 0.00000 ) -.8075833
15 (-2.99646-001)+J( 0.00000 ) -.2996436
16 (-1.65139-002)+J( 0.00000 ) -.0165139
17 ( 7.76791-003)+J( 0.00000 ) .0077679
18 (-1.82088-001)+J( 0.00000 ) -.1820880
```

(-3.64338+001)+J(0.00000)	0.00000	1.00000	(-3.23683-003)+J(0.00000)	-0.032368	0.00000
			(-3.12716-002)+J(0.00000)	-0.312716	0.00000
			(6.22636-002)+J(0.00000)	0.622636	0.00000
			(0.00000)+J(0.00000)	0.000000	0.00000
			(-6.89940-002)+J(0.00000)	-0.068940	0.00000
			(-2.32924-003)+J(0.00000)	-0.023292	0.00000
			(-3.61644-002)+J(0.00000)	-0.361644	0.00000
			(3.30802-002)+J(0.00000)	0.330802	0.00000
			(-7.24145-003)+J(0.00000)	-0.072415	0.00000
			(-2.14271-002)+J(0.00000)	-0.214271	0.00000
			(1.00000+000)+J(0.00000)	1.000000	0.00000
			(1.17196-001)+J(0.00000)	0.117196	0.00000
			(2.96287-001)+J(0.00000)	0.296287	0.00000
			(3.73570-001)+J(0.00000)	0.373570	0.00000
			(1.36428-001)+J(0.00000)	0.136428	0.00000
			(-9.50841-002)+J(0.00000)	-0.095084	0.00000
			(1.17806-002)+J(0.00000)	0.117806	0.00000
			(-5.48777-001)+J(0.00000)	-0.548777	0.00000
(-2.24420+001)+J(8.56895-001)	2.24593+001	0.99927	(1.27324-002)+J(1.29115-002)	0.181334	45.40013
			(9.94790-003)+J(8.58487-003)	0.131779	40.65162
			(1.21372-002)+J(4.08009-002)	0.425850	-73.35532
			(0.00000)+J(0.00000)	0.000000	0.00000
			(-1.31416-001)+J(1.17974-001)	0.176601	-138.08526
			(7.51559-004)+J(1.13639-003)	0.013624	56.52112
			(-6.88112-002)+J(9.88960-002)	0.120816	-124.82940
			(5.66234-002)+J(3.43325-002)	0.0562786	31.19334
			(-1.19345-001)+J(4.73786-002)	0.1284053	158.34745
			(-1.60041-001)+J(1.69560-001)	0.2473164	-136.71716
			(-1.06053-001)+J(1.20487-001)	0.1604983	-131.35910
			(-1.14622-002)+J(1.27656-002)	0.171564	-131.92064
			(-4.65424-002)+J(6.00989-002)	0.0760136	-127.75528
			(-7.84142-002)+J(1.09227-001)	0.1344594	-125.67459
			(-2.70649-002)+J(3.71191-002)	0.0459384	-126.00719
			(5.72371-002)+J(3.62457-001)	0.3669486	81.02628
			(1.00000+000)+J(0.00000)	1.000000	0.00000
			(3.92977-001)+J(4.44319-001)	0.5931699	48.50894

LINEAR MODEL

$$(-1, -2504 + 0011) + J(2, 05063 + 0001)$$

FIG 100 LINEAR MODEL 83/9/30K 2/18/76

(-2.6374+000)+J(0.0000)	1.00000	1	(-8.91095+001)+J(0.0000)	-8.91095	0.0000
		2	(1.22868+002)+J(0.0000)	-0.122868	0.0000
		3	(-6.60625+002)+J(0.0000)	-0.660625	0.0000
		4	(0.00000)+J(0.0000)	0.000000	0.0000
		5	(4.70569+001)+J(0.0000)	4.70568	0.0000
		6	(5.15167+002)+J(0.0000)	0.51514	0.0000
		7	(1.05207+001)+J(0.0000)	1.05207	0.0000
		8	(-5.03653+001)+J(0.0000)	-0.03653	0.0000
		9	(-4.05727+001)+J(0.0000)	-0.05727	0.0000
		10	(-3.72017+001)+J(0.0000)	-0.37201	0.0000
		11	(-5.55517+001)+J(0.0000)	-0.55517	0.0000
		12	(8.74984+002)+J(0.0000)	0.87498	0.0000
		13	(-5.35707+001)+J(0.0000)	-0.53570	0.0000
		14	(-6.78707+001)+J(0.0000)	-0.67870	0.0000
		15	(1.00000+000)+J(0.0000)	1.00000	0.0000
		16	(-6.10927+001)+J(0.0000)	-0.61092	0.0000
		17	(-4.35923+001)+J(0.0000)	-0.43592	0.0000
		18	(-1.42277+001)+J(0.0000)	-0.14227	0.0000
(-1.6415+000)+J(1.25524+001)	1.6549+000	99716	(2.45712+001)+J(1.20257+001)	2.76154	27.15255
		1	(-5.52277+002)+J(4.43307+002)	0.07119	140.86952
		2	(-1.15674+001)+J(1.95693+002)	0.15796	172.89374
		3	(0.00000)+J(0.0000)	0.00000	0.0000
		4	(-3.00228+001)+J(2.35885+002)	0.01157	175.5138
		5	(-5.44507+002)+J(1.78812+002)	0.57783	161.97476
		6	(-1.37297+001)+J(2.37362+002)	0.39334	170.1900
		7	(8.71277+002)+J(5.84233+002)	0.05134	34.03337
		8	(4.51441+002)+J(4.15663+002)	0.01279	42.5486
		9	(3.37257+002)+J(7.57237+002)	0.02846	65.67994
		10	(-2.04147+001)+J(6.84476+002)	0.21546	18.15603
		11	(-4.44027+002)+J(4.49227+002)	0.95500	152.0984
		12	(2.10217+001)+J(6.57732+002)	0.20260	17.13744
		13	(2.56897+001)+J(8.45669+002)	0.27052	18.22141
		14	(1.00000+000)+J(0.0000)	1.00000	0.0000
		15	(2.55307+001)+J(7.92441+002)	0.26710	17.24359
		16	(3.77047+002)+J(4.20059+002)	0.56447	48.08894
		17	(-3.13777+002)+J(2.34778+003)	0.04144	176.77523
		18			

(-1.77145-001)+J(0.00000)	0.00000	1.00000	1	(1.74714-003)+J(0.00000)	0.00000	0.00000
			2	(7.15500-003)+J(0.00000)	0.00000	0.00000
			3	(5.62906-002)+J(0.00000)	0.00000	0.00000
			4	(0.00000)+J(0.00000)	0.00000	0.00000
			5	(1.80207-002)+J(0.00000)	0.00000	0.00000
			6	(8.17413-004)+J(0.00000)	0.00000	0.00000
			7	(4.95879-002)+J(0.00000)	0.00000	0.00000
			8	(-1.77407-002)+J(0.00000)	0.00000	0.00000
			9	(1.16788-001)+J(0.00000)	0.00000	0.00000
			10	(-5.03032-002)+J(0.00000)	0.00000	0.00000
			11	(-7.65879-002)+J(0.00000)	0.00000	0.00000
			12	(-7.62293-003)+J(0.00000)	0.00000	0.00000
			13	(-4.95113-002)+J(0.00000)	0.00000	0.00000
			14	(-6.35569-002)+J(0.00000)	0.00000	0.00000
			15	(-2.05864-002)+J(0.00000)	0.00000	0.00000
			16	(-3.63171-001)+J(0.00000)	0.00000	0.00000
			17	(1.00000+000)+J(0.00000)	0.00000	0.00000
			18	(-1.05206-001)+J(0.00000)	0.00000	0.00000

(-5.45363-001)+J(0.00000)	0.00000	1.00000	1	(2.89403-001)+J(0.00000)	0.00000	0.00000
			2	(1.26248-001)+J(0.00000)	0.00000	0.00000
			3	(-2.34841-001)+J(0.00000)	0.00000	0.00000
			4	(0.00000)+J(0.00000)	0.00000	0.00000
			5	(-1.53740-001)+J(0.00000)	0.00000	0.00000
			6	(-1.83740-001)+J(0.00000)	0.00000	0.00000
			7	(-5.02872-004)+J(0.00000)	0.00000	0.00000
			8	(7.54442-002)+J(0.00000)	0.00000	0.00000
			9	(2.11424-002)+J(0.00000)	0.00000	0.00000
			10	(1.51837-001)+J(0.00000)	0.00000	0.00000
			11	(2.04761-001)+J(0.00000)	0.00000	0.00000
			12	(1.00000+000)+J(0.00000)	0.00000	0.00000
			13	(2.05781-001)+J(0.00000)	0.00000	0.00000
			14	(2.20373-001)+J(0.00000)	0.00000	0.00000
			15	(2.69426-001)+J(0.00000)	0.00000	0.00000
			16	(1.74084-001)+J(0.00000)	0.00000	0.00000
			17	(1.36488-002)+J(0.00000)	0.00000	0.00000
			18	(-8.16476-002)+J(0.00000)	0.00000	0.00000

(-1.00000+001)+J(0.00000) 0.00000	1.00000	1	(5.62998-002)+J(0.00000)	.0562998	.00000
			2	(4.32258-002)+J(0.00000)	.0432258	.00000
			3	(1.00000+000)+J(0.00000)	1.0000000	.00000
			4	(-1.66634-002)+J(0.00000)	-.0166634	.00000
			5	(3.03390-001)+J(0.00000)	.3033898	.00000
			6	(-2.56052-003)+J(0.00000)	-.0025605	.00000
			7	(6.09095-001)+J(0.00000)	.6090947	.00000
			8	(5.69958-002)+J(0.00000)	.569958	.00000
			9	(5.02972-001)+J(0.00000)	.5029725	.00000
			10	(2.05947-001)+J(0.00000)	.2059475	.00000
			11	(2.80615-002)+J(0.00000)	.0280615	.00000
			12	(1.99829-003)+J(0.00000)	.0019983	.00000
			13	(7.39322-003)+J(0.00000)	.0073932	.00000
			14	(1.12019-001)+J(0.00000)	.1120197	.00000
			15	(2.81415-002)+J(0.00000)	.0281415	.00000
			16	(3.30674-001)+J(0.00000)	.3306743	.00000
			17	(9.97145-001)+J(0.00000)	.9971452	.00000
			18	(6.56746-001)+J(0.00000)	.6567458	.00000

***** THE MATRICES IN FINAL FORM *****

F-MATRIX

	SNEAN	SNCOV	PTS	PTUS	PTW	TT25H	TT25C	TT3	TT4PHI	TTAPLO
SNEAN	-1.0210+000	7.1705+001	-8.4248+001	3.5347+002	1.0306+000	-4.8436+001	-1.5353+001	-5.5470+002	5.3043+002	-8.0352+003
SNCOV	-1.0585+001	-1.0590+000	-5.7337+002	6.0930+001	-3.5037+001	6.5996+001	-4.1317+002	-6.4263+002	4.3657+001	4.7948+002
PTS	3.6036+000	-5.8150+000	-8.0500+000	-1.0993+001	2.6046+000	-2.7465+000	-1.2014+000	-8.4575+001	-1.4638+001	-5.3028+001
PTUS	6.2797+001	3.2499+002	2.4643+001	-1.1610+002	-1.7229+001	2.0199+002	1.7576+001	1.5505+001	-2.5841+001	-3.4445+001
PTW	4.6025+001	3.6437+001	1.1300+002	3.9550+002	-4.7850+002	3.1420+001	2.7172+001	3.6447+000	4.6059+001	1.5246+001
TT25H	3.6733+000	-2.2145+000	7.0542+001	-7.0448+003	3.8770+002	-1.8470+001	4.9522+001	-4.2267+002	4.6518+002	-4.2283+002
TT25C	2.9258+000	-2.3400+000	1.7976+000	-8.6685+003	-6.2770+002	4.0372+000	-1.8750+001	-5.7400+002	-6.4577+002	-5.7337+002
TT3	-2.0352+000	6.5442+000	-1.0209+000	3.9545+000	3.1842+002	1.4561+001	-7.2058+001	-1.9970+001	3.8901+002	3.4960+002
TT4PHI	-2.1241+002	4.0293+02	-1.0515+002	3.1842+002	3.3397+003	7.2364+002	-1.0622+002	3.9367+000	-5.0010+001	3.5400+003
TTAPLO	-2.2739+003	5.6432+003	-1.4470+003	4.2495+003	4.4482+004	9.5574+003	-1.4870+003	5.2482+001	-6.0012+000	-6.6710+001
TT4	-1.0213+001	-5.0440+001	-1.0242+000	-1.1014+000	1.1616+001	3.5870+001	-1.9918+000	2.9305+001	-1.2733+001	1.3656+001
TT5H	3.6926+001	2.5565+001	1.5627+001	-1.2708+001	1.1649+001	-1.0663+000	1.0618+001	8.2708+000	-1.4602+001	-1.6119+000
TT5C	1.7749+001	3.4432+001	6.2355+002	-5.0632+000	4.5594+000	-4.3530+001	4.1707+002	3.3078+000	-5.4009+000	-6.4558+001
TT5	-3.1912+001	-1.2563+000	3.7283+000	-5.9841+000	1.6015+000	2.0009+002	-3.5015+002	3.8614+000	-6.5845+000	-7.7028+001
TT6C	-5.3659+002	2.7721+001	3.5760+002	-1.7682+003	-1.3687+003	-1.8423+001	1.9853+001	1.0732+001	-1.7886+003	-1.7825+003
TT7H	-1.1505+001	1.0059+001	4.6062+001	2.3683+001	7.2827+000	-6.3408+000	1.2367+000	-9.3751+001	6.0661+001	-3.3553+001

F-MATRIX

	TTJ	TTUHT	TTUSLO	TT5	TT5C	TTM
SNEAN	-3.0840+001	3.4472+001	2.8122+002	-4.3411+002	-3.2940+002	-1.5373+002
SNCOV	-1.3562+001	-1.0601+003	-1.0201+003	-1.0198+003	-5.1011+003	-1.0203+003
PTS	-2.4171+000	-5.7465+001	-6.2726+001	1.1012+000	5.6134+001	-5.7483+001
PTUS	3.2966+001	2.5842+001	-2.5083+001	-8.6134+002	1.4640+000	2.5847+001
PTW	1.3225+002	2.2444+001	2.2840+001	2.6507+001	2.3529+001	2.2334+001
TT25H	-4.5154+002	0.2066+002	-4.2284+002	-2.6425+002	2.6413+002	-4.2235+002
TT25C	-5.7307+002	-5.7399+002	-6.4378+002	-5.5600+002	6.0993+002	-5.7408+002
TT3	3.0941+002	3.0352+002	3.4934+002	2.8767+002	-3.6037+002	3.4356+002
TT4PHI	4.4022+001	3.5104+003	3.5401+003	-8.6478+003	-5.3122+003	3.5003+003
TTAPLO	6.3556+000	-4.2480+004	-3.2481+004	-1.2747+003	-6.3734+004	-4.2483+004
TT4	-4.0090+001	1.3455+001	1.3958+001	-1.1049+001	-1.7031+001	1.3457+001
TT5H	4.2307+001	-5.0000+001	0.0000	-7.2339+003	8.6495+003	0.0000
TT5C	2.0331+001	-1.8000+001	-2.0010+000	3.4751+003	8.6495+003	-8.6866+004
TT5	2.5233+001	-2.6451+000	-3.1104+001	-1.0860+001	1.5004+002	-1.4004+002
TT6C	-2.3253+002	-1.7409+003	-1.7887+003	-1.7882+003	-2.0000+001	-1.7890+003
TT7H	-4.0763+000	-4.4056+001	-1.6054+001	2.5855+001	2.0619+001	-5.0050+001

F100 LINEAR MODEL 20/9/10K NEW 1/30/76

D-MATRIX	MEMB	AMIX	CIVV	RCVV	BLC
ENMY	6.0284-001	-4.0519-001	4.5317-002	2.2553-001	-7.2103-001
MEAN	-6.4548-003	-3.4254-002	-3.4229-002	-7.1036-003	9.1487-003
TTG	0.0000	0.0000	0.0000	0.0000	0.0000
SMAF	-1.7706-001	-1.4281-001	4.9324-001	-1.5390-001	-4.5798-001
SMC	3.4919-001	1.7340-001	-6.0110-002	4.0480-001	-5.9708-001
	-6.6481-002	2.4342-002	-3.7625-003	-4.7170-003	9.5170-002
	-1.4284-002	4.7430-003	-5.4850-003	-1.7043-003	2.1600-002

F100 LINEAR MODEL 20/9/30K NEW 1/30/76

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-0.50333+002)+j(-0.00000)	0.00000	1.00000	1 (-2.14041-003)+j(-0.00000)	-.0021404	.00000
			2 (-7.59885-004)+j(-0.00000)	.0007295	.00000
			3 (-5.54937-003)+j(-0.00000)	-.0055494	.00000
			4 (-5.99646-004)+j(-0.00000)	.0005998	.00000
			5 (-1.00000+000)+j(-0.00000)	1.0000000	.00000
			6 (-1.08053-004)+j(-0.00000)	.0001081	.00000
			7 (-1.73106-004)+j(-0.00000)	-.0001731	.00000
			8 (-1.09219-004)+j(-0.00000)	-.0001099	.00000
			9 (-3.77861-005)+j(-0.00000)	.0000378	.00000
			10 (-4.89714-006)+j(-0.00000)	.0000049	.00000
			11 (-2.74565-004)+j(-0.00000)	-.0002746	.00000
			12 (-2.70037-002)+j(-0.00000)	.0270037	.00000
			13 (-1.07332-002)+j(-0.00000)	-.0107332	.00000
			14 (-3.56806-003)+j(-0.00000)	-.0035681	.00000
			15 (-3.98973-006)+j(-0.00000)	-.0000040	.00000
			16 (-1.48196-002)+j(-0.00000)	-.0168196	.00000
(-1.19293+002)+j(-0.00000)	0.00000	1.00000	1 (-9.20737-003)+j(-0.00000)	-.0092074	.00000
			2 (-1.54860-003)+j(-0.00000)	-.0018486	.00000
			3 (-2.37652-002)+j(-0.00000)	-.0237652	.00000
			4 (-9.15582-001)+j(-0.00000)	.9155823	.00000
			5 (-1.00000+000)+j(-0.00000)	1.0000000	.00000
			6 (-8.40211-004)+j(-0.00000)	.0008402	.00000
			7 (-1.02316-003)+j(-0.00000)	.0010237	.00000
			8 (-4.66379-002)+j(-0.00000)	-.0466379	.00000
			9 (-5.56233-003)+j(-0.00000)	-.0055623	.00000
			10 (-1.14165-004)+j(-0.00000)	.0007142	.00000
			11 (-3.65581-003)+j(-0.00000)	-.0036581	.00000
			12 (-9.97170-001)+j(-0.00000)	.0099717	.00000
			13 (-3.88844-003)+j(-0.00000)	.0038844	.00000
			14 (-4.34102-002)+j(-0.00000)	.0434102	.00000
			15 (-1.09234-002)+j(-0.00000)	-.0001098	.00000
			16 (-1.28876-001)+j(-0.00000)	-.0128876	.00000

1	1.00000	(-5.74145+001)+J(0.00000)	0.00000	1.00000	(-6.26522+003)+J(0.00000)	-0.005482	0.00000
2					(-2.3337+003)+J(0.00000)	-0.003134	0.00000
3					(7.2653+003)+J(0.00000)	0.072863	0.00000
4					(-5.9473+002)+J(0.00000)	-0.059473	0.00000
5					(-4.25130+002)+J(0.00000)	-0.045130	0.00000
6					(1.5659+003)+J(0.00000)	0.015566	0.00000
7					(1.56522+003)+J(0.00000)	0.015468	0.00000
8					(5.4893+003)+J(0.00000)	0.054786	0.00000
9					(3.3818+001)+J(0.00000)	0.338177	0.00000
10					(3.7441+002)+J(0.00000)	0.374441	0.00000
11					(-4.26522+002)+J(0.00000)	-0.043248	0.00000
12					(1.0000+000)+J(0.00000)	1.00000000	0.00000
13					(3.7355+001)+J(0.00000)	3.735500	0.00000
14					(1.60253+001)+J(0.00000)	1.602533	0.00000
15					(-7.00524+004)+J(0.00000)	-0.007409	0.00000
16					(-5.41445+001)+J(0.00000)	-0.561848	0.00000

[illegible]

1	(-1.055686002)*J(-2.2622-004)	.016674	-177.67749
2	(4.8765003)*J(-3.2703-003)	.006492	-34.02659
3	(1.2357002)*J(-5.2828-003)	.017904	-22.2162
4	(-1.1735002)*J(-6.5923-003)	.015606	-19.5195
5	(9.5440002)*J(-7.2935-003)	.003319	-4.6678
6	(3.3461003)*J(-2.6642-004)	.003552	-4.35459
7	(3.4813003)*J(-6.2305-006)	.0034781	.00254
8	(3.3695003)*J(-1.0559-003)	.0035000	162.44359
9	(-4.0027001)*J(-3.17715-01)	.517721	-41.58933
10	(4.9858002)*J(-8.8026-002)	.0619147	-142.1487
11	(-3.5165002)*J(-9.5521-002)	.0628791	-124.55280
12	(1.0000000)*J(0.00000)	1.000000	.00000
13	(3.7056001)*J(-1.0440-003)	.3720574	-1.4037
14	(2.65349003)*J(-2.6984-002)	.043515	-95.5467
15	(-2.7095003)*J(-3.1058-004)	.007180	-175.5311
16	(1.24510001)*J(-1.7353-001)	.211795	-54.89735

1	(-1.2673+002)+J(-1.4987-003)	0.15352	174.73564
2	(-1.45376+003)+J(-1.25129-003)	0.017225	133.1137
3	(-3.5175+002)+J(-1.37150-002)	158.26994	158.26994
4	(-6.43354+002)+J(-4.62363-002)	0.95408	44.40506
5	(-2.2408+001)+J(-1.7341-002)	2344739	44.40509
6	(-5.4415+003)+J(-5.7771-002)	0.59994	95.53474
7	(-3.2664+002)+J(-1.18249-001)	126449	74.45819
8	(-1.56124+001)+J(-3.29665-002)	155724	11.3374
9	(-2.6620+001)+J(-7.7433-002)	313965	16.73466
10	(-2.3735+002)+J(-6.4058-003)	0.23455	15.9352
11	(-1.4912+001)+J(-6.5700-002)	1602507	24.3509
12	(-2.4290+001)+J(-9.4314-002)	2900935	16.9362
13	(-6.25669+002)+J(-2.67183-002)	0.97547	16.5774
14	(-7.37834+001)+J(-1.09266-001)	7575613	8.1503
15	(-5.2656+001)+J(-3.27374-001)	615670	32.1241
16	(-1.00000+000)+J(-0.00000)	1.00000	0.0000

1	(-1.23500+001)*J(0.00000	1.00000	(-4.5022+003+J(0.0000)	-004502	0.0000
2			(-1.2317+003+J(0.0000)	-001652	0.0000
3			(-6.4177+003+J(0.0000)	-004918	0.0000
4			(-4.2794+002+J(0.0000)	-042784	0.0000
5			(-8.4234+002+J(0.0000)	-084234	0.0000
6			(-1.0870+002+J(0.0000)	-010870	0.0000
7			(-3.0427+002+J(0.0000)	-030427	0.0000
8			(-1.44135+002+J(0.0000)	-0146135	0.0000
9			(-1.5146+003+J(0.0000)	-0015415	0.0000
10			(-1.44750+004+J(0.0000)	-0001448	0.0000
11			(-2.4046+003+J(0.0000)	-004870	0.0000
12			(-1.5024+002+J(0.0000)	-0170024	0.0000
13			(-5.4502+003+J(0.0000)	-0046360	0.0000
14			(-3.5270+001+J(0.0000)	-352702	0.0000
15			(-1.0000+000+J(0.0000)	-1.000000	0.0000
16			(-3.5068+001+J(0.0000)	-350687	0.0000

[illegible]


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(-6.53325+000)+J( 0.00000 ) 0.00000 1.00000
1 ( 7.49774-002)+J( 0.00000 ) 0.00000 0.00000
2 ( 1.55550-002)+J( 0.00000 ) 0.00000 0.00000
3 ( 1.00000+000)+J( 0.00000 ) 1.0000000
4 ( 1.97154-001)+J( 0.00000 ) 0.00000
5 ( 4.58661-001)+J( 0.00000 ) 0.00000
6 ( 8.39161-002)+J( 0.00000 ) 0.00000
7 ( 1.82523-001)+J( 0.00000 ) 0.00000
8 ( 8.54270-002)+J( 0.00000 ) 0.00000
9 ( 1.79549-002)+J( 0.00000 ) 0.00000
10 ( 6.15684-004)+J( 0.00000 ) 0.00000
11 ( 2.38771-002)+J( 0.00000 ) 0.00000
12 ( 5.51139-002)+J( 0.00000 ) 0.00000
13 ( 7.71885-003)+J( 0.00000 ) 0.00000
14 ( 2.12913-001)+J( 0.00000 ) 0.00000
15 ( 2.71493-001)+J( 0.00000 ) 0.00000
16 ( 3.26423-001)+J( 0.00000 ) 0.00000
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(-1.12983+000)+J( 3.91995+001) 1.25279+000 .94979
1 ( 1.00000+000)+J( 0.00000 ) 1.0000000
2 ( 3.79596-002)+J( 1.15771-001) 0.00000
3 ( 8.15927-001)+J( 6.12635-002) 0.00000
4 ( 4.37103-001)+J( 3.43626-001) 0.00000
5 ( 6.29591-001)+J( 2.33183-001) 0.00000
6 ( 2.50861-001)+J( 2.44098-002) 0.00000
7 ( 2.97482-001)+J( 6.00715-002) 0.00000
8 ( 1.58595-001)+J( 1.11994-001) 0.00000
9 ( 6.62883-002)+J( 6.11639-002) 0.00000
10 ( 5.49741-003)+J( 7.03116-002) 0.00000
11 ( 8.27032-002)+J( 7.49285-002) 0.00000
12 ( 1.88762-002)+J( 9.61794-002) 0.00000
13 ( 8.73534-002)+J( 1.42858-001) 0.00000
14 ( 1.50827-002)+J( 1.68530-001) 0.00000
15 ( 3.10571-001)+J( 6.76086-002) 0.00000
16 ( 3.58668-002)+J( 4.85961-002) 0.00000
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(-1.59179+000)+J( 0.00000 ) 0.00000 1.00000
1 (-2.04781-001)+J( 0.00000 ) 0.00000
2 (-2.04808-003)+J( 0.00000 ) 0.00000
3 (-2.87059-001)+J( 0.00000 ) 0.00000
4 (-8.46804-002)+J( 0.00000 ) 0.00000
5 (-1.12194-001)+J( 0.00000 ) 0.00000
6 (-8.29477-002)+J( 0.00000 ) 0.00000
7 (-8.56170-002)+J( 0.00000 ) 0.00000
8 (-3.10962-002)+J( 0.00000 ) 0.00000
9 ( 1.45383-002)+J( 0.00000 ) 0.00000
10 ( 4.47071-003)+J( 0.00000 ) 0.00000
11 (-1.77361-002)+J( 0.00000 ) 0.00000
12 ( 7.30556-003)+J( 0.00000 ) 0.00000
13 ( 1.00000+000)+J( 0.00000 ) 1.0000000
14 (-3.92557-002)+J( 0.00000 ) 0.00000
15 (-3.43370-002)+J( 0.00000 ) 0.00000
16 (-3.57066-002)+J( 0.00000 ) 0.00000
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*** THE MATRICES IN FINAL FORM ***

CASE 10

F-MATRIX

SUFAN	SNCOM	PT7M	NECOM	PT3	FTT	PT45	TT25H	TT25C	TT3
-7.0840+000	2.5378+000	-3.3698+000	-4.7907+001	9.2303+002	0.0000	6.0222+000	-1.7188+000	-2.8707+001	-1.7908+001
-2.1576+000	-5.1120+000	-2.3250+001	-2.8168+001	5.3365+000	0.0000	-2.7155+000	1.6778+000	-1.8834+001	-1.0028+001
1.1602+000	-4.4935+000	-6.4600+000	3.5139+000	2.7157+001	0.0000	3.8584+000	2.1555+000	-1.0997+000	-1.0268+000
0.0000	0.0000	0.0000	-1.0000+001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
1.4804+002	1.4308+002	2.4078+001	1.4910+001	-1.6550+002	0.0000	-2.3100+000	-1.2257+002	1.4422+001	1.7523+001
0.0000	0.0000	0.0000	0.0000	0.0000	-2.5000+001	0.0000	0.0000	0.0000	0.0000
9.0312+001	-2.8635+001	7.4880+000	1.5553+001	5.0821+002	0.0000	-5.7450+002	-4.9413+001	3.7605+000	-3.2946+001
9.0365+000	-2.1503+000	4.6790+001	3.2258+001	2.4102+001	0.0000	2.1810+003	-1.9430+001	3.4577+001	3.2711+003
4.3825+000	-5.2021+000	1.0374+000	3.9628+002	5.9451+001	0.0000	1.2083+002	3.7654+000	-1.9200+001	1.5385+002
-4.5607+000	6.8957+000	-7.1411+001	7.4231+002	4.9943+000	0.0000	-4.1662+003	1.4221+001	-5.2555+001	-2.0010+001
-1.5643+001	-3.7465+002	-2.8089+002	1.7797+001	1.6860+002	0.0000	-4.6820+003	1.2363+001	-1.9671+002	3.8015+000
-2.0793+002	-9.9447+003	-3.7083+003	2.3396+002	2.3500+003	0.0000	-5.6177+004	1.4521+002	-2.5950+003	5.0700+001
-2.0599+001	-3.3958+001	-3.2939+000	2.0354+001	2.6117+000	0.0000	-2.2621+002	1.7333+001	-2.4278+000	2.6887+001
-4.1950+001	-3.4612+000	-5.4759+002	6.2339+001	-1.0701+001	0.0000	1.0371+001	3.5886+001	-3.9816+002	7.5855+000
-1.4759+001	-3.8442+001	-2.1959+002	2.5154+001	-4.2790+000	0.0000	4.1481+000	1.5416+001	-1.5683+002	3.0344+000
-1.0016+000	-1.5879+000	3.6512+000	3.6429+001	-5.2371+000	0.0000	1.3474+000	4.4227+001	-4.2477+002	3.7526+000
3.2320+002	2.2212+001	3.2520+002	-7.1284+003	-2.1379+002	0.0000	0.0000	-1.5536+001	1.9819+001	1.6189+001
-6.6155+000	9.9590+000	1.5726+000	-1.0152+000	1.7649+002	0.0000	8.0243+000	-6.6727+000	1.2160+000	-3.2120+001

F-MATRIX

SUFAN	SNCOM	PT7M	NECOM	PT3	FTT	PT45	TT25H	TT25C	TT3
4.3500+001	9.3693+002	-1.7142+000	2.8503+000	3.6079+001	-1.6371+001	1.1134+002	4.6843+002	5.9232+002	5.9232+002
3.5586+000	4.4803+001	-1.3736+000	6.8433+002	6.3641+002	6.0707+002	4.5987+002	5.9232+002	5.9232+002	5.9232+002
-6.1255+002	-5.9300+001	-3.4378+000	-6.5756+001	-6.4837+001	2.2789+000	6.0182+001	-6.7101+001	-6.7101+001	-6.7101+001
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
-2.2501+000	-2.2341+000	4.1724+001	-2.2380+000	-2.2379+000	-2.0441+000	-1.0908+000	-2.2380+000	-2.2380+000	-2.2380+000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
-7.9859+001	-1.1123+001	1.7614+002	-2.0960+000	-2.0447+000	-1.8803+000	-1.8958+000	-1.8958+000	-1.8958+000	-1.8958+000
3.1613+003	2.1814+003	3.2717+002	3.2725+003	3.2710+003	8.7257+003	2.8538+002	3.2725+003	3.2725+003	3.2725+003
1.5365+002	1.5386+002	2.3077+002	1.5385+002	1.5386+002	2.7470+002	9.2513+002	1.5385+002	1.5385+002	1.5385+002
-5.9508+003	-5.9519+003	-8.3319+003	-8.3325+003	-5.9513+003	-1.0713+002	4.1660+002	-5.9513+003	-5.9513+003	-5.9513+003
-5.0000+001	8.3667+004	4.6072+001	-2.8096+003	-2.8099+003	-1.8730+003	-5.6202+003	-2.8101+003	-2.8101+003	-2.8101+003
-5.9994+000	-6.6600+001	6.1436+000	-3.3717+004	-3.3717+004	-6.2477+004	-6.7443+004	-3.3717+004	-3.3717+004	-3.3717+004
-2.9945+002	-0.0707+002	4.4050+001	-3.0699+002	-3.4737+002	-6.2208+002	-1.9633+001	-3.0698+002	-3.0698+002	-3.0698+002
-1.2985+001	-1.4187+000	5.9983+001	4.9990+001	1.6178+002	7.4689+003	4.9798+003	3.1119+002	3.1119+002	3.1119+002
-5.1953+000	-5.6603+001	2.8990+001	-1.8000+001	-1.9440+002	3.1372+003	1.7921+003	1.2550+002	1.2550+002	1.2550+002
-6.4120+000	-6.8940+001	2.9632+001	-3.4932+000	-3.7330+001	-1.9730+001	1.9355+002	2.5271+002	2.5271+002	2.5271+002
0.0000	0.0000	4.4852+002	0.0000	0.0000	0.0000	-2.0000+001	0.0000	0.0000	0.0000
1.2319+000	3.0100+001	-4.6858+000	1.9055+001	1.9061+001	3.5044+001	1.5624+001	-4.9820+001	-4.9820+001	-4.9820+001

D-MATRIX

	ANVIX	CTVV	RCVV	BLC
SNFAN	-1.5580-001	4.2385-001	-7.6479-003	3.3352-001
SNFAN	0.0000	1.2282-001	8.9481-003	9.1751-001
SNFAN	-7.4501+000	-2.2505-001	2.0978-002	-3.8935+000
SNFAN	0.0000	0.0000	0.0000	0.0000
SNFAN	2.0057+000	-8.2952+000	-4.7013-001	-1.7301+002
SNFAN	0.0000	0.0000	0.0000	0.0000
SNFAN	9.0821-001	-2.6783+000	-1.5174-001	2.3379+001
SNFAN	3.0177-001	-1.1856-001	6.4244-002	3.6960-002
SNFAN	7.8159-002	-3.8673-001	1.5230-002	4.3215-003
SNFAN	-5.4926-002	2.4603-001	1.1141-002	-1.1931-001
SNFAN	-2.9170-003	9.3054-003	5.6052-004	-2.3041+000
SNFAN	-4.0182-004	1.3083-003	7.4133-005	3.0262-001
SNFAN	-1.7086-001	1.2494+000	7.1079-002	2.3616+001
SNFAN	-4.5281-003	2.2651-002	1.3029-003	3.1140+000
SNFAN	-1.8644-003	9.0431-003	5.3158-004	-1.3254+000
SNFAN	-3.2170-002	6.3189-003	1.7263-003	-1.4081+000
SNFAN	1.1540-003	6.2480-003	-6.3061-004	1.7393-002
SNFAN	1.3525-002	9.1517-001	-3.0674-002	1.5979+000

H-MATRIX

	SNFAN	SNCOM	PT7M	WFCOM	PT3	FTIT	PT45	TT25H	TT25C	TT3
SNFAN	-5.7382-001	-1.0744+000	5.9570-001	-1.8550-001	3.0419-001	0.0000	1.3135+000	8.5511-001	-7.6695-002	-6.7714-002
SNFAN	8.6375-001	2.0199-002	-0.3206-003	1.5462-002	-2.2123-003	0.0000	0.0000	-1.4479-002	-3.1536-003	0.0000
SNFAN	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
SNFAN	1.8534+000	1.7743+000	-1.8589-001	3.3289-002	-1.8685-001	0.0000	-2.8499-003	-1.2930+000	0.0000	0.0000
SNFAN	6.4237+000	2.6007+001	9.8337-001	-3.7711-001	-6.8927+000	0.0000	7.5535-003	-9.7670+000	-2.8600-001	-3.8271-003
SNFAN									7.2413-001	1.0396-002

H-MATRIX

	TT4PHI	TT4DLO	TT4	TT4SMI	TT4SLO	TT5	TT6C	TT7M
SNFAN	2.1023-001	5.8244-002	-7.4279-001	3.7880-002	3.4926-002	8.6007-001	3.9661-001	3.8163-002
SNFAN	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-2.3355-004	0.0000
SNFAN	0.0000	0.0000	1.0000+000	0.0000	0.0000	0.0000	0.0000	0.0000
SNFAN	-3.8235-003	-3.8244-003	-5.2113-003	-3.8270-003	-3.8272-003	-6.7558-003	-2.3250-002	-3.8271-003
SNFAN	9.8081-003	9.8290-003	1.2904-002	1.0721-002	9.8277-003	1.8117-002	5.9128-002	9.8305-003

D-MATRIX

	ANVIX	CTVV	RCVV	BLC
SNFAN	-1.5580-001	4.2385-001	-7.6479-003	3.3352-001
SNFAN	0.0000	1.2282-001	8.9481-003	9.1751-001
SNFAN	-7.4501+000	-2.2505-001	2.0978-002	-3.8935+000
SNFAN	0.0000	0.0000	0.0000	0.0000
SNFAN	2.0057+000	-8.2952+000	-4.7013-001	-1.7301+002
SNFAN	0.0000	0.0000	0.0000	0.0000
SNFAN	9.0821-001	-2.6783+000	-1.5174-001	2.3379+001
SNFAN	3.0177-001	-1.1856-001	6.4244-002	3.6960-002
SNFAN	7.8159-002	-3.8673-001	1.5230-002	4.3215-003
SNFAN	-5.4926-002	2.4603-001	1.1141-002	-1.1931-001
SNFAN	-2.9170-003	9.3054-003	5.6052-004	-2.3041+000
SNFAN	-4.0182-004	1.3083-003	7.4133-005	3.0262-001
SNFAN	-1.7086-001	1.2494+000	7.1079-002	2.3616+001
SNFAN	-4.5281-003	2.2651-002	1.3029-003	3.1140+000
SNFAN	-1.8644-003	9.0431-003	5.3158-004	-1.3254+000
SNFAN	-3.2170-002	6.3189-003	1.7263-003	-1.4081+000
SNFAN	1.1540-003	6.2480-003	-6.3061-004	1.7393-002
SNFAN	1.3525-002	9.1517-001	-3.0674-002	1.5979+000

313176

[illegible][illegible]


```
(-3.52297+0.01)+J( 0.00000 ) 0.00000 1.00000
1 (-3.51768-0.03)+J( 0.00000 ) -.0035177 .00000
2 (-1.14331-0.01)+J( 0.00000 ) -.1143311 .00000
3 ( 5.98055-0.02)+J( 0.00000 ) .0598055 .00000
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 (-5.40737-0.02)+J( 0.00000 ) -.0540737 .00000
6 (-2.79759-0.03)+J( 0.00000 ) -.0027966 .00000
7 (-9.58388-0.02)+J( 0.00000 ) -.0958388 .00000
8 (-1.33474-0.02)+J( 0.00000 ) -.0133474 .00000
9 (-3.61502-0.02)+J( 0.00000 ) -.0361502 .00000
10 ( 8.32583-0.02)+J( 0.00000 ) .0832583 .00000
11 ( 1.00000+0.00)+J( 0.00000 ) 1.0000000 .00000
12 ( 1.16593-0.01)+J( 0.00000 ) .1165932 .00000
13 ( 3.13688-0.01)+J( 0.00000 ) .3136860 .00000
14 ( 4.15891-0.01)+J( 0.00000 ) .4158911 .00000
15 ( 1.51330-0.01)+J( 0.00000 ) .1513305 .00000
16 (-1.38004-0.01)+J( 0.00000 ) -.1380036 .00000
17 ( 4.65666-0.02)+J( 0.00000 ) .0465666 .00000
18 (-4.10914-0.01)+J( 0.00000 ) -.4109140 .00000
```

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(-7.20371+0.00)+J( 4.12167+0.00) A.29999+0.00 .86797
1 ( 5.08711-0.01)+J( 6.48084-0.01) .8238931 51.87004
2 (-1.38244-0.01)+J(-4.47676-0.03) .1383169 -178.14525
3 ( 6.95664-0.01)+J(-1.68294-0.01) .7155550 -13.43833
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 ( 8.40557-0.02)+J( 3.53100-0.01) .3629668 76.60992
6 (-6.85276-0.03)+J( 1.48078-0.03) .0070128 167.73481
7 ( 1.27086-0.01)+J( 3.70700-0.01) .3918792 71.07694
8 ( 5.44173-0.01)+J( 2.71538-0.01) .6081585 26.53184
9 ( 6.46513-0.01)+J( 2.09290-0.01) .6795451 17.93790
10 ( 3.43365-0.01)+J( 9.70362-0.02) .3548127 15.78049
11 ( 1.36843-0.01)+J(-1.68917-0.01) .2177184 -51.23549
12 ( 2.73063-0.03)+J(-1.73711-0.02) .0175511 -81.05163
13 ( 1.14618-0.01)+J(-1.52334-0.01) .1906560 -53.84168
14 ( 1.68446-0.01)+J(-1.64154-0.01) .2442268 -42.23003
15 ( 2.85578-0.02)+J(-6.27914-0.02) .0689805 -65.54373
16 ( 2.72804-0.01)+J(-4.83945-0.01) .5555869 -60.58069
17 ( 1.00000+0.00)+J( 0.00000 ) 1.0000000 .00000
18 ( 4.03573-0.01)+J(-5.01542-0.01) .6437515 -51.17762
```

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F100 LINEAR MODEL 83/1.2/0K 3/3/76

1	(-6.84432-001)+J(0.00000)	1.00000	1 (1.45493-001)+J(0.00000)	1454930	0.00000
2			2 (9.00615-002)+J(0.00000)	0900615	0.00000
3			3 (-2.44381-002)+J(0.00000)	-0244381	0.00000
4			4 (0.00000)+J(0.00000)	0000000	0.00000
5			5 (1.72081-001)+J(0.00000)	1720809	0.00000
6			6 (4.39902-002)+J(0.00000)	0439902	0.00000
7			7 (1.33876-001)+J(0.00000)	1338758	0.00000
8			8 (5.75895-002)+J(0.00000)	0575895	0.00000
9			9 (4.12499-002)+J(0.00000)	0412499	0.00000
10			10 (8.41860-002)+J(0.00000)	0841860	0.00000
11			11 (-3.46222-002)+J(0.00000)	-0346222	0.00000
12			12 (1.00000+000)+J(0.00000)	1000000	0.00000
13			13 (-4.3613-002)+J(0.00000)	-043613	0.00000
14			14 (-7.43416-002)+J(0.00000)	-0743416	0.00000
15			15 (-9.6862-002)+J(0.00000)	-096862	0.00000
16			16 (-1.1643-001)+J(0.00000)	-116432	0.00000
17			17 (4.35167-002)+J(0.00000)	0435167	0.00000
18			18 (-4.81428-002)+J(0.00000)	-0481428	0.00000

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1	1.00000	(-1.9373+001)+J(0.00000)	0.00000	1.00000	(4.16280-003)+J(0.00000)	0.00000	0.0041528	0.00000
2					(-1.17627-02)+J(0.00000)	0.00000	-0.117627	0.00000
3					(-1.10152-01)+J(0.00000)	0.00000	-1.101524	0.00000
4					(0.00000)+J(0.00000)	0.00000	0.000000	0.00000
5					(-5.73032-02)+J(0.00000)	0.00000	-0.0573032	0.00000
6					(-6.14677-04)+J(0.00000)	0.00000	-0.006147	0.00000
7					(-5.59064-02)+J(0.00000)	0.00000	-0.0559064	0.00000
8					(2.06162-02)+J(0.00000)	0.00000	0.0206162	0.00000
9					(-1.97284-02)+J(0.00000)	0.00000	-0.197284	0.00000
10					(7.2346-03)+J(0.00000)	0.00000	0.0072325	0.00000
11					(5.30225-02)+J(0.00000)	0.00000	0.0530225	0.00000
12					(5.42689-03)+J(0.00000)	0.00000	0.0054269	0.00000
13					(3.4586-02)+J(0.00000)	0.00000	0.034586	0.00000
14					(5.01916-02)+J(0.00000)	0.00000	0.0501916	0.00000
15					(1.66070-02)+J(0.00000)	0.00000	0.166070	0.00000
16					(1.00000+00)+J(0.00000)	0.00000	1.0000000	0.00000
17					(-6.07216-01)+J(0.00000)	0.00000	-0.6072157	0.00000
18					(8.05395-01)+J(0.00000)	0.00000	0.8053950	0.00000

6013

(-1.0)

*** THE MATRICES IN FINAL FORM ***

CASE 11

F-MATRIX

SNFAN	SNCOM	PT7M	WFCOM	PT3	FTIT	PT45	TT25H	TT25C	TT3
-1.1470+000	9.4073+002	-8.7803+001	-2.2609+001	8.6111+002	0.0000	1.1509+000	-2.6881+002	5.0773+002	-7.4661+003
-9.5478+002	-1.5100+000	-3.7471+001	-1.0329+002	1.0222+000	0.0000	-4.9521+001	4.1475+001	4.2422+002	-7.5021+002
2.3495+000	-4.1455+000	-9.3480+000	1.0428+000	6.8658+001	0.0000	4.0863+000	3.4417+000	8.0710+002	-5.2590+001
0.0000	0.0000	0.0000	-1.0000+001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
2.8253+001	2.0161+002	1.1224+002	1.6990+001	-1.6250+002	0.0000	-2.9310+000	-1.6579+002	-1.3209+001	1.8694+001
0.0000	0.0000	0.0000	0.0000	0.0000	-2.5000+001	0.0000	0.0000	0.0000	0.0000
2.0095+001	-4.1349+001	1.1787+001	-2.3531+002	4.4825+002	0.0000	-5.9710+002	-1.0571+002	-4.1902+001	-6.8127+001
1.1503+001	-2.8253+001	2.4429+000	-5.3823+001	-3.9763+002	0.0000	1.4484+001	-1.9650+001	-2.2860+001	-7.0999+002
8.6050+000	-3.7954+002	6.7646+000	1.9008+000	-7.7319+002	0.0000	-6.3671+001	1.2513+001	-2.0430+001	-1.0964+001
-7.1068+001	7.7741+000	-2.8600+000	-8.0634+001	4.4163+000	0.0000	8.9280+002	1.5390+001	-3.5004+001	-1.9950+001
-3.5655+002	-7.9672+002	-1.7841+001	1.7512+001	2.8863+002	0.0000	5.9756+003	2.0717+001	1.8423+002	3.9199+000
-4.7793+003	-1.9635+002	-1.8526+002	2.3582+002	3.8240+003	0.0000	7.1717+004	2.7599+002	2.5099+003	5.2271+001
-4.5775+000	-3.0175+001	-1.8408+001	1.9828+001	3.4966+000	0.0000	5.8451+001	2.7659+001	2.2742+000	1.7512+001
-1.4791+001	-3.5537+000	-6.1897+001	6.1107+001	-1.0307+001	0.0000	1.0388+001	9.7587+001	9.5062+002	7.6329+000
-5.8921+002	-1.3416+000	-2.5573+001	2.4438+001	-4.1231+000	0.0000	4.1551+000	3.9034+001	3.8044+002	3.0544+000
9.5711+001	-1.4997+000	3.5107+000	3.1701+001	-5.0195+000	0.0000	1.1072+000	7.4710+001	8.7658+002	3.7820+000
-2.0086+001	5.1680+001	3.2496+001	6.4632+002	-6.5533+002	0.0000	-1.5338+002	-4.8386+001	1.9632+001	2.4265+001
-1.3628+001	1.8501+001	1.1170+001	-1.6979+000	-5.7446+001	0.0000	8.8744+000	-1.5446+001	-7.9027+001	-1.5553+001

F-MATRIX

TT4PHI	TT4PLO	TT4	TT45HI	TT45LO	TT5	TT6C	TT7M
1.0453+001	4.3614+002	-2.9217+001	5.5604+001	9.1584+002	1.4933+003	2.8871+002	3.6337+002
6.1118+001	7.1490+002	-2.5067+001	4.3206+003	5.1064+003	4.3203+003	-2.3564+003	4.3207+003
3.6965+001	-1.1709+001	-2.7196+000	-1.7354+001	-1.6667+001	2.4440+000	4.7555+001	-1.7158+001
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
-1.8936+000	-1.6445+000	4.1820+001	-1.6444+000	-1.8433+000	-1.6445+000	2.8898+001	-1.5949+000
-1.0849+002	-4.5098+001	1.3336+002	-2.1267+001	2.3630+002	0.0000	0.0000	0.0000
1.9311+001	2.0023+001	-5.3947+002	3.7048+001	-3.7047+001	-3.7045+001	-3.6121+001	-3.7048+001
-5.7194+001	-5.8062+001	5.3405+002	2.0021+001	2.0020+001	2.0304+001	-8.5189+003	2.0587+001
6.5118+002	5.3853+002	3.7560+002	5.3851+002	-5.9024+001	-5.8044+001	1.1250+002	-5.7914+001
-5.0000+001	3.9844+003	4.5857+001	3.9841+003	-1.9921+003	3.9840+003	2.1255+003	5.1019+002
-5.6000+000	-6.4620+001	6.1273+000	4.7875+004	-2.3903+004	3.9840+003	3.9826+003	5.9775+003
4.0501+001	3.6496+001	-4.7350+001	3.6496+001	3.7860+001	4.7808+004	4.7749+004	7.1730+004
-1.2454+001	-1.7601+000	5.9346+001	-4.9940+001	-1.8489+002	3.7007+001	4.1685+002	3.5903+001
-4.9816+000	-5.4383+001	2.3731+001	-1.7931+001	-1.9933+000	7.1301+003	1.8484+002	2.5088+002
-6.0979+000	-6.1127+001	2.0227+001	-3.4860+000	-3.3642+001	-1.9730+002	7.6052+003	9.9839+003
-1.2548+002	-9.7618+003	7.3916+002	-9.7607+003	-1.2550+002	-1.9730+002	2.6010+002	3.7323+002
1.4069+000	4.4453+001	-4.8875+000	3.0191+001	3.1652+001	4.0247+001	-2.0000+001	-9.7601+003
						1.1010+001	-4.9690+001

GOMATRIK

MEMBR	AMNIX	CIVV	RCVV	BLC
0.0000	-6.712E+02	-2.607E+03	4.924E+04	2.216E+01
0.0000	-2.598E+03	-6.832E+05	5.521E+03	1.123E+01
0.0000	-6.175E+00	1.269E+02	1.870E+02	1.607E+01
1.0000E+01	0.0000	0.0000	0.0000	0.0000
0.0000	-9.598E+01	1.950E+02	5.175E+01	-1.914E+02
0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	2.103E+01	-3.184E+01	-7.499E+01	-1.914E+02
0.0000	-1.100E+02	1.500E+02	1.171E+03	-2.642E+01
0.0000	1.596E+00	1.173E+02	7.674E+03	1.022E+00
0.0000	1.022E+01	4.864E+04	3.426E+02	1.989E+00
0.0000	1.050E+02	-3.457E+05	-6.163E+04	-2.773E+00
0.0000	1.354E+03	4.720E+06	-8.381E+05	-3.700E+01
0.0000	2.014E+01	-2.670E+03	-8.544E+02	3.291E+01
0.0000	2.760E+02	1.808E+01	-2.470E+02	3.674E+00
0.0000	9.785E+03	-6.779E+06	-1.143E+03	-1.470E+02
0.0000	2.402E+02	3.132E+04	1.474E+03	-2.001E+00
0.0000	1.509E+03	-1.195E+03	1.037E+03	-1.621E+01
0.0000	-6.479E+01	-6.204E+02	6.137E+02	1.249E+01

H-VATPIX

	SUFAN	SNCOM	PT7M	WFCOM	PTS	FIT	PT45	T125M	T125C	T73
F2HX	2.6104-001	-3.5435-001	-1.8575-001	-4.5916-001	2.7578-001	0.0000	1.0809+000	9.1168-001	1.3189-001	-1.2153-002
F2HJ	6.9558-001	3.5016-004	-2.5011-003	9.8214-003	0.0000	0.0000	0.0000	-1.5008-004	3.5025-004	0.0000
F2HJ	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
F2HJ	1.3272+001	6.4099-001	4.7533+000	2.4292-002	4.2481-002	0.0000	1.4786-001	3.9772-001	5.8519-001	8.4631-002
F2HJ	1.2724+000	1.1546+001	5.1152+000	9.0031-001	-7.2306+000	0.0000	-1.6320-001	-6.4331+000	-6.3354-001	-9.2582-002
F2HJ	1.5733-001	-1.5102-001	-6.1922-001	-7.9583-002	4.9804-002	0.0000	1.9900-002	3.3755-002	1.6677-001	1.1133-002
F2HJ	1.0331-001	6.1732-000	-1.5879-001	-1.6241-002	-2.2523-003	0.0000	5.1630-003	3.0515-002	5.9224-002	2.8976-003

MATRIX

	TP4PHI	TP4BL0	TP4	TP4SHI	TP4SL0	TP5	TP6C	TP7M
PMNY	2.0179-001	9.7245-002	-5.3205-001	7.2107-002	7.3483-002	7.1409-002	2.3067-001	7.1550-002
MEAN	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
TP2	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
SWAF	0.1024-001	9.1907-002	5.0182-000	9.1427-002	9.4957-002	9.1768-002	9.2333-003	9.0068-002
SWAC	-1.1507-001	-1.0480-001	-6.3368-002	-1.0155-001	-1.0500-001	-1.0204-001	-1.0370-002	-1.0023-001
DP25GT	1.7235-002	3.2545-002	7.6200-003	1.2220-003	1.2411-002	1.2599-002	1.2994-003	1.1223-003
DP25SC	3.4693-003	3.2644-003	1.9677-003	3.2678-003	3.2076-003	3.2785-003	2.8611-004	3.2555-003

F100 LINEAR MODEL 83/9/45K 2/24/76

D-MATRIX				
	MFMBH	ANMIX	CIVV	RCVV
FMY	0.0000	2.8561-002	2.2710-003	-9.7421-004
MFAN	0.0000	9.2896-003	2.9489-003	2.4234-005
TTU	0.0000	0.0000	0.0000	0.0000
SHAF	0.0000	4.5344-001	4.1220-003	4.7825-003
SMHC	0.0000	-3.4051-002	6.8301-004	-4.6298-002
DP25GT	0.0000	3.5028-002	1.3590-003	-8.9200-004
DP25SC	0.0000	1.2468-002	5.8570-004	1.9324-004
				3.0950-002
				5.3197-001
				2.5309-002
				0.0000
				3.6763+000
				-1.2589+000
				1.2850-001

F100 LINEAR MODEL R3/9/4SK 2/24/76

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-2.50000-001)+J(0.00000)	0.00000	1.00000	1 (0.00000)+J(0.00000)	0.000000	0.0000
			2 (0.00000)+J(0.00000)	0.000000	0.0000
			3 (0.00000)+J(0.00000)	0.000000	0.0000
			4 (0.00000)+J(0.00000)	0.000000	0.0000
			5 (0.00000)+J(0.00000)	0.000000	0.0000
			6 (1.00000+000)+J(0.00000)	1.000000	0.0000
			7 (0.00000)+J(0.00000)	0.000000	0.0000
			8 (0.00000)+J(0.00000)	0.000000	0.0000
			9 (0.00000)+J(0.00000)	0.000000	0.0000
			10 (0.00000)+J(0.00000)	0.000000	0.0000
			11 (0.00000)+J(0.00000)	0.000000	0.0000
			12 (0.00000)+J(0.00000)	0.000000	0.0000
			13 (0.00000)+J(0.00000)	0.000000	0.0000
			14 (0.00000)+J(0.00000)	0.000000	0.0000
			15 (0.00000)+J(0.00000)	0.000000	0.0000
			16 (0.00000)+J(0.00000)	0.000000	0.0000
			17 (0.00000)+J(0.00000)	0.000000	0.0000
			18 (0.00000)+J(0.00000)	0.000000	0.0000

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(-5.92011+002)+J(0.00000)	0.00000	1.00000	1 (-1.94045-003)+J(0.00000)	0.0019404	0.0000
			2 (8.18853-004)+J(0.00000)	0.008189	0.0000
			3 (-7.01971-003)+J(0.00000)	0.0070197	0.0000
			4 (0.00000)+J(0.00000)	0.000000	0.0000
			5 (8.47977-003)+J(0.00000)	0.0084798	0.0000
			6 (7.07112-006)+J(0.00000)	0.000071	0.0000
			7 (1.00000+000)+J(0.00000)	1.000000	0.0000
			8 (-1.67126-004)+J(0.00000)	0.001671	0.0000
			9 (1.18256-003)+J(0.00000)	0.011826	0.0000
			10 (-2.62182-004)+J(0.00000)	0.002622	0.0000
			11 (9.86739-005)+J(0.00000)	0.000987	0.0000
			12 (1.31898-005)+J(0.00000)	0.000132	0.0000
			13 (-1.29413-003)+J(0.00000)	0.0012941	0.0000
			14 (-1.88588-002)+J(0.00000)	0.0188588	0.0000
			15 (-7.50489-003)+J(0.00000)	0.0075049	0.0000
			16 (-1.86712-003)+J(0.00000)	0.0018671	0.0000
			17 (-1.09175-005)+J(0.00000)	0.000109	0.0000
			18 (-1.61482-002)+J(0.00000)	0.0161482	0.0000

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(-1.72102+002)+J( 0.00000 ) 0.00000 1.00000
1 (-7.46618-003)+J( 0.00000 ) -.0074662 .00000
2 (-3.00676-003)+J( 0.00000 ) -.0030068 .00000
3 (-3.03298-002)+J( 0.00000 ) -.00303298 .00000
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 (-9.56187-001)+J( 0.00000 ) .9561872 .00000
6 (-1.88464-005)+J( 0.00000 ) -.0000188 .00000
7 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
8 ( 3.43340-004)+J( 0.00000 ) .0003433 .00000
9 ( 6.39106-003)+J( 0.00000 ) .0063911 .00000
10 (-2.88154-002)+J( 0.00000 ) -.0288154 .00000
11 ( 1.30484-002)+J( 0.00000 ) .0130484 .00000
12 ( 1.69632-003)+J( 0.00000 ) .0016963 .00000
13 (-3.30669-002)+J( 0.00000 ) -.0330669 .00000
14 ( 1.45999-002)+J( 0.00000 ) .0145999 .00000
15 ( 5.73796-003)+J( 0.00000 ) .0057380 .00000
16 ( 3.27751-002)+J( 0.00000 ) .0327751 .00000
17 (-1.83591-004)+J( 0.00000 ) -.0001836 .00000
18 (-7.777991-002)+J( 0.00000 ) -.0777991 .00000
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(-5.64891+001)+J( 0.00000 ) 0.00000 1.00000
1 (-7.95637-003)+J( 0.00000 ) -.0079564 .00000
2 (-3.74402-003)+J( 0.00000 ) -.0037440 .00000
3 ( 5.42611-004)+J( 0.00000 ) .0005426 .00000
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 (-3.32695-002)+J( 0.00000 ) -.0332695 .00000
6 (-3.94026-003)+J( 0.00000 ) -.0039403 .00000
7 (-1.31312-001)+J( 0.00000 ) .1313124 .00000
8 (-1.52175-003)+J( 0.00000 ) -.0015217 .00000
9 ( 1.32232-002)+J( 0.00000 ) .0132232 .00000
10 ( 4.12547-003)+J( 0.00000 ) .0041255 .00000
11 ( 2.61939-001)+J( 0.00000 ) .2619386 .00000
12 ( 3.22104-002)+J( 0.00000 ) .0322104 .00000
13 (-3.72675-002)+J( 0.00000 ) -.0372675 .00000
14 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
15 ( 3.77953-001)+J( 0.00000 ) .3779535 .00000
16 ( 1.714821-001)+J( 0.00000 ) .1714821 .00000
17 (-6.91746-003)+J( 0.00000 ) -.0069175 .00000
18 (-9.88868-001)+J( 0.00000 ) -.9888676 .00000
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(-5.061n3+0n1)+J( 0.00000 ) 0.00000 1.00000
1 ( 1.00000-003)+J( 0.00000 ) .0010600 .00000
2 (-4.55325-005)+J( 0.00000 ) .0000455 .00000
3 ( 1.01919-002)+J( 0.00000 ) .0101919 .00000
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 ( 8.07193-003)+J( 0.00000 ) .0080719 .00000
6 ( 1.67089-004)+J( 0.00000 ) .0001671 .00000
7 (-4.67607-002)+J( 0.00000 ) .0046707 .00000
8 (-6.79107-003)+J( 0.00000 ) .0067911 .00000
9 ( 1.34947-002)+J( 0.00000 ) .0134947 .00000
10 ( 1.76831-003)+J( 0.00000 ) .0017683 .00000
11 (-4.32421-002)+J( 0.00000 ) .0432421 .00000
12 (-5.26337-003)+J( 0.00000 ) .0052634 .00000
13 ( 3.55877-004)+J( 0.00000 ) .0035559 .00000
14 (-3.79638-002)+J( 0.00000 ) .0379638 .00000
15 (-1.42540-002)+J( 0.00000 ) .0142540 .00000
16 (-1.28602-002)+J( 0.00000 ) .0128602 .00000
17 (-8.60630-003)+J( 0.00000 ) .0086063 .00000
18 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
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(-4.63680+0n1)+J( 0.00000 ) 0.00000 1.00000
1 (-1.11409-002)+J( 0.00000 ) .0111409 .00000
2 ( 6.37626-003)+J( 0.00000 ) .0063763 .00000
3 ( 1.49169-002)+J( 0.00000 ) .0149169 .00000
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 (-3.88460-003)+J( 0.00000 ) .0038846 .00000
6 (-4.80241-003)+J( 0.00000 ) .0048024 .00000
7 (-4.65669-002)+J( 0.00000 ) .0465669 .00000
8 (-7.55702-003)+J( 0.00000 ) .0075570 .00000
9 ( 3.24445-002)+J( 0.00000 ) .0324445 .00000
10 ( 1.46461-003)+J( 0.00000 ) .0014641 .00000
11 (-5.12878-001)+J( 0.00000 ) .5128786 .00000
12 (-6.18914-002)+J( 0.00000 ) .0618914 .00000
13 (-4.07322-002)+J( 0.00000 ) .0407322 .00000
14 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
15 ( 3.72929-001)+J( 0.00000 ) .3729287 .00000
16 ( 5.96877-002)+J( 0.00000 ) .0596877 .00000
17 (-2.40901-002)+J( 0.00000 ) .0240901 .00000
18 ( 6.39145-001)+J( 0.00000 ) .6391454 .00000
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(-4.48687+001)+J( 0.00000 ) 0.00000 1.00000
1 (-1.24496-002)+J( 0.00000 ) -.012496 .00000
2 (-1.14761-002)+J( 0.00000 ) -.0114761 -.00000
3 (-8.54091-003)+J( 0.00000 ) -.0085409 .00000
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 (-1.80480-002)+J( 0.00000 ) -.0180480 -.00000
6 (-4.96328-003)+J( 0.00000 ) -.0049633 .00000
7 (-8.79318-003)+J( 0.00000 ) -.0087932 .00000
8 (-2.46557-003)+J( 0.00000 ) -.0024656 .00000
9 (-2.36135-002)+J( 0.00000 ) -.0236135 .00000
10 (-2.27686-005)+J( 0.00000 ) -.0000228 .00000
11 (-8.11658-001)+J( 0.00000 ) -.8116584 .00000
12 (-9.75999-002)+J( 0.00000 ) -.0975999 .00000
13 (-9.06890-002)+J( 0.00000 ) -.0906890 .00000
14 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
15 ( 3.71974-001)+J( 0.00000 ) .3719737 .00000
16 ( 4.43687-002)+J( 0.00000 ) .0443687 .00000
17 (-1.86215-002)+J( 0.00000 ) -.0186215 .00000
18 ( 3.82365-001)+J( 0.00000 ) .3823645 .00000
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(-2.07060+001)+J( 3.44658+000) 2.09999+001 .98643
1 ( 4.82723-003)+J(-1.56939-003) .0050759 -18.00996
2 (-1.43082-003)+J(-3.98318-003) .0042324 -109.75911
3 (-3.89054-002)+J(-8.17292-004) -.0389140 -178.79650
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 (-2.46577-002)+J( 3.31787-002) .0413380 126.61869
6 ( 7.25472-004)+J(-7.17555-004) .0010204 -44.68567
7 (-1.23541-001)+J(-4.49095-003) .1236228 -177.91811
8 (-1.53299-002)+J(-2.81118-002) .0320200 -118.60442
9 (-3.47056-002)+J( 1.74059-001) .1774856 101.27631
10 (-5.18724-002)+J( 7.76619-002) .0933923 123.74001
11 (-1.48713-002)+J( 9.24973-002) .0936852 99.13359
12 (-1.11528-003)+J( 9.61346-003) -.0098766 -96.48371
13 (-1.21811-002)+J( 5.12365-002) .0526646 103.37341
14 (-5.61427-002)+J( 7.77847-002) .0959295 125.82066
15 (-1.80931-002)+J( 2.69405-002) -.0324523 -123.88511
16 ( 2.35021-001)+J( 4.20761-002) .2387580 10.15020
17 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
18 ( 6.56590-001)+J(-1.71160-002) .6588122 -1.48889
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(-2.16875+001)+J( 0.00000 ) 0.00000 1.00000
1 (-4.95621-004)+J( 0.00000 ) -.0004956 .00000
2 (-3.34921-003)+J( 0.00000 ) -.0033492 .00000
3 ( 1.68231-002)+J( 0.00000 ) .0168231 .00000
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 ( 5.84814-002)+J( 0.00000 ) .0584814 .00000
6 (-2.29635-004)+J( 0.00000 ) -.0002296 .00000
7 (-1.69995-002)+J( 0.00000 ) -.0169995 .00000
8 (-1.86811-002)+J( 0.00000 ) -.0186811 .00000
9 (-8.74413-002)+J( 0.00000 ) -.0874413 .00000
10 ( 7.55682-002)+J( 0.00000 ) .0755682 .00000
11 ( 5.09831-002)+J( 0.00000 ) .0509831 .00000
12 ( 5.39769-003)+J( 0.00000 ) .0053977 .00000
13 ( 2.50061-002)+J( 0.00000 ) .0250061 .00000
14 ( 2.23086-002)+J( 0.00000 ) .0223086 .00000
15 ( 7.55512-003)+J( 0.00000 ) .0075551 .00000
16 (-1.96368-001)+J( 0.00000 ) -.1963682 .00000
17 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
18 ( 1.20062-001)+J( 0.00000 ) .1200625 .00000
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(-6.54573+000)+J( 0.00000 ) 0.00000 1.00000
1 ( 1.31927-001)+J( 0.00000 ) .1319274 .00000
2 (-1.01277-002)+J( 0.00000 ) -.0101277 .00000
3 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 ( 3.73159-001)+J( 0.00000 ) .3731589 .00000
6 ( 3.91980-003)+J( 0.00000 ) .0039198 .00000
7 ( 1.04861-001)+J( 0.00000 ) .1048607 .00000
8 ( 2.97552-001)+J( 0.00000 ) .2975521 .00000
9 ( 5.52128-001)+J( 0.00000 ) .5521282 .00000
10 ( 2.55318-001)+J( 0.00000 ) .2553180 .00000
11 (-6.20774-002)+J( 0.00000 ) -.0620774 .00000
12 (-2.18724-003)+J( 0.00000 ) -.0021872 .00000
13 (-7.92658-002)+J( 0.00000 ) -.0792658 .00000
14 (-1.14993-001)+J( 0.00000 ) -.0114993 .00000
15 (-1.60692-002)+J( 0.00000 ) -.0160692 .00000
16 ( 1.05744-001)+J( 0.00000 ) .1057440 .00000
17 ( 8.21170-001)+J( 0.00000 ) .8211700 .00000
18 ( 4.26539-001)+J( 0.00000 ) .4265390 .00000
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(-5.01840-001)+J( 0.00000 ) 0.00000 1.00000
1 ( 8.63503-001)+J( 0.00000 ) .8635034 .00000
2 ( 9.53952-001)+J( 0.00000 ) .9539518 .00000
3 ( 1.86405-001)+J( 0.00000 ) .1864049 .00000
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
6 ( 4.05987-002)+J( 0.00000 ) .0405987 .00000
7 ( 4.23660-001)+J( 0.00000 ) .4236602 .00000
8 ( 5.25953-001)+J( 0.00000 ) .5259529 .00000
9 ( 4.10466-001)+J( 0.00000 ) .4104662 .00000
10 ( 9.79211-001)+J( 0.00000 ) .9792114 .00000
11 ( 8.48721-002)+J( 0.00000 ) .0848721 .00000
12 ( 4.78673-001)+J( 0.00000 ) .4786731 .00000
13 ( 7.37588-003)+J( 0.00000 ) .0073759 .00000
14 (-5.24351-002)+J( 0.00000 ) -.0524351 .00000
15 (-6.38666-002)+J( 0.00000 ) -.0638666 .00000
16 (-1.45792-001)+J( 0.00000 ) -.1457920 .00000
17 ( 4.30380-001)+J( 0.00000 ) .4303796 .00000
18 ( 3.41774-002)+J( 0.00000 ) .0341774 .00000
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(-7.14144-001)+J( 0.00000 ) 0.00000 1.00000
1 (-8.68830-001)+J( 0.00000 ) -.8688295 .00000
2 (-8.03930-001)+J( 0.00000 ) -.8039295 .00000
3 (-3.22478-001)+J( 0.00000 ) -.3224785 .00000
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 (-8.90021-001)+J( 0.00000 ) -.8900207 .00000
6 ( 9.50008-003)+J( 0.00000 ) .0095001 .00000
7 (-4.44167-001)+J( 0.00000 ) -.4441668 .00000
8 (-5.40532-001)+J( 0.00000 ) -.5405319 .00000
9 (-4.97636-001)+J( 0.00000 ) -.4976364 .00000
10 (-8.90734-001)+J( 0.00000 ) -.8907337 .00000
11 (-8.30501-002)+J( 0.00000 ) -.0830501 .00000
12 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
13 (-1.29082-002)+J( 0.00000 ) -.0129082 .00000
14 (-1.79970-002)+J( 0.00000 ) -.0179970 .00000
15 (-2.46328-002)+J( 0.00000 ) -.0246328 .00000
16 ( 4.86030-002)+J( 0.00000 ) .0486030 .00000
17 (-5.20052-001)+J( 0.00000 ) -.5200518 .00000
18 (-9.32892-002)+J( 0.00000 ) -.0932892 .00000
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(-1.62340+001)+J( 0.00000 ) 0.00000 1.00000
1 ( 3.84943-003)+J( 0.00000 ) .0038494 .00000
2 ( 3.24928-003)+J( 0.00000 ) .0032493 .00000
3 ( 4.06235-002)+J( 0.00000 ) .0406235 .00000
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 ( 1.99239-002)+J( 0.00000 ) .0199239 .00000
6 ( 1.65456-003)+J( 0.00000 ) .0016546 .00000
7 ( 8.83190-004)+J( 0.00000 ) .0008832 .00000
8 (-1.92358-002)+J( 0.00000 ) -.0192358 .00000
9 ( 1.91304-001)+J( 0.00000 ) .0191305 .00000
10 (-7.56214-002)+J( 0.00000 ) -.0756214 .00000
11 (-1.17344-001)+J( 0.00000 ) -.0117349 .00000
12 (-1.12873-002)+J( 0.00000 ) -.0112873 .00000
13 (-7.96544-002)+J( 0.00000 ) -.0796544 .00000
14 (-1.20167-001)+J( 0.00000 ) -.0120167 .00000
15 (-3.79890-002)+J( 0.00000 ) -.0379890 .00000
16 (-4.01575-001)+J( 0.00000 ) -.0401575 .00000
17 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
18 (-1.30504-001)+J( 0.00000 ) -.1305042 .00000
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(-2.13242+000)+J( 0.00000 ) 0.00000 1.00000
1 (-3.79039-001)+J( 0.00000 ) -.3790392 .00000
2 ( 2.76686-002)+J( 0.00000 ) .0276686 .00000
3 (-3.13268-001)+J( 0.00000 ) -.3132682 .00000
4 ( 0.00000 )+J( 0.00000 ) .0000000 .00000
5 ( 1.25872-002)+J( 0.00000 ) .0125872 .00000
6 ( 4.84226-004)+J( 0.00000 ) .0004842 .00000
7 ( 6.02249-002)+J( 0.00000 ) .0602249 .00000
8 (-2.81785-001)+J( 0.00000 ) -.2817846 .00000
9 (-3.14959-001)+J( 0.00000 ) -.3149599 .00000
10 (-1.67313-001)+J( 0.00000 ) -.1673133 .00000
11 (-1.10027-001)+J( 0.00000 ) -.110027 .00000
12 (-2.86648-002)+J( 0.00000 ) -.0286648 .00000
13 (-1.00020-001)+J( 0.00000 ) -.1000202 .00000
14 (-1.15397-001)+J( 0.00000 ) -.115397 .00000
15 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
16 (-2.20168-001)+J( 0.00000 ) -.220168 .00000
17 (-3.42224-001)+J( 0.00000 ) -.3422243 .00000
18 (-9.81506-002)+J( 0.00000 ) -.0981506 .00000
```


(-1.72803+001)+J(0.00000	1	(4.03358-003)+J(0.00000)	.0040336	.00000
2 (4.47968-004)+J(0.00000	2)	.0004480	.00000
3 (2.18033-002)+J(0.00000	3)	.0218033	.00000
4 (0.00000)+J(0.00000	4)	.0000000	.00000
5 (3.52794-003)+J(0.00000	5)	.0035279	.00000
6 (8.86331-004)+J(0.00000	6)	.0008863	.00000
7 (-4.17355-002)+J(0.00000	7)	.0417355	.00000
8 (-5.72831-003)+J(0.00000	8)	.0057283	.00000
9 (1.37988-001)+J(0.00000	9)	.1379881	.00000
10 (-4.10104-002)+J(0.00000	10)	.0410104	.00000
11 (-5.63462-002)+J(0.00000	11)	.0563462	.00000
12 (-5.55057-003)+J(0.00000	12)	.0055506	.00000
13 (-3.68293-002)+J(0.00000	13)	.0368293	.00000
14 (-6.85664-002)+J(0.00000	14)	.0685664	.00000
15 (-2.20742-002)+J(0.00000	15)	.0220742	.00000
16 (-2.41408-001)+J(0.00000	16)	.2414081	.00000
17 (1.00000+000)+J(0.00000	17)	1.0000000	.00000
18 (3.62355-002)+J(0.00000	18)	.0362355	.00000

(-1.88370+000)+J(0.00000	1	(1.33180-001)+J(0.00000)	.1331802	.00000
2 (-5.35343-002)+J(0.00000	2)	.0535343	.00000
3 (-1.24890-002)+J(0.00000	3)	.0124890	.00000
4 (0.00000)+J(0.00000	4)	.0000000	.00000
5 (-1.38026-001)+J(0.00000	5)	.1380264	.00000
6 (-2.67053-002)+J(0.00000	6)	.0267053	.00000
7 (-1.86884-001)+J(0.00000	7)	.1868842	.00000
8 (9.75705-002)+J(0.00000	8)	.0975705	.00000
9 (2.53534-002)+J(0.00000	9)	.0253534	.00000
10 (2.66420-002)+J(0.00000	10)	.0266420	.00000
11 (9.36602-002)+J(0.00000	11)	.0936602	.00000
12 (-3.20967-002)+J(0.00000	12)	.0320967	.00000
13 (9.56427-002)+J(0.00000	13)	.0956427	.00000
14 (9.40393-002)+J(0.00000	14)	.0940393	.00000
15 (1.00000+000)+J(0.00000	15)	1.0000000	.00000
16 (1.21712-001)+J(0.00000	16)	.1217120	.00000
17 (2.21427-002)+J(0.00000	17)	.0221427	.00000
18 (-1.91994-002)+J(0.00000	18)	.0191994	.00000

F100 LINEAR MODEL 53/9/75K 2/24/76

(-1.00000+0.001)+J(0.00000)	0.00000	1.00000	1	(1.15548-0.01)+J(0.00000)	.1155482	.00000
				2	(3.43644-0.03)+J(0.00000)	.0034364	.00000
				3	(6.90574-0.01)+J(0.00000)	.6905738	.00000
				4	(-7.14935-0.01)+J(0.00000)	-.7149348	.00000
				5	(5.51412-0.02)+J(0.00000)	.0551412	.00000
				6	(9.56526-0.03)+J(0.00000)	.095653	.00000
				7	(-3.79054-0.01)+J(0.00000)	-.3790537	.00000
				8	(3.08301-0.01)+J(0.00000)	.3083012	.00000
				9	(5.04951-0.01)+J(0.00000)	.5049515	.00000
				10	(3.61742-0.01)+J(0.00000)	.3617421	.00000
				11	(-3.35781-0.01)+J(0.00000)	-.3357811	.00000
				12	(-2.39525-0.02)+J(0.00000)	-.0239525	.00000
				13	(-3.14820-0.01)+J(0.00000)	-.3148200	.00000
				14	(-4.26645-0.01)+J(0.00000)	-.4266445	.00000
				15	(-1.07013-0.01)+J(0.00000)	-.1070133	.00000
				16	(-2.78388-0.01)+J(0.00000)	-.2783881	.00000
				17	(1.00000+0.00)+J(0.00000)	1.0000000	.00000
				18	(-1.19112-0.02)+J(0.00000)	-.0119112	.00000

D.3 SELECTED REDUCED ORDER MODELS

D.3.1 Definition of Reduction Matrices (see Chapter IV)

Modal Decomposition

$$\dot{\delta x} = F\delta x + G\delta u$$

$$\delta x = Tz$$

$$FT = T\Lambda$$

where

Λ is block diagonal

Partition:

$$\begin{bmatrix} \dot{z}_1 \\ \vdots \\ \dot{z}_2 \end{bmatrix} = \begin{bmatrix} \Lambda_1 & 0 \\ \vdots & \vdots \\ 0 & \Lambda_2 \end{bmatrix} \begin{bmatrix} z_1 \\ \vdots \\ z_2 \end{bmatrix} + \begin{bmatrix} \Xi_1 \\ \vdots \\ \Xi_2 \end{bmatrix} u$$

$$\begin{bmatrix} \delta x_1 \\ \vdots \\ \delta x_2 \end{bmatrix} = \begin{bmatrix} T_{11} & T_{12} \\ \vdots & \vdots \\ T_{21} & T_{22} \end{bmatrix} \begin{bmatrix} z_1 \\ \vdots \\ z_2 \end{bmatrix}$$

$$\delta y = \begin{bmatrix} H_1 & H_2 \end{bmatrix} \begin{bmatrix} \delta x_1 \\ \vdots \\ \delta x_2 \end{bmatrix} + D\delta u$$

Reduction:

$$\delta \dot{x}_1 = F_r \delta x_1 + G_r \delta u$$

$$\delta y = H_r \delta x_1 + D_r \delta u$$

$$\delta x_2 = H^* \delta x_1 + D^* \delta u$$

Table D.9 shows the equivalence of the above matrix names and the listing.

D.3.2 Normalization

Matrices are normalized as in Section D.2. The eigensystem shown is not normalized and matrices listed at the end are the final reduced, unnormalized system.

D.3.3 Case Index

Table D.10 lists the cases included.

Table D.9
Index of Reduction Matrices
(In order of appearance in printout)

MATRIX	TITLE
Λ_1	LAMBDA1
T_{11}	T_{11}
Ξ_1	XI1
T_{21}	T_{21}
T_{22}	T_{22}
Λ_2	LAMBDA2
T_{12}	T_{12}
H_1	H_1
H_2	H_2
Ξ_2	XI2
T_{11}^{-1}	T_{11} INVERSE
F_r	FT
Λ_2^{-1}	LAMBDA2 INVERSE
G_r	GR
H^*	H^*
H_r	HR
D^*	D^*
D_r	DR
F,G,H,D	Unnormalized Output

Table D.10
Index to Model Reductions

CASE	PLA (DEG)	ALTITUDE (FT)	MACH NO.
1	83	45,000	0.9
2	83	30,000	0.9
3	83	0	0
4	83	0	1.2
5	20	30,000	0.9
6	20	0	0
7	52	0	0

CASE 1

THE REDUCED MATRICES FR*GR*HR*DR WILL BE SAVED FOR OPTSYS ON FILE 12
INTERMEDIATE DATA WILL BE READ FROM RECORD NO. 2 OF FILE 10

THESE WILL BE 12 EIGENVALUES ELIMINATED. THE TOLERANCE LEVEL FOR ELIMINATION IS .100
1 OF THESE EIGENVALUES ARE COMPLEX. TO BE ELIMINATED ARE--

(-.250000+000i .000000)
(-.592000+000i .000000)
(-.564000+002i .000000)
(-.506000+002i .000000)
(-.483000+002i .000000)
(-.344000+002i .000000)
(-.207000+002i .344000+001i)
(-.215000+002i .000000)
(-.710000+000i .000000)
(-.162000+002i .000000)
(-.172000+002i .000000)
(-.213000+001i .000000)

THE IDENTIFYING TITLE FOR F*GR*HR*DR ON OPTSYS OUPUT =REDUCED MATRICES .9/45K 83 FIFTH ORDER

F100 LINEAR MODEL .9/85K H3 3/5/76

LAMBDA1

	1	2	3	4	5
1	-1.7219+002	0.0000	0.0000	0.0000	0.0000
2	0.0000	-6.5857+000	0.0000	0.0000	0.0000
3	0.0000	0.0000	-5.6164+001	0.0000	0.0000
4	0.0000	0.0000	0.0000	-1.8837+000	0.0000
5	0.0000	0.0000	0.0000	0.0000	-1.0000+001

T11

	1	2	3	4	5
1	-7.0662-003	1.3193+001	8.6350+001	1.3318+001	1.1555+001
2	-3.0068-003	-1.0125+002	9.5395+001	-5.3534+002	3.4364+003
3	-3.0330-002	1.0003+000	1.8640+001	-1.2489+002	6.9057+001
4	0.0000	0.0000	0.0000	0.0000	-7.1493+001
5	9.5619-001	3.7314+001	1.0000+000	-1.3803+001	5.5191+002

XT1

	1	2	3	4	5
1	-3.5752-001	3.4308+000	3.4263+002	5.8523+001	-2.0373+002
2	0.0000+000	-6.2729+000	1.0352+002	-1.7632+002	-4.4472+000
3	2.5448+001	1.9406+001	-5.5718+004	-7.7295+004	5.1628+002
4	7.7338+001	1.5482+000	-1.1421+002	1.0983+002	1.7148+002
5	-1.3947+001	0.0000	0.0000	0.0000	0.0000

F100 LINEAR MODEL .0/0CK A3 3/5/76

T21

	1	2	3	4	5
1	-1.8826-005	3.0188-003	0.0599-002	-2.6705-002	9.5653-003
2	1.0000+000	1.0000+000	0.2336-001	-1.8688-001	-3.7905-001
3	1.0333-004	2.0785-001	0.2595-001	0.7571-002	3.0830-001
4	5.1011-003	5.5215-001	0.1007-001	2.5353-002	5.0495-001
5	-2.8815-002	2.5532-001	0.7921-001	2.6842-002	3.6174-001
6	1.3048-002	-0.2077-002	0.0076-002	0.3660-002	-3.3578-001
7	1.4043-003	-2.1872-003	0.7887-001	-3.2097-002	-2.3953-002
8	-1.3047-002	-7.0266-002	7.1758-003	0.5643-002	-3.1982-001
9	1.4000-002	-1.1409-001	-5.2435-002	0.0039-002	-4.2664-001
10	5.7380-003	-1.6069-002	-6.3867-002	1.0000+000	-1.0701-001
11	3.2775-002	1.0574-001	-1.4579-001	1.2171-001	-2.7839-001
12	-1.8359-004	3.2117-001	4.1038-001	2.2143-002	1.0000+000
13	-7.7799-002	0.2654-001	3.0177-002	-1.9199-002	-1.1191-002

T22

	1	2	3	4	5	6	7	8	9	10
1	1.0000+000	7.0771-006	-3.9403-003	1.6709-004	-4.8024-003	-4.9633-003	-2.6968-003	0.9589-004	-2.2963-004	9.5001-003
2	0.0000	1.0000+000	-1.3131-001	-4.6761-002	-4.6567-002	8.7932-003	3.0287-001	1.6370-001	-1.6999-002	-4.4417-001
3	0.0000	-1.6713-000	-1.5217-003	-6.7911-003	-7.5570-003	-2.4656-003	3.5719-003	8.9101-002	-1.8881-002	-5.4053-001
4	0.0000	1.1226-003	1.3225-002	1.3499-002	3.2845-002	2.3614-002	3.0148-001	-3.9169-001	-8.7441-002	-4.9764-001
5	0.0000	-2.4219-004	0.1225-003	1.7683-003	1.4641-003	-2.2769-005	2.2535-001	-1.2985-001	7.5568-002	-6.9073-001
6	0.0000	0.8670-005	2.6194-001	-4.3242-002	-5.1288-001	-8.1166-001	1.5129-001	-2.1256-001	5.0983-002	-8.3050-002
7	0.0000	1.3100-002	3.2210-002	-5.2634-003	-6.1891-002	-9.7600-002	1.4897-002	-2.3122-002	5.3977-003	1.0000+000
8	0.0000	-1.2941-003	-3.7268-002	3.5588-004	-4.0732-002	-9.0689-002	9.3650-002	-1.1287-001	2.5006-002	-1.2908-002
9	0.0000	-1.8259-002	1.0000+000	-3.7984-002	1.0000+000	1.0000+000	2.3610-001	-1.2489-001	2.2309-002	-1.7997-002
10	0.0000	-2.5049-003	3.7795-001	1.4254-002	3.7293-001	3.7197-001	7.8420-002	-4.4923-002	7.5551-003	-2.4633-002
11	0.0000	-1.8671-003	1.7148-001	-1.2860-002	5.9688-002	4.4369-001	-5.3478-001	-3.9512-001	-1.9637-001	4.8803-002
12	0.0000	-1.0918-005	-6.9175-003	0.6063-003	-2.4090-002	-1.8622-002	-2.4964-000	-1.2343-000	1.0000+000	-5.2005-001
13	0.0000	-1.6104-002	-9.8647-001	1.0000+000	6.3915-001	3.6236-001	-1.6653+000	-7.7015-001	1.2006-001	-9.3289-002

T22

	11	12	13
1	1.6506-003	5.8633-004	4.8423-004
2	0.0000	-1.1716-002	6.0223-002
3	-1.0236-002	-5.7283-003	-2.8178-001
4	1.0130-001	1.3793-001	-3.1496-001
5	-7.5621-002	-4.1010-002	-1.6731-001
6	-1.1730-001	-5.4506-002	-1.1008-001
7	-1.1287-002	-5.5506-003	2.8643-002
8	-7.0654-002	-1.6429-002	-1.0002-001
9	-1.2017-001	-6.8566-002	-1.1500-001
10	-3.7849-002	-5.2074-002	1.0000+000
11	-4.0156-001	-2.4101-001	-2.2017-001
12	1.0000+000	1.0000+000	-3.4222-001
13	-1.3050-001	3.6278-002	-9.8151-002

LAYER 2

	1	2	3	4	5	6	7	8	9	10
1	-2.5000+001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
2	-5.0201+002	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
3	0.0000	0.0000	-5.4489+001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4	0.0000	0.0000	0.0000	-5.0610+001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000	0.0000	-4.6368+001	0.0000	0.0000	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.0000	0.0000	0.0000	-4.4869+001	0.0000	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-2.0706+001	3.4466+000	0.0000	0.0000
8	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-3.4466+000	-2.0706+001	0.0000	0.0000
9	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-2.1887+001	0.0000
10	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-7.1415+001
11	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
12	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
13	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

LAYER 2

	11	12	13
1	0.0000	0.0000	0.0000
2	0.0000	0.0000	0.0000
3	0.0000	0.0000	0.0000
4	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.0000
8	0.0000	0.0000	0.0000
9	0.0000	0.0000	0.0000
10	0.0000	0.0000	0.0000
11	-1.6236+001	0.0000	0.0000
12	0.0000	-1.7200+001	0.0000
13	0.0000	0.0000	-2.1524+000

T12

	1	2	3	4	5	6	7	8	9	10
1	0.0000	-1.0000+003	-7.9560+003	1.0600+003	-1.1141+002	-1.2450+002	-1.3988+002	-2.0403+003	-4.9562+004	-8.6883+001
2	0.0000	4.1885+002	-3.7440+003	-4.5532+005	6.3763+003	1.1476+002	-1.3444+003	1.1710+002	-3.3492+003	-8.0393+001
3	0.0000	-7.0197+003	5.4261+004	1.0192+002	1.4917+002	8.5409+003	9.6116+002	5.0061+002	1.6823+002	-3.2248+001
4	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	5.0708+003	-3.1249+002	8.0719+003	-3.8846+003	-1.8048+002	1.0251+001	-5.2394+002	5.8481+002	-8.9002+001

T12
 1 1.0000-001 1.0000-001 1.0000-001
 2 1.0000-001 1.0000-001 1.0000-001
 3 1.0000-001 1.0000-001 1.0000-001
 4 1.0000-001 1.0000-001 1.0000-001
 5 1.0000-001 1.0000-001 1.0000-001

H1
 1 2.4104-001 -9.5405-001 -1.8575-001 -4.5916-001 2.7578-001
 2 6.0558-001 3.5010-000 0.0000 0.0000 0.0000
 3 0.0000 0.0000 0.0000 0.0000 0.0000
 4 1.3727-001 6.0009-001 -4.7534-000 2.4292-002 4.2481-002
 5 1.2724-000 1.1586-001 5.1152-000 9.031-001 -7.2306+000
 6 1.8575-001 -3.5102-001 -6.1928-001 -7.9583-002 4.9804-002
 7 1.0331-001 6.1723-002 -1.8679-001 -1.8241-002 -2.2531-003

H2
 1 0.0000 1.0000-001 9.1185-001 1.3184-001 -1.2155-002 2.0179-001 8.7245-002 -5.3205-001 7.2107-002 7.3443-002
 2 0.0000 0.0000 -1.5008-000 3.5025-004 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 3 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 4 0.0000 1.4786-001 3.9772-001 5.8519-001 8.4631-002 1.0284-001 9.1097-002 5.8182-002 9.1427-002 9.4959-002
 5 0.0000 -1.6320-001 -6.4331-000 -6.3354-001 -9.2582-002 -1.1307-001 -1.0180-001 -6.3368-002 -1.0155-001 -1.0500-001
 6 0.0000 1.0400-002 3.8755-001 1.6677-001 1.1137-002 1.3235-002 1.2235-002 7.6200-003 1.2220-002 1.2411-002
 7 0.0000 5.1630-003 3.0515-002 5.9224-002 2.8976-003 3.4693-003 3.2664-003 1.9077-003 3.2678-003 3.2076-003

H3
 1 7.1004-001 2.3047-001 7.1554-002
 2 0.0000 0.0000 0.0000
 3 0.0000 0.0000 0.0000
 4 9.1768-002 9.2332-003 9.0668-002
 5 1.0204-001 -1.0370-002 -1.0023-001
 6 1.2305-002 1.2394-003 1.2335-002
 7 1.2785-003 2.8514-004 3.2555-003

XT2

	1	2	3	4	5
1	9.7142-002	7.4650-002	-2.0655-004	2.2425-004	1.3452-001
2	-3.7215+000	2.1220+001	-3.4580-001	-1.2845+000	9.8585-001
3	4.1444+001	1.5214+001	4.0181-002	9.5703-001	-2.3396+002
4	1.0642+002	4.6380+001	5.6206-002	2.1415+000	-5.2492+002
5	-1.8719+002	-4.6388+001	1.6553-001	-2.9877+000	6.9645+002
6	1.2145+002	4.8690+001	1.1734-001	2.1242+000	-4.8651+002
7	1.8197+001	7.6704+000	4.0155-002	1.2459-001	-3.5528+000
8	5.7177+000	1.7233+000	6.8152-002	-7.1150+003	-3.1256+000
9	3.8435-001	-1.3601+001	-1.2612-001	1.7833-001	-4.5636+001
10	1.2453-001	1.0910+001	3.9347-004	1.2339-003	3.1105-001
11	-4.2756+001	-7.3283+001	-5.7406-001	-4.3450-001	-9.8557+001
12	1.6724+002	1.1309+002	8.4246-001	5.6319-001	1.3705+002
13	-1.1254+001	-1.1224+000	1.0921-002	-1.0286-002	8.3022-001

T11 INVERSE

	1	2	3	4	5
1	4.5053-001	-1.4044+000	-4.5936-001	-2.9672-001	1.0304+000
2	2.4770-002	-2.4065+001	9.8282-001	9.5451-001	3.0593-002
3	3.1026+001	7.7024+001	-3.4530-002	2.0782-002	3.7494+003
4	5.0982+000	-4.8287+000	-7.7544+001	1.1664-001	3.1510+003
5	0.0000	0.0000	0.0000	-1.3987+000	0.0000

FR

	SNEAN	SNECM	PT7W	WFCOM	PT3
SNEAN	-2.6041-001	-7.5613+001	-1.2332+000	3.6608-001	1.2955+000
SNECM	5.2773-001	-1.6443+000	-2.3196-001	-4.1270-002	5.3383-001
PT7W	2.3336+000	-5.0154+000	-8.8862+000	1.8241+000	5.1796+000
WFCOM	0.0000	0.0000	0.0000	-1.0000+001	0.0000
PT3	-7.0045+001	2.3017+002	7.3034+001	4.7299+001	-1.6973+002

FIG 1 LINEAR MODEL .9/454 R3 3/5/76

UNNORMALIZED EIGENSYSTEM.

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-1.72192+0.02j)+j(0.00000)	0.00000	1.00000	1 (-7.81727-001)+j(0.00000) 2 (-3.98969-001)+j(0.00000) 3 (-3.52501-003)+j(0.00000) 4 (0.00000)+j(0.00000) 5 (1.00000+000)+j(0.00000)	-7817274 -3989693 -0035250 0000000 1.0000000	.00000 .00000 .00000 .00000 .00000
(-1.58370+0.00j)+j(0.00000)	0.00000	1.00000	1 (1.00000+000)+j(0.00000) 2 (-5.09420-001)+j(0.00000) 3 (-1.04093-004)+j(0.00000) 4 (0.00000)+j(0.00000) 5 (-1.03520-002)+j(0.00000)	1.0000000 -5094204 -0001041 0000000 -0103520	.00000 .00000 .00000 .00000 .00000
(-4.58573+0.00j)+j(0.00000)	0.00000	1.00000	1 (1.00000+000)+j(0.00000) 2 (-9.72878-002)+j(0.00000) 3 (8.41394-003)+j(0.00000) 4 (0.00000)+j(0.00000) 5 (2.82511-002)+j(0.00000)	1.0000000 -0972878 0084139 0000000 0282511	.00000 .00000 .00000 .00000 .00000
(-5.81840-0.01j)+j(0.00000)	0.00000	1.00000	1 (7.14255-001)+j(0.00000) 2 (1.00000+000)+j(0.00000) 3 (1.71152-004)+j(0.00000) 4 (0.00000)+j(0.00000) 5 (8.26208-003)+j(0.00000)	7142552 1.0000000 0001712 0000000 0082621	.00000 .00000 .00000 .00000 .00000
(-1.00000+0.01j)+j(0.00000)	0.00000	1.00000	1 (-5.90192-001)+j(0.00000) 2 (-2.22445-002)+j(0.00000) 3 (-3.91539-003)+j(0.00000) 4 (1.00000+000)+j(0.00000) 5 (-2.81324-003)+j(0.00000)	-5901923 -0222445 -0039154 1.0000000 -0028132	.00000 .00000 .00000 .00000 .00000

LAMRDAR INVERSE												
	1	2	3	4	5	6	7	8	9	10		
1	-4.0000+000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		
2	0.0000	-1.4802-003	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		
3	0.0000	0.0000	-1.7703-002	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		
4	0.0000	0.0000	0.0000	-1.9759-002	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		
5	0.0000	0.0000	0.0000	0.0000	-2.1567-002	0.0000	0.0000	0.0000	0.0000	0.0000		
6	0.0000	0.0000	0.0000	0.0000	0.0000	-2.2267-002	0.0000	0.0000	0.0000	0.0000		
7	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-4.8993-002	0.0000	0.0000	0.0000		
8	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	7.8221-003	-7.8221-003	0.0000	0.0000		
9	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-4.6110-002	0.0000	0.0000		
10	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-1.4003+000		
11	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		
12	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		
13	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		

LAMRDAR INVERSE												
	11	12	13									
1	0.0000	0.0000	0.0000									
2	0.0000	0.0000	0.0000									
3	0.0000	0.0000	0.0000									
4	0.0000	0.0000	0.0000									
5	0.0000	0.0000	0.0000									
6	0.0000	0.0000	0.0000									
7	0.0000	0.0000	0.0000									
8	0.0000	0.0000	0.0000									
9	0.0000	0.0000	0.0000									
10	0.0000	0.0000	0.0000									
11	-6.1584-002	0.0000	0.0000									
12	0.0000	-5.7816-002	0.0000									
13	0.0000	0.0000	-4.6695-001									

GP	WFSH	AMTX	CTVV	RCVV	BLC
SNEAN	-6.5504-002	-1.0301-001	-2.7750-003	-1.2615-003	2.8534-001
SNECM	8.8873-003	1.9113-002	1.4052-003	-4.5590-003	5.7858-001
PTV	-1.6153-001	-5.1386-000	8.3741-003	-2.7330-002	-3.4075-001
WFCOM	1.0000+001	0.0000	0.0000	0.0000	0.0000
PT3	-8.0577+000	-5.5305+000	-1.2039-001	5.7571-001	-1.9632+002

FILED MODEL 9/05X 3/5/76

H#	FMX	MEAN	TTU	SMAF	SMC
SNAF	-1.3315-001	1.5028-001	2.3138-002	-1.1903-002	1.6857-004
SNAF	-4.3306-001	-2.0348-001	-2.2601-001	3.2057-001	1.0346+000
PTU	7.0717-001	1.1986-001	1.9846-001	-1.2500-001	1.1739-002
MECH	2.3336-001	4.4828-002	5.0567-001	-1.6969-001	2.5095-002
PTU	4.4444-001	6.1220-001	2.0954-001	-2.3024-001	-1.8125-002
PTU	5.0495-001	3.0089-001	-1.4272-001	0.1925-001	1.2160-002
PTU	-2.7235-002	5.2183-001	5.4319-003	3.7110-002	3.3746-003
TTU	5.1009-001	3.9010-001	-1.3713-001	3.9280-001	-3.6169-002
TTU	5.0444-001	-4.4666-001	1.9064-001	0.9254-001	1.1626-002
TTU	5.0406+000	-4.8320+000	7.9167-001	2.4795-001	8.3324-003
TTU	6.0144-001	7.7217-001	4.7438-004	0.9175-001	3.6844-002
TTU	2.7553-001	2.2387-002	7.7512-001	-4.0333-001	2.6616-002
TTU	-1.2014-001	1.2329-001	4.6666-001	4.4535-001	-6.7049-002

H#	FMX	MEAN	TTU	SMAF	SMC
SNAF	1.2570+000	-1.0597+000	-1.4253-004	-4.9790-002	1.4594+000
SNAF	4.3558-001	3.4819-004	-2.3537-003	9.7807-003	7.0283-006
PTU	5.1000-001	3.0010-001	-1.3713-001	3.9280-001	-3.6169-002
SMC	-4.2896-001	1.4353-001	4.6177+000	2.2049-001	2.0280-001
SMC	-4.2013-000	1.3076+001	3.4073+000	1.5403+000	-7.4880+000
DOFSC	5.5978-001	0.4373-001	4.7835-001	-1.1745-001	7.8178-002
DOFSC	1.6453-001	4.1261-002	-1.2507-001	-2.3349-002	4.3396-003

H#	FMX	MEAN	TTU	SMAF	SMC
SNAF	3.0607-001	3.2825-001	-1.0868-003	1.1683-003	5.4837-001
SNAF	-2.7052-002	4.1304-002	-1.4375-003	-1.9737-003	-2.6190-001
PTU	4.4564-002	4.1121-002	1.0042-003	-0.9153-005	1.2735-001
PTU	1.6643-001	2.3379-001	1.5699-004	2.3910-004	1.0894-001
PTU	1.4321-001	9.2003-002	6.0784-004	2.6359-003	2.3628-003
PTU	-5.5647-002	4.1283-002	9.2847-004	-5.6599-004	6.1172-001
PTU	2.3475-001	2.1957-001	-6.7150-004	2.3347-003	6.8505-001
TTU	1.2910+002	5.0935-002	8.5118-004	-6.1235-004	6.7236-001
TTU	-5.3737-002	4.9519-002	7.1964-004	-9.6409-004	5.5076-001
TTU	-1.5647-001	-1.5328+000	1.0560-002	-1.3865-002	1.3905-000
TTU	-1.5774-001	1.1097-001	1.0912-003	-1.2191-003	9.3546-001
TTU	4.2662-001	4.0610-001	4.7203-005	1.2604-003	4.2635-001
TTU	-1.4224-001	1.0003-001	-1.1745-003	1.1800-003	4.9121-001

F100 LINEAR MODEL .9/454 R3 3/5/76

DE	MEAN	AMTX	CIVV	RCVV	PLC
EVXX	0.850-003	2.1053-001	3.1277-003	-0.2815-003	1.1679+000
MEAN	2.7085-005	0.1650-003	2.0485-003	2.4541-005	2.5347-002
TTU	1.2410-002	5.025-002	8.5114-004	-0.1235-004	6.7236-001
SUB	1.8175-002	5.0733-001	5.1740-003	3.9598-003	4.1607+000
SUBC	-0.7434-001	-3.8485-001	-7.1844-003	-4.4764-002	-2.7730+000
DEPCT	3.8152-002	7.0374-002	1.0014-003	-0.5661-004	2.6329-001
DEPCT	7.7445-003	2.5045-002	6.7143-004	1.9470-004	6.0645-002

UNIT 11 VERIFICATION, 231-04-0450-5
 PROCESSOR BY DRIVER 1100 SERIES FLT PROCESSOR LEVEL W8 AT 3104:43 PM ON FRIDAY, MARCH 5, 1976 (CREATING CYCLE 0)

1.	F				REDUCED MATRICES	.9/45K	83	FIFTH ORDER
2.		9605+00	5965+00	1111+04	1337+01	1297+03		
3.		7955+00	1644+01	2648+03	1910+00	6773+02		
4.		2500+02	5181+02	6885+01	7394+02	5756+00		
5.		0000	0000	0000	1000+02	0000		
6.		7434+00	1816+01	8572+03	1725+01	1697+03		
7.	G			REDUCED MATRICES	.9/45K	83	FIFTH ORDER	
8.		2392+00	3610+03	2723+02	8001+01	2600+04		
9.		4113+01	2088+02	1747+02	1417+02	7194+04		
10.		4524+03	2077+02	9120+01	7441+01	3711+01		
11.		1000+02	0000	0000	0000	0000		
12.		2939+00	1030+03	1239+02	1411+02	1924+05		
13.	HY			REDUCED MATRICES	.9/45K	83	FIFTH ORDER	
14.		3705+00	4559+00	4317+01	7515+01	4308+02		
15.		4335+02	1905+05	1318+01	2221+03	4375+05		
16.		1405+00	6004+01	3614+02	4196+00	1059+01		
17.		2048+03	1862+05	6021+01	1165+04	2939+03		
18.		6201+04	1524+03	4789+01	8306+04	1107+01		
19.		5705+04	1729+04	4302+01	4372+04	7977+03		
20.		1677+04	3314+05	1152+01	8706+05	4938+04		
21.	DY			REDUCED MATRICES	.9/45K	83	FIFTH ORDER	
22.		5229+02	2842+03	9048+01	3097+01	3379+04		
23.		6354+04	2000+00	1799+00	3743+03	1546+01		
24.		1379+01	5129+02	2443+01	4394+00	1930+04		
25.		9607+04	2873+01	7355+03	1406+03	5909+00		
26.		2549+04	1901+01	1070+02	1621+02	4019+00		
27.		1414+04	2450+01	1901+02	2397+03	2633+00		
28.		2607+05	6047+02	6714+03	4467+04	6065+01		

THE REDUCED MATRICES FR,GP,WR,ND WILL BE SAVED FOR OPTSYS ON FILE 12
 INTERMEDIATE DATA WILL BE READ FROM RECORD NO. 8 OF FILE 10

CASE 2

THERE WILL BE 9 EIGENVALUES ELIMINATED. THE TOLERANCE LEVEL FOR ELIMINATION IS .100
 3 OF THESE EIGENVALUES ARE COMPLEX, TO BE ELIMINATED ARE--

(-.250000+.000000)
 (-.400800+.000000)
 (-.431000+.000000)
 (-.500000+.000000)
 (-.391000+.000000)
 (-.550000+.000000)
 (-.150000+.000000)
 (-.220000+.000000)
 (-.175000+.000000)

THE IDENTIFYING TITLE FOR FR,GP,WR,ND ON OPTSYS OUTPUT REDUCED MATRICES .9/30K 83 FIFTH ORDER

F100 LINEAR MODEL -9/30X A3 3/4/76

L4R041

	1	2	3	4	5
1	-2.1327+002	0.0000	0.0000	0.0000	0.0000
2	0.0000	-1.7691+000	0.0000	0.0000	0.0000
3	0.0000	0.0000	-2.1084+000	0.0000	0.0000
4	0.0000	0.0000	0.0000	-9.7423+000	0.0000
5	0.0000	0.0000	0.0000	0.0000	-1.0000+001

T11

	1	2	3	4	5
1	-1.0633+002	1.0000+000	1.0000+000	6.1742+002	6.1056+002
2	-2.1103+003	1.3300+001	-8.3426+003	4.1500+002	4.4100+002
3	-1.4893+002	-2.1037+001	-1.4135+001	1.0000+000	9.9686+001
4	0.0000	0.0000	0.0000	0.0000	-4.0182+002
5	6.2039+001	-4.8443+001	-6.6546+001	3.0734+001	2.9534+001

X11

	1	2	3	4	5
1	-1.5110+001	3.3401+001	-2.6151+001	6.0436+002	-5.1850+002
2	2.3412+000	1.8885+000	8.2194+005	-4.5755+002	-4.1443+000
3	-2.5401+000	-1.3064+000	-5.5174+003	5.7571+002	4.0466+000
4	2.0712+002	-7.0765+000	-1.2034+003	-2.7869+002	-9.4846+000
5	-2.4887+002	0.0000	0.0000	0.0000	0.0000

T21

	1	2	3	4	5
1	-2.7148-005	-1.1580-001	-9.8612-002	-2.5124-003	-2.0782-003
2	1.0000+000	-5.0455-002	-1.0729-001	6.0216-001	5.0850-001
3	4.3371-003	4.4673-001	4.8695-001	7.2369-002	6.3671-002
4	3.6610-003	3.2471-001	3.4981-001	5.0056-001	5.0453-001
5	-1.9047-002	4.5185-001	3.6824-001	2.1436-001	2.1422-001
6	1.2422-002	6.2172-001	6.4500-001	4.1866-002	2.1480-002
7	1.6223-003	-2.3509-001	-1.6667-001	2.9139-003	1.5281-003
8	-4.4011-002	6.0952-001	6.5685-001	1.8474-002	1.0431-003
9	-7.3642-003	7.6741-001	8.2100-001	1.2303-001	1.0521-001
10	1.7243-002	7.7747-001	8.0087-001	3.4920-001	3.2688-001
11	3.0433-004	3.2555-001	3.5568-001	9.6782-001	1.0000+000
12	-2.6143-002	8.4333-003	3.4314-002	6.6394-001	6.0642-001

T22

	1	2	3	4	5	6	7	8	9	10
1	1.0000+000	-8.4300-005	3.1109-003	2.4430-003	2.9152-007	-1.0658-004	-1.6421-001	-7.8977-005	9.8144-003	3.9738-003
2	0.0000	1.0000+000	1.8414-002	1.8963-001	-3.9923-004	-4.5586-002	5.7071-003	-1.8830-001	4.4813-002	-6.4500-001
3	0.0000	4.4066-003	3.8158-002	-1.2200-001	1.9334-004	8.7705-003	7.3753-002	3.2514-001	-2.2225-001	3.6745-001
4	0.0000	2.1911-003	-2.1120-002	-3.2264-002	4.4350-004	-4.5343-003	2.1460-002	1.2349-001	-2.3803-001	-1.1475-001
5	0.0000	-5.7805-003	-4.9299-002	1.6940-002	-2.4304-004	-4.4354-004	1.5043-001	-1.4610-001	-5.0372-001	-1.3405-001
6	0.0000	2.0715-003	2.2181-001	4.9300-001	-1.7590-003	1.0000+000	1.9481-001	-6.1857-001	-7.3143-001	-8.3007-001
7	0.0000	3.9151-004	3.3448-002	1.0995-001	-2.1128-004	1.1634-001	1.0000+000	-7.4043-002	-6.6160-002	-8.8883-002
8	0.0000	-2.3055-002	-5.4951-001	2.9015-001	2.1040-005	2.3540-001	1.9523-001	-3.2822-001	-5.9306-001	-3.8360-001
9	0.0000	-2.0830-002	-3.0004-001	1.3000-000	1.2495-001	7.9582-002	2.0780-001	-6.0424-001	-8.2283-001	-6.7621-001
10	0.0000	2.0270-003	2.2520-001	4.0317-001	-6.5002-005	-3.2104-002	1.6368-001	-1.7662-000	-3.0349-001	1.8148-000
11	0.0000	3.0644-004	-1.7230-003	9.8268-003	-2.3936-004	5.7776-003	1.4500-002	-2.8397-001	-6.5232-001	1.5115+000
12	0.0000	-5.4725-003	1.1811-000	-4.5265-001	1.0000+000	-3.0552-001	-7.7195-002	-2.0469-000	2.2354-001	2.6009+000

T23

	11	12
1	4.4656-004	7.1443-004
2	-0.0546-002	6.7842-002
3	-5.6607-002	-2.4019-002
4	3.1001-001	1.3577-001
5	6.2362-002	-5.8505-002
6	-1.3520-002	9.3806-002
7	-9.0545-004	-9.2440-003
8	-2.1002-002	-6.1404-002
9	-5.0941-002	-7.7662-002
10	6.0154-001	-4.1224-001
11	-2.3232-000	1.0000+000
12	-7.1937-004	-1.5075-001

LAMPD42

	1	2	3	4	5	6	7	8	9	10
1	-2.5000-001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
2	0.0000	-4.0001+002	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
3	0.0000	0.0000	-4.3172+001	3.2303+001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4	0.0000	0.0000	-3.2363+001	-4.3178+001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000	0.0000	-5.0012+001	0.0000	0.0000	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.0000	0.0000	0.0000	-3.9164+001	0.0000	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-5.5142+001	0.0000	0.0000	0.0000
8	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-1.6054+001	7.2603+000	0.0000
9	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-7.2603+000	-1.6054+001	0.0000
10	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-2.2613+001
11	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-4.5085+001
12	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

LAMPD42

	11	12
1	0.0000	0.0000
2	0.0000	0.0000
3	0.0000	0.0000
4	0.0000	0.0000
5	0.0000	0.0000
6	0.0000	0.0000
7	0.0000	0.0000
8	0.0000	0.0000
9	0.0000	0.0000
10	4.5085+001	0.0000
11	-2.2613+001	0.0000
12	0.0000	-1.7340+001

T12

	1	2	3	4	5	6	7	8	9	10
1	0.0000	-5.7446+003	1.0256+003	-9.7617+003	3.1902+005	3.8613+003	2.7687+001	4.8155+002	2.6245+002	8.9459+002
2	0.0000	1.0251+003	2.7725+003	-4.2611+002	1.2707+005	-3.1806+002	1.2737+001	1.7652+002	3.9213+002	7.0083+002
3	0.0000	-3.9758+003	4.4404+002	-2.9459+001	-7.6315+005	2.2775+002	-2.2269+001	2.3884+001	-9.0347+002	-2.3781+002
4	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	1.7354+001	5.1459+001	7.8703+001	-1.0337+004	-1.2487+002	-1.3844+001	-1.3547+002	2.5266+001	-9.7630+001

T12

	11	12
1	-2.9475+003	9.0343+004
2	-4.6905+003	9.0003+003
3	-1.0149+001	9.1601+002
4	0.0000	0.0000
5	4.0851+002	2.8024+002

H1

	1	2	3	4	5
1	1.3005-001	9.2763-001	2.0000-001	1.5079-001	2.3644-001
2	4.0260-001	4.0014-004	2.0023-003	5.9453-003	-9.7154-004
3	0.0000	0.0000	0.0000	0.0000	0.0000
4	1.2008-001	6.0052-001	3.5410-000	-3.3911-000	-6.9507-001
5	4.2772-001	8.9104-000	3.6464-000	4.0826-000	-5.0835-000
6	2.5065-001	3.2272-001	5.5997-001	-5.8694-001	-6.5450-002
7	1.1711-001	6.8282-002	-1.4475-001	-1.4702-001	-3.2033-002

H2

	1	2	3	4	5	6	7	8	9	10
1	0.0000	9.2824-001	8.1408-001	3.1664-002	-1.5029-001	1.7552-001	-5.4036-003	-9.7053-001	2.2289-001	6.1507-001
2	0.0000	2.2019-003	4.4388-000	8.0010-004	1.7953-003	-1.1115-003	5.1031-004	9.0217-003	-5.7182-003	7.1364-002
3	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.0000+000	0.0000	0.0000
4	0.0000	1.9045-000	3.1522-001	1.0069-000	1.5111-000	-9.3284-001	4.3291-001	7.7560+000	-4.8258+000	6.0119-001
5	0.0000	-2.0072+000	-5.8510+000	-1.0665+000	-1.5682+000	9.8169-001	-4.5410-001	-8.1622+000	5.0781+000	-6.3085-001
6	0.0000	3.0541-001	4.4512-001	2.5506-000	2.4144-001	-1.4080-001	6.9397-002	1.2385+000	-7.6981-001	9.5995-002
7	0.0000	7.7911-002	5.7286-002	8.2090-001	6.1744-002	-3.7851-002	1.7960-002	3.1627-001	-1.9619-001	2.4621-002

H2

	11	12
1	1.3358-001	-2.7544-002
2	5.1183-004	7.1156-004
3	0.0000	0.0000
4	5.2340-001	6.0278-001
5	-5.5738-001	-6.3204-001
6	8.0747-002	9.4513-002
7	2.1756-002	2.0578-002

X12

	1	2	3	4	5
1	1.3737-001	1.0108-001	-2.4081-004	6.3614-004	1.8929-001
2	1.2344-001	-4.7013+001	5.5712-001	7.5317-001	6.9787+002
3	3.9507-000	5.2115+000	-2.1408-002	2.5581-002	-5.4984+001
4	-2.8764-001	-1.3119+000	2.5430-003	-2.6097-002	-1.3901+001
5	-7.5008+000	6.3666-002	-5.2121-002	-2.3677-002	1.9020+001
6	-4.5184+000	-2.8483+000	2.6274-004	-5.5372-002	2.1590+001
7	2.8607-001	2.1886-001	-6.1187-004	2.7744-004	1.9785-001
8	-1.0115+000	-3.7034-001	1.1905-002	-3.9162-002	-9.5929+000
9	2.0202+000	-6.2252+000	-3.2251-002	-4.0035-003	-4.3401+000
10	-1.2801+000	7.6554-001	9.4151-003	-3.5072-002	4.8377+000
11	1.5066+000	5.8551+000	1.0382-002	-3.0622-002	1.8452+000
12	1.4190-001	1.4547+001	2.0870-003	-1.1469-002	1.3743-001

F100 LINEAR MODEL 0.0/30K AS 3/9/76

T11 INVERSE

	1	2	3	4	5
1	9.498E-001	-1.968E+000	-4.730E-001	-5.454E-001	1.610E+001
2	1.603E-002	6.530E+000	-2.719E-001	4.248E-001	1.581E-002
3	9.831E-001	-6.560E+000	2.120E-001	-4.444E-001	-3.759E-004
4	1.059E-001	1.544E-001	9.731E-001	2.460E+001	2.724E-002
5	0.000E	0.000E	0.000E	-2.468E+001	0.000E

FO

	SHEAN	SACOM	PTTM	WFCOM	PT3
SHEAN	-7.125E-002	-2.028E+000	-1.425E+000	-8.600E-001	3.520E+000
SACOM	3.728E-001	-2.742E+000	-5.327E-001	5.477E-001	7.121E-001
PTTM	1.578E+000	-7.901E+000	-1.100E+001	4.511E+000	4.672E+000
WFCOM	0.000E	0.000E	0.000E	-1.000E+001	0.000E
PT3	-1.278E+002	2.571E+002	5.091E+001	7.663E+001	-2.138E+002

FIG 00 LINEAR MODEL 09/30V A3 3/9/76
UNNORMALIZED EIGENSYSTEM.

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-2.13072+0.021+J(0.00000	0.00000	1.00000	1 (-6.64524-0.01)+J(0.00000) 2 (-2.16183-0.01)+J(0.00000) 3 (-2.64949-0.03)+J(0.00000) 4 (0.00000)+J(0.00000) 5 (1.00000+0.00)+J(0.00000)	-8645245 -2161829 -0026499 0000000 1.0000000	0.0000 0.0000 0.0000 0.0000 0.0000
(-2.15245+0.000+J(0.00000	0.00000	1.00000	1 (1.00000+0.00)+J(0.00000) 2 (-1.06723-0.02)+J(0.00000) 3 (-3.98680-0.04)+J(0.00000) 4 (0.00000)+J(0.00000) 5 (-1.31925-0.02)+J(0.00000)	1.0000000 -0106723 -0003969 0000000 -0131925	0.0000 0.0000 0.0000 0.0000 0.0000
(-9.74225+0.000+J(0.00000	0.00000	1.00000	1 (1.00000+0.00)+J(0.00000) 2 (8.55666-0.01)+J(0.00000) 3 (3.54330-0.02)+J(0.00000) 4 (0.00000)+J(0.00000) 5 (9.85520-0.02)+J(0.00000)	1.0000000 8556659 0354330 0000000 0985520	0.0000 0.0000 0.0000 0.0000 0.0000
(-1.78911+0.000+J(0.00000	0.00000	1.00000	1 (1.00000+0.00)+J(0.00000) 2 (1.51944-0.01)+J(0.00000) 3 (-4.63568-0.04)+J(0.00000) 4 (0.00000)+J(0.00000) 5 (-9.69082-0.03)+J(0.00000)	1.0000000 1819437 -0004604 0000000 -0096908	0.0000 0.0000 0.0000 0.0000 0.0000
(-1.00000+0.000+J(0.00000	0.00000	1.00000	1 (1.00000+0.00)+J(0.00000) 2 (9.16468-0.01)+J(0.00000) 3 (3.57304-0.02)+J(0.00000) 4 (-3.55797-0.01)+J(0.00000) 5 (9.56971-0.02)+J(0.00000)	1.0000000 9184684 0357304 -3557970 0956971	0.0000 0.0000 0.0000 0.0000 0.0000

LAMPQ2 INVERSE

	1	2	3	4	5	6	7	8	9	10
1	-4.0000+000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
2	0.0000	-2.4950-003	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
3	0.0000	0.0000	-1.0824-002	-1.1115-002	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4	0.0000	0.0000	1.1115-002	-1.4828-002	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000	0.0000	-1.9995-002	0.0000	0.0000	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.0000	0.0000	0.0000	-2.5534-002	0.0000	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-1.8135+000	0.0000	0.0000	0.0000
8	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-5.1712-002	-2.3366-002	0.0000
9	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	2.3366-002	-5.1712-002	0.0000
10	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-4.4208-002
11	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	8.8137-004
12	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

LAMPQ2 INVERSE

	1	12
1	0.0000	0.0000
2	0.0000	0.0000
3	0.0000	0.0000
4	0.0000	0.0000
5	0.0000	0.0000
6	0.0000	0.0000
7	0.0000	0.0000
8	0.0000	0.0000
9	0.0000	0.0000
10	-8.9137-004	0.0000
11	-4.0206-002	0.0000
12	0.0000	-5.7571-002

Go

	WFMH	ANVTX	CTVV	ACVV	BLC
SMFAN	-7.0907-003	1.0770-001	-1.2824-003	3.6594-003	4.7762+000
SKCCH	-2.0000-001	8.5753-003	5.5319-002	-9.0849-003	-1.0910-002
PTW	-1.1133+000	-6.8240+000	7.2091-003	-4.0803-002	-5.1781+000
AFCCM	1.0000+001	0.0000	0.0000	0.0000	0.0000
PT3	4.2838+000	-1.7858+001	-2.5374-001	3.2559-001	-3.3032+002

HB	N1	N2	P T7	WF	P B
SHEAN	-0.0212-002	-1.0958-001	A.7552-003	-1.6104-002	-1.9067-003
SACOM	0.9242-001	0.1345-001	0.6235-002	-0.7459-001	1.6261+000
PTW	0.0610-001	-1.0831-001	0.1256-002	1.8417-001	1.9473-002
KECOM	0.5042-001	-1.0440-001	0.4554-001	-1.5722-001	2.4537-002
PTI	1.0002-001	0.1809-001	1.4442-001	2.9651-002	-1.6445-002
FTT	0.8340-001	-3.0312-001	3.6045-003	0.6562-001	3.0729-002
PLK	-1.6520-001	-0.6329-001	3.2270-002	0.4429-003	-9.6586-004
T2SM	0.1403-001	-2.1974-001	0.6285-003	0.3522-001	-6.0964-002
T2SC	0.3509-001	-3.0150-001	0.4500-002	3.4955-001	3.3215-003
IT3	0.7220-001	-7.1340-001	3.0515-001	0.7029-001	0.9359-002
TTUCHT	0.4456-001	-5.4796-002	0.2076-001	-0.9607-001	3.2023-002
TUPLD	1.3655-001	-1.5687-002	0.6341-001	3.3624-001	-2.3959-002

HB	FTT	PTW	T2SM	T2SC	IT3
FTT	1.7078+000	-2.7359+000	1.1405-001	-2.3991-001	1.8660+000
PTW	0.4051-001	-1.2373-003	1.2310-003	0.1946-003	2.0377-003
T2SM	0.1603-001	-2.1974-001	0.6285-003	0.3522-001	-6.0964-002
SMF	1.5007+001	-0.7237-001	1.8667+000	-3.3241+000	1.9255+000
SMC	0.4247+000	1.1332+001	1.4755+000	2.9973+000	-7.9459+000
DE25Q1	1.1170+000	-0.3492-001	-2.3462-001	-5.1841-001	3.6400-001
DE25SC	1.1179-001	-5.0047-003	-5.5097-002	-1.4226-001	7.6649-002

DB	FTT	PTW	T2SM	T2SC	IT3
FTT	1.7078+000	-2.7359+000	1.1405-001	-2.3991-001	1.8660+000
PTW	0.4051-001	-1.2373-003	1.2310-003	0.1946-003	2.0377-003
T2SM	0.1603-001	-2.1974-001	0.6285-003	0.3522-001	-6.0964-002
SMF	1.5007+001	-0.7237-001	1.8667+000	-3.3241+000	1.9255+000
SMC	0.4247+000	1.1332+001	1.4755+000	2.9973+000	-7.9459+000
DE25Q1	1.1170+000	-0.3492-001	-2.3462-001	-5.1841-001	3.6400-001
DE25SC	1.1179-001	-5.0047-003	-5.5097-002	-1.4226-001	7.6649-002

FINN	LINEAR MODEL	9/30K	AS	2/9/76
Do				
MEMPH				
ANVTX				
CTVV				
KCVV				
PLC				
FINNY	-1.7028-001	3.7825-001	4.2054-003	-3.2776-003
AFAN	2.7289-004	7.7844-003	2.0127-003	1.6147-005
TVU	-1.4802-001	1.1101-001	1.1528-003	7.4115-004
SAFE	2.0770-001	1.1157-000	3.4244-002	1.9905-002
SUHC	2.8428-001	1.1122-000	1.1405-002	-4.3145-002
DP25UT	1.3206-002	2.2318-001	3.1089-003	1.5641-003
DP25SC	1.0987-002	6.0658-002	1.0670-003	8.5937-004
				2.2500+000
				1.0647-002
				9.2220-001
				9.4598+000
				-9.5598+000
				1.4967+000
				3.6910-001

001 T 1 L WENF100ALT.SPHH100-10
 PROCESSED BY UNIVAC 1100 SERIES FLY PROCESSOR LEVEL 08 AT 4150139 PM ON TUESDAY, MARCH 9, 1976 (CREATING CYCLE 0)

1.	F	REDUCED MATRICES	9/30K	83	FIFTH ORDER
2.	-7125-01	-1595-01	-7428-03	-1592-01	-1526-03
3.	-4736-00	-2743-01	-3095-03	-1286-01	-4568-02
4.	-3402-02	-1360-01	-1101-02	-1526-01	-5376-00
5.	-0000	-0000	-0000	-1000-02	-0000
6.	-2534-01	-4004-01	-5030-03	-2811-01	-2134-03
7.	G	REDUCED MATRICES	9/30K	83	FIFTH ORDER
8.	-1493-01	-7047-03	-1266-02	-9175-01	-4790-05
9.	-4727-00	-3486-03	-7555-01	-3024-02	-1591-03
10.	-4507-02	-5325-02	-1542-00	-2239-00	-1136-03
11.	-1009-02	-0000	-0000	-0000	-0000
12.	-1544-00	-1242-04	-5645-02	-1019-02	-6567-05
13.	HY	REDUCED MATRICES	9/30K	83	FIFTH ORDER
14.	-6874-00	-1070-01	-3624-02	-2580-00	-5442-02
15.	-7841-02	-1179-04	-6821-02	-1349-03	-1240-02
16.	-1795-00	-5501-01	-1270-01	-2349-00	-8974-00
17.	-2600-03	-1137-04	-1431-01	-1021-03	-1012-02
18.	-1100-03	-1537-03	-1320-01	-9560-04	-6912-02
19.	-1114-03	-4873-04	-1069-01	-9561-04	-1631-02
20.	-3171-04	-3097-06	-2536-02	-2620-04	-3665-03
21.	DY	REDUCED MATRICES	9/30K	83	FIFTH ORDER
22.	-1821-00	-7756-03	-2036-02	-4751-01	-1305-05
23.	-5115-05	-3360-00	-3541-00	-4919-03	-1294-01
24.	-7448-01	-1154-03	-3374-01	-5422-00	-2699-04
25.	-5100-05	-6603-01	-5701-02	-8284-03	-1575-01
26.	-9047-05	-6000-01	-2318-02	-1865-02	-1653-01
27.	-2430-05	-8705-01	-3309-02	-3910-03	-1497-01
28.	-2026-05	-2306-01	-1067-02	-2146-03	-3691-00

END ELT. TIME: 2.2612 SECONDS.

0FTN

CASE 3

THE REDUCED MATRICES FR,GR,UP,DR WILL BE SAVED FOR OPTSYS ON FILE 12
 INFORMATIONAL DATA WILL BE READ FROM RECORD NO. 1 OF FILE 10

THESE WILL BE 12 EIGENVALUES ELIMINATED. THE TOLERANCE LEVEL FOR ELIMINATION IS .100
 1 OF THESE EIGENVALUES ARE COMPLEX, TO BE ELIMINATED ARE--

(-150000+000)
 (-577300+000)
 (-586800+002)
 (-500000+002)
 (-355500+002)
 (-326700+002)
 (-179100+002)
 (-184100+002)
 (-688000+000)
 (-306900+002)
 (-220000+002)
 (-190000+001)

THE IDENTIFYING TITLE FOR FR,GR,UP,DR ON OPTSYS OUTPUT REDUCED MATRICES 0/0K 87 FIFTH ORDER

LANE041

	1	2	3	4	5
1	-1.7443+002	0.0000	0.0000	0.0000	0.0000
2	0.0000	-5.7190+000	1.2930+000	0.0000	0.0000
3	0.0000	-1.5930+000	-6.7190+000	0.0000	0.0000
4	0.0000	0.0000	0.0000	-2.6289+000	0.0000
5	0.0000	0.0000	0.0000	0.0000	-1.0000+001

TII

	1	2	3	4	5
1	-2.4811-002	1.2774+000	-2.4362-002	1.0000+000	3.1625-001
2	-8.1045-003	-2.0373-001	-1.2380-001	6.7854-001	2.0876-002
3	-2.4155-002	0.5055-001	-1.7305+000	3.8667-001	4.9698-001
4	0.0000	0.0000	0.0000	0.0000	-6.5202-001
5	8.2583-001	-2.7686-001	-1.0242+000	7.4828-001	3.5569-002

XII

	1	2	3	4	5
1	4.5707-001	-2.8603+001	-1.0907-001	6.7656-001	-2.1011+002
2	-2.4521+000	-0.4747-001	1.4069-002	2.1306-002	-1.3537+000
3	-2.4422+000	3.5197+000	2.1025-002	1.5860-002	2.6908+000
4	8.7904-001	6.5102-001	2.3222-003	-1.0916-002	-1.2607+000
5	-1.5335+001	0.0000	0.0000	0.0000	0.0000

T21

1	1.0000+000	-3.3855+002	1.179+002	2.062+002	-4.533+004
2	1.0000+000	-1.4305+001	-8.7513+001	6.5379+001	-5.4493+002
3	2.5913+003	1.1720+000	7.9933+001	6.761+001	4.340+001
4	2.5145+003	1.1162+000	4.8693+001	5.9249+001	5.0683+001
5	-2.7354+002	4.7667+001	5.7125+001	9.6503+001	5.6903+001
6	1.0748+002	0.4225+001	1.2023+001	2.7411+001	1.5371+002
7	1.3348+003	0.3587+002	1.2855+002	-0.3776+002	1.1087+003
8	-2.1762+002	7.7346+001	1.0023+001	1.9762+001	-3.1373+002
9	1.1973+003	0.9340+001	1.5024+001	2.6443+001	1.0134+002
10	5.4223+004	1.2511+001	3.8755+002	-0.0055+001	4.5394+003
11	2.5240+002	1.0323+000	1.3354+001	2.0715+001	2.1633+001
12	1.1513+004	1.1543+000	1.1145+000	6.8234+001	1.0000+000
13	-4.4142+002	1.0575+000	-2.0006+001	2.4366+001	3.1944+001

T22

1	1.0000+000	7.8743+006	-3.9559+003	6.702+005	-5.6227+004	-3.2207+003	1.4860+002	5.6598+003	9.3670+005	4.1398+003
2	0.0000	1.0000+000	1.4410+001	7.7912+005	-5.8455+002	1.5999+002	8.4128+002	1.9283+001	1.7590+002	7.7864+002
3	0.0000	2.3404+004	8.1553+003	5.2666+004	-2.9011+003	1.2527+002	-1.1748+001	-1.8088+001	-4.8795+003	6.2362+002
4	0.0000	2.4372+004	2.7349+003	4.7556+003	-1.2051+002	-8.6583+005	-1.0584+001	-1.1337+001	8.0286+002	4.8333+002
5	0.0000	-2.6097+004	6.1175+003	-2.2552+003	2.6971+002	-1.6222+002	7.5071+001	-1.4637+001	6.8234+003	1.3467+001
6	0.0000	6.2223+005	3.3311+001	-5.7588+003	1.0000+000	-1.5405+001	1.2951+002	-5.2101+002	-4.5536+003	3.4613+002
7	0.0000	0.5555+004	4.1242+002	-7.0111+004	1.1682+001	1.6449+002	1.3334+001	5.0573+003	-4.5760+004	1.0000+000
8	0.0000	6.2116+004	-6.5344+002	3.2082+002	2.3964+001	-6.5046+003	-8.3368+001	-1.4582+001	3.5487+003	2.2408+002
9	0.0000	1.3342+002	1.0000+000	-1.4245+002	9.2665+002	6.1553+001	1.2314+000	-1.5147+001	7.2940+003	-6.4478+003
10	0.0000	-7.4287+003	3.7083+001	-1.3347+001	-3.3497+002	2.3349+001	4.0024+001	-2.6318+002	-2.3997+003	-7.8663+003
11	0.0000	-2.7270+002	1.8245+001	-1.9043+003	-2.5555+002	5.3533+002	-2.4071+000	2.4134+000	-9.2831+002	-3.1189+002
12	0.0000	5.9150+004	-2.8266+004	7.1440+003	1.2651+002	4.9463+005	-5.9569+001	2.1081+001	1.0000+000	5.1150+002
13	0.0000	-1.2545+002	-7.5640+001	1.0000+000	-2.2744+001	1.0000+000	-2.3393+000	3.5536+000	2.3723+001	-2.3392+002

T22

1	1.0000+000	6.3445+004	-2.5950+002	2.5950+002	1.0000+000
2	-7.5922+002	-9.7220+003	1.8153+002	1.8153+002	1.0000+000
3	5.2400+003	6.6400+005	9.6353+002	9.6353+002	1.0000+000
4	1.5445+002	-1.0048+001	7.9317+002	7.9317+002	1.0000+000
5	-1.1774+001	0.7778+002	1.1557+001	1.1557+001	1.0000+000
6	-7.5820+002	5.8432+002	7.0482+002	7.0482+002	1.0000+000
7	7.2552+003	-6.3500+003	-2.3544+002	-2.3544+002	1.0000+000
8	-2.8440+002	3.4447+002	6.4124+002	6.4124+002	1.0000+000
9	-2.5140+002	-2.6147+002	7.4355+002	7.4355+002	1.0000+000
10	-2.5140+002	-2.6147+002	1.3300+000	1.3300+000	1.0000+000
11	5.0041+001	8.0041+001	4.7440+002	4.7440+002	1.0000+000
12	-2.4340+001	1.0000+000	8.5345+002	8.5345+002	1.0000+000
13	1.0000+000	8.1743+001	-4.0295+003	-4.0295+003	1.0000+000

LAMBDA2

	1	2	3	4	5	6	7	8	9	10
1	-2.5000-001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
2	0.0000	-5.7700+002	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
3	0.0000	0.0000	-5.8800+001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4	0.0000	0.0000	0.0000	-5.0045+001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000	0.0000	-3.8857+001	0.0000	0.0000	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.0000	0.0000	0.0000	-4.7671+001	0.0000	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-1.7917+001	0.0000	0.0000	0.0000
8	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-4.3901+000	-1.7917+001	0.0000	0.0000
9	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-1.8418+001	0.0000
10	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-5.8825-001
11	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
12	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
13	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

LAMBDA2

	11	12	13
1	0.0000	0.0000	0.0000
2	0.0000	0.0000	0.0000
3	0.0000	0.0000	0.0000
4	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.0000
8	0.0000	0.0000	0.0000
9	0.0000	0.0000	0.0000
10	0.0000	0.0000	0.0000
11	-2.0000+001	0.0000	0.0000
12	0.0000	-2.2001+001	0.0000
13	0.0000	0.0000	-1.9075+000

T12

	1	2	3	4	5	6	7	8	9	10
1	0.0000	-4.8800-002	-2.5925-002	8.0503-004	4.7635-003	-2.7262-002	8.4327-002	-4.8242-002	-1.8133-003	1.2405-001
2	0.0000	3.1188-002	-1.5714-002	2.4031-005	-4.4373-002	8.2965-003	1.5953-001	3.1802-002	-2.7468-004	1.3804-001
3	0.0000	-6.1583-003	6.0730-003	9.7613-005	1.9255-002	1.8600-002	5.9000-002	-2.0758-001	1.2508-002	-4.4868-002
4	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	2.7648-003	-6.4444-002	1.4132-002	1.1055-002	1.2685-002	3.6424-002	2.6632-001	2.7792-002	1.2563-001

T12

	11	12	13
1	1.0452-002	6.2847-003	1.6976-001
2	1.0070-002	6.6607-003	6.5797-002
3	-7.1111-002	-2.5432-002	-2.6682-002
4	0.0000	0.0000	0.0000
5	-7.6511-002	2.3466-003	2.9236-002

H1

	1	2	3	4	5
1	3.7261-001	-5.9229-001	6.5338-002	-3.5518-002	1.3652-001
2	4.1747-001	1.7228-004	-1.0706-003	5.9175-003	0.0000
3	0.0000	0.0000	0.0000	0.0000	0.0000
4	3.0581+000	3.6997-001	3.3209+000	1.1445-001	7.4384-004
5	9.1320-001	8.2553+000	3.5799+000	3.8052-001	-5.1378+000
6	1.6631-001	-3.7048-001	-6.4609-001	-0.8833-002	4.7498-002
7	9.5332-002	5.7653-002	-1.7076-001	-1.1453-002	-3.4621-003

H2

	1	2	3	4	5	6	7	8	9	10
1	0.0000	6.3580-001	5.3329-001	4.0233-002	-4.6489-002	8.8500-002	1.4036-002	-3.7962-001	4.4344-003	5.0607-003
2	0.0000	0.0000	-1.8555-004	1.7233-004	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
3	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.0000+000	0.0000	0.0000
4	0.0000	6.8874-002	-2.7053-001	3.4662-001	2.6610-002	3.7364-002	3.4020-002	9.2951-003	3.2228-002	3.2226-002
5	0.0000	-7.7789-002	3.4350+000	-3.7470-001	-3.5252-002	-3.9417-002	-3.615-002	-9.4970-003	-3.5319-002	-3.5008-002
6	0.0000	1.1112-002	3.4183-001	1.7019-001	6.4978-003	7.8205-003	7.5249-003	2.0507-003	6.8561-003	6.8568-003
7	0.0000	3.4480-003	3.5063-002	4.1064-002	1.6366-003	2.1701-003	2.1462-003	5.1266-004	1.6480-003	1.6481-003

H2

	11	12	13
1	4.1534-001	1.1017-001	5.1559-003
2	0.0000	0.0000	0.0000
3	0.0000	0.0000	0.0000
4	3.0574-002	-2.6685-002	3.2475-002
5	-3.3772-002	3.3771-002	-3.5132-002
6	4.1479-003	-5.5543-003	6.7004-003
7	1.4500-003	-1.2279-003	1.8866-003

X12

	1	2	3	4	5
1	1.155-001	7.409-002	3.859-004	2.6976-004	1.9173-001
2	-4.0702-001	-7.6413+000	1.3192-001	-5.1217-001	2.0322+002
3	2.359+001	1.489+001	-4.766-002	4.0885-001	-1.1775+002
4	6.475+001	4.836+001	-3.542-002	1.1404+000	-2.629+002
5	-2.2328+001	-1.337+001	2.7592-002	-3.2036-001	6.1024+001
6	-4.4073+001	-2.8456+001	7.8159-002	-6.4970-001	1.6404+002
7	-4.1649+000	-2.536+000	2.0952-002	-2.7612-002	-3.999+000
8	-4.0222+000	-4.539+000	8.3421-002	3.6403-002	-6.485+000
9	1.1906+001	1.4387+001	-1.037+001	-7.0998-002	1.9101+001
10	2.7561-001	1.8135-001	9.1207-004	3.6650-004	2.790-001
11	-3.3381-001	4.037+000	-2.0789-001	-2.7200-001	3.3794+001
12	-5.8124+000	-7.1222+000	2.3283-002	-5.3876-002	-1.767+000
13	6.2426-001	7.1107-001	3.8125-003	-1.1164-003	3.1617-001

T11 INVERSE

	1	2	3	4	5
1	4.2320-001	-1.4772+002	-5.9003-001	-2.3490-001	1.187+000
2	5.932-001	9.2445-001	-5.1468-002	3.0085-001	1.0559-002
3	3.7553-001	-2.2922-001	-5.6168-001	-2.5182-001	-6.6633-003
4	2.5311-001	1.1302+000	-9.4071-002	8.8814-002	1.5732-002
5	0.0100	0.0000	0.0000	-1.5335+000	0.0000

FR

	SKEAN	SKEAN	SKEAN	PTM	WCOM	PT3
1	-3.251+000	-2.7556+000	-3.7690+000	5.8819-001	5.0294+000	1.653+000
2	1.2558+000	-5.0412+000	-9.0781-001	1.8249-001	5.2380+000	0.0000
3	0.0306+000	-7.0229+000	-1.0034+001	-1.0000+001	-1.7147+002	0.0000
4	0.0100	0.0000	0.0000	3.2902+001	0.0000	0.0000
5	-5.8355+001	2.3507+002	8.1783+001	3.2902+001	0.0000	0.0000

R100 LINEAR MODEL ODK R3 2/17/76

LAMBDA2 INVERSE

	11	12	13
1	0.0000	0.0000	0.0000
2	0.0000	0.0000	0.0000
3	0.0000	0.0000	0.0000
4	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.0000
8	0.0000	0.0000	0.0000
9	0.0000	0.0000	0.0000
10	0.0000	0.0000	0.0000
11	-0.5332-002	0.0000	0.0000
12	0.0000	-0.5452-002	0.0000
13	0.0000	0.0000	-5.2426-001

GP

	CVSH	AVIX	CIVV	RCVV	BLC
SNEAN	1.0097-002	-9.0002-002	1.4735-002	-6.0250-003	2.1502+000
SNCOM	2.0070-001	1.5152-001	-3.3260-003	-1.9759-002	6.1043-001
PTV	-4.1507-001	-4.9100+000	-2.5900-002	-3.0350-002	-1.7520+000
MECOM	1.0000+001	0.0000	0.0000	0.0000	0.0000
PTZ	-3.0097+000	2.0007+000	1.1529-001	6.5202-001	-1.6012+002

H*

	RMV	MEAN	TTU	SMVF	SMVC
SNEAN	-2.0005-002	9.0055-002	6.0013-003	-9.0066-003	-5.7539-004
SNCOM	1.5037-001	-5.4005-001	-1.4905-001	7.6015-002	1.0046+000
PTV	7.0015-001	2.0040-001	2.1601-001	-1.5300-001	2.5600-002
MECOM	5.0020-001	2.0000-001	3.0001-001	-2.1679-001	3.0050-002
PTZ	5.0001-001	5.1006-001	2.0001-001	-3.0000-001	1.0000-003
PTT	4.0010-001	-5.7018-001	-5.7000-002	2.0000-002	2.0000-002
PTD	0.0000-003	0.0000-003	1.0000-003	0.0000-003	1.0000-003
PTM	5.0000-001	0.0000-001	-4.0000-001	2.0000-001	-2.0000-001
TTZ	-1.0000-002	-6.0000-001	-6.0000-001	1.0000-001	1.0000-001
TTM	0.0000-001	1.0000-001	1.0000-001	1.0000-001	1.0000-001
TTD	4.0000-001	-3.0000-001	6.0000-001	-7.0000-001	3.0000-002
TTM	3.0000-001	-3.0000-001	5.0000-001	0.0000-002	-5.0000-002

FIG LINEID MODEL 0/0X A3 2/17/75

HE	FTIT	PTUS	TT25H	TT25C	TT3
FNW	1.1412+000	-1.5504+000	2.2015+001	-1.3321-001	9.6590-001
APIN	A.173-001	1.7917-004	-1.0086-003	5.967-003	-3.0619-007
TT4	5.7935-001	-4.6682-001	-6.8218-002	2.500-001	-2.3186-002
SWAF	4.0376+000	2.2316-001	-3.2495+000	1.2531-001	8.5979-002
SMC	-2.6019+000	9.4400+000	2.5131+000	1.0720+000	-5.2641+000
DP2GT	5.3232-001	-5.1332-001	-5.2093-001	-1.2622-001	7.9715-002
DP2SC	1.6143-001	2.6946-002	-1.3049-001	-2.7932-002	3.6010-003

D*	FNW	MEAN	TT4	SM4F	SMHC
SN4N	1.5301-001	2.6943-001	1.5445-003	1.0960-003	5.5780-001
SN4M	-1.8945-002	-2.1788-002	-9.2754-005	-1.2883-003	3.9840-001
PT4	A.7379-002	8.4252-002	-1.5304-003	-7.6318-004	1.7714-001
ME4M	1.3243-001	1.3372-001	-1.1929-003	-3.2322-004	2.0191-001
PT3	2.6442-001	1.5251-001	-1.1802-003	2.0111-003	1.4793-001
PT4	7.1724-002	7.4101-002	-1.7954-003	-1.2095-003	6.4852-001
PT5	4.1928-001	2.7816-001	1.2450-003	4.4657-004	4.8932-001
TT25H	1.0325-001	7.4194-002	-1.4703-003	-1.0062-003	6.8114-001
TT25C	A.2411-002	7.5015-002	-1.9040-003	-1.3100-003	6.9345-001
TT3	5.4825-001	4.1956-001	1.7961-003	-1.0611-003	4.0639-001
TT4H1	7.1446-002	1.3891-001	-2.5309-003	-3.1447-003	1.0275+000
TT4H2	5.2087-001	3.4098-001	-9.7771-004	-4.1675-004	5.1258-001
TT4	1.1015-001	2.5138-001	6.5509-004	-6.5599-004	6.6391-001

D*	FNW	MEAN	TT4	SM4F	SMHC
SN4N	1.5301-001	2.6943-001	1.5445-003	1.0960-003	5.5780-001
SN4M	-1.8945-002	-2.1788-002	-9.2754-005	-1.2883-003	3.9840-001
PT4	A.7379-002	8.4252-002	-1.5304-003	-7.6318-004	1.7714-001
ME4M	1.3243-001	1.3372-001	-1.1929-003	-3.2322-004	2.0191-001
PT3	2.6442-001	1.5251-001	-1.1802-003	2.0111-003	1.4793-001
PT4	7.1724-002	7.4101-002	-1.7954-003	-1.2095-003	6.4852-001
PT5	4.1928-001	2.7816-001	1.2450-003	4.4657-004	4.8932-001
TT25H	1.0325-001	7.4194-002	-1.4703-003	-1.0062-003	6.8114-001
TT25C	A.2411-002	7.5015-002	-1.9040-003	-1.3100-003	6.9345-001
TT3	5.4825-001	4.1956-001	1.7961-003	-1.0611-003	4.0639-001
TT4H1	7.1446-002	1.3891-001	-2.5309-003	-3.1447-003	1.0275+000
TT4H2	5.2087-001	3.4098-001	-9.7771-004	-4.1675-004	5.1258-001
TT4	1.1015-001	2.5138-001	6.5509-004	-6.5599-004	6.6391-001

[illegible]

CASE 4

RESTORED MATRICES

EIGENVALUES
 -.2500+00 .0000
 -.5718+03 .0000
 -.1789+03 .0000
 -.5773+02 .0000
 -.5009+02 .0000
 -.4978+02 .0000
 -.3890+02 .0000
 -.2014+01 .0000
 -.5141+01 .0000
 -.7325+01 .3912+01
 -.7325+01 -.3912+01
 -.1805+02 .3871+01
 -.1805+02 -.3871+01
 -.1668+02 .0000
 -.2121+02 .0000
 -.1955+02 .0000
 -.1000+02 .0000

F100 LINEAR MODEL 1.2/OK R3 3/3/76

LAMBDA1

	1	2	3	4	5
1	-1.7895+002	0.0000	0.0000	0.0000	0.0000
2	0.0000	-5.114+000	0.0000	0.0000	0.0000
3	0.0000	0.0000	-7.3250+000	3.9124+000	0.0000
4	0.0000	0.0000	-3.9124+000	-7.3250+000	0.0000
5	0.0000	0.0000	0.0000	0.0000	-1.0000+001

Y11

	1	2	3	4	5
1	-3.5781-002	1.0000+000	-1.1760-001	-1.5193-001	4.1627-001
2	-2.8808-003	3.2119-001	2.0566-002	5.2937-003	1.8919-002
3	-2.6110-002	9.2372-001	-1.6224-001	4.1399-002	3.2400-001
4	0.0000	0.0000	0.0000	0.0000	-4.4372-001
5	7.8803-001	9.8765-001	-2.1447-002	-7.5020-002	1.3326-001

X11

	1	2	3	4	5
1	-9.1337-001	4.2754+000	-1.0971+001	-5.8325-001	-2.1886+002
2	5.6568+000	-1.5513-001	5.6259-002	1.4474-002	-3.9497+000
3	-1.1703+001	3.4263+001	1.7868+000	7.6872-002	1.6669+001
4	-2.7987+000	-2.1172+001	-3.1681+000	2.1857-001	-7.4613+000
5	-2.2537+001	0.0000	0.0000	0.0000	0.0000

T21

	1	2	3	4	5
1	8.967-006	3.693-003	1.598-003	-3.350-004	1.650-003
2	1.000+000	9.152-001	-3.047-002	-7.946-002	9.582-002
3	5.418-004	6.213-001	-1.274-001	-6.757-002	4.210-001
4	-1.683-003	6.159-001	-1.520-001	-5.473-002	5.038-001
5	-2.562-002	6.098-001	-8.340-002	-2.258-002	4.357-001
6	7.673-003	-1.659-002	-3.418-002	3.685-002	-8.245-002
7	-4.896-002	2.214-001	-1.026-001	1.142-001	2.737-001
8	-1.969-002	-1.290-001	-2.413-002	3.261-002	-1.051-001
9	-2.562-003	-7.946-002	-4.844-002	3.637-002	-7.047-002
10	-2.687-003	-2.047-003	-7.235-003	1.344-002	-1.782-002
11	2.096-002	-1.526-001	-4.415-002	1.100-001	-5.589-002
12	3.751-004	8.299-001	-2.401-001	-1.066-002	1.000+000

T22

	1	2	3	4	5	6	7	8	9	10
1	1.000+000	8.113-006	-4.089-003	2.077-004	-4.286-004	-6.075-003	-1.273-002	-1.619-003	-3.729-003	-2.110-003
2	0.000	1.000+000	5.451-003	1.340-002	-2.237-003	4.217-002	3.766-002	-4.242-002	-3.251-002	-6.669-002
3	0.000	1.718-004	1.523-002	-1.703-004	3.872-004	3.553-002	5.772-002	-2.186-002	7.203-002	6.209-002
4	0.000	1.493-004	1.732-002	2.451-004	-3.347-004	2.674-002	5.691-002	5.143-002	9.563-002	1.448-001
5	0.000	-2.207-004	-1.986-002	1.780-003	3.372-003	-4.481-002	2.344-002	6.973-002	1.483-001	8.132-002
6	0.000	2.854-005	9.448-001	1.803-001	1.787-002	9.585-001	-1.326-002	1.701-001	2.343-001	1.341-001
7	0.000	-1.542-002	-8.498-001	1.000-000	1.000+000	-3.789-001	-3.358-002	1.226-000	-1.776-001	1.000+000
8	0.000	-4.550-004	-1.570-001	-1.316-004	-1.132-004	2.344-001	-1.547-002	9.283-002	1.645-001	9.037-002
9	0.000	-1.886-002	1.000+000	-4.405-002	9.037-002	1.000+000	-1.149-002	1.844-001	2.573-001	1.484-001
10	0.000	-8.321-003	3.785-001	-1.652-002	3.380-002	3.676-001	1.000+000	6.518-002	8.173-002	4.732-002
11	0.000	-2.444-003	2.134-001	-2.391-003	5.209-003	-7.363-002	-5.473-002	9.249-001	2.313-002	6.038-001
12	0.000	-5.807-006	-8.664-003	-1.417-004	1.814-004	-2.753-002	6.240-002	5.008-001	-1.403-002	8.657-001

T22

	11	12
1	-5.796-004	-3.903-004
2	-1.347-004	-5.697-002
3	1.861-003	1.870-002
4	-6.151-002	-1.031-003
5	2.920-002	-4.602-005
6	4.742-002	2.925-002
7	-5.237-002	1.000+000
8	2.720-002	1.932-002
9	5.191-002	3.224-002
10	1.757-002	1.065-002
11	-4.839-001	9.160-001
12	1.000+000	-5.874-002

LAMBDA2

	1	2	3	4	5	6	7	8	9	10
1	-2.5000+001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
2	0.0000	-5.7177+002	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
3	0.0000	0.0000	-5.7735+001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4	0.0000	0.0000	0.0000	-5.0093+001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000	0.0000	-4.9778+001	0.0000	0.0000	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.0000	0.0000	0.0000	-3.8898+001	0.0000	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-2.0141+000	0.0000	0.0000	0.0000
8	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-1.8048+001	3.8711+000	0.0000
9	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-3.8711+000	-1.8048+001	0.0000
10	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-1.6564+001
11	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
12	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

LAMBDA2

	11	12
1	0.0000	0.0000
2	0.0000	0.0000
3	0.0000	0.0000
4	0.0000	0.0000
5	0.0000	0.0000
6	0.0000	0.0000
7	0.0000	0.0000
8	0.0000	0.0000
9	0.0000	0.0000
10	0.0000	0.0000
11	0.0000	0.0000
12	0.0000	0.0000

	1	2	3	4	5	6	7	8	9	10
1	-1.0221+002	-6.2191+002	1.0189+003	-2.5309+003	-8.8582+002	1.1431+001	-3.6026+002	-1.9436+002	3.9721+003	-2.5738+002
2	0.0000	1.2446+002	3.8802+004	-4.3399+004	-1.1608+002	-6.6077+003	-1.3738+002	-3.7189+002	-2.5738+002	-9.6815+002
3	-0.8118+003	-1.3399+001	-0.1675+003	1.8383+002	-8.0404+002	-3.8601+002	-1.2961+001	-5.9207+003	0.0000	0.0000
4	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5	1.0000+003	5.8194+003	9.6991+003	-1.9157+002	-9.9267+003	3.5618+002	-4.5222+002	-4.9674+002	-7.2211+002	0.0000

AD-A052 346 SYSTEMS CONTROL INC PALO ALTO CALIF AERONAUTICAL AND--ETC F/G 21/5
F100 MULTIVARIABLE CONTROL SYNTHESIS PROGRAM. VOLUME II. APPEND--ETC(U)
JUN 77 R L DE HOFF, W E HALL, R J ADAMS F33615-75-C-2053
UNCLASSIFIED AFAPL-TR-77-35-VOL-2 NL

SYSTEMS CONTROL INC PALO ALTO CALIF AERONAUTICAL AND--ETC F/G 21/5
F100 MULTIVARIABLE CONTROL SYNTHESIS PROGRAM. VOLUME II. APPEND--ETC(U)
JUN 77 R L DE HOFF, W E HALL, R J ADAMS F33615-75-C-2053
AFAPL-TR-77-35-VOL-2 NL

AFAPL-TR-77-35-VOL-2

NL

3 of 6
AD
A052346

AD
A052346

100

M1																				
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
1	-	.7563-001	-1.0749+000	5.9537-001	-1.8345-001	3.0440-001														
2		.5875-001	2.0199-002	-4.3206-003	1.6462-002	-2.2183-003														
3		0.0000	0.0000	0.0000	0.0000	0.0000														
4		1.4635+000	1.7743+000	3.8884-001	3.3162-002	-1.9887-001														
5		6.3234+000	2.6007+001	9.8371-001	-3.7676-001	-6.8427+000														

M2																				
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
1	0.0000	1.3135+000	8.5655-001	-7.7121-002	-2.3402-002	-3.1412-001	3.8134-002	-2.0584-001	3.7831-002	3.6896-002										
2	0.0000	0.0000	-1.4479-002	-3.1536-003	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000										
3	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000										
4	0.0000	-2.8469-003	-1.2931+000	-2.8599-001	-6.5846-003	2.9006-002	-3.8253-003	-3.8625-002	-3.8252-003	-3.8254-003										
5	0.0000	7.5953-003	-9.7668+000	7.2409-001	1.7874-002	-7.8579-002	9.8255-003	1.0361-001	1.0716-002	9.8227-003										

M2

11	12
1	8.6605-001
2	0.0000
3	-2.3355-004
4	0.0000
5	-6.7546-003
6	-2.3246-002
7	1.8114-002
8	5.9118-002

188

X12

1	2	3	4	5
1	8.6605-001	3.0593-003	3.7434-004	1.1944-001
2	0.0000	7.8249+000	4.3811-001	2.5182+002
3	1.0958+001	2.3143+000	-1.3756-001	-4.7597-001
4	3.5722+000	7.0566-001	-5.3141-002	-1.9508+001
5	7.1853+000	2.0791+000	-1.2804-001	-3.2272+001
6	-1.8512+001	-3.1240+000	1.5484-001	5.2365+001
7	4.9548+001	1.6222-003	1.5799-003	6.4955-001
8	-3.2483+001	-2.5011+001	-1.9404-001	-3.0208+001
9	2.2845+001	1.3162+001	-1.1358-003	-5.7298+000
10	3.8380+001	2.8415+001	2.2258-001	3.6257+001
11	-2.0571+000	-3.3178+000	1.8315+000	-6.6095+000
12	9.3924-001	9.5951+000	1.6431+000	2.4640+001

F100 LINEAR MODEL 1.2/OK 83 3/3/76

TII INVERS

	1	2	3	4	5
1	-6.4044+001	-1.7111+000	5.6437-003	-3.2205-001	1.2199+000
2	1.1850-001	1.9005+000	2.5577-001	3.8955-001	3.5272-002
3	-5.5104-001	1.2017+001	-3.5733+000	-2.6162+000	-7.9931-003
4	-5.2200+000	3.6102+000	4.8451+000	-1.5099+000	-4.8953-002
5	0.0000	0.0000	0.0000	-2.2537+000	0.0000

FD

	SVLEN	SVCCM	PT7M	WFCCM	PT3
SVLEN	-9.0478+000	-8.7656-001	-3.5775+000	5.2210-001	7.5861+000
SVCCM	-1.5159+000	-8.0314+000	7.7652-001	-2.2407-001	1.8786+000
PT7M	6.8220-001	-8.0726+000	-9.0286+000	2.6780+000	5.5701+000
WFCCM	0.0000	0.0000	0.0000	-1.0000+001	0.0000
PT3	8.9854+001	2.3875+002	-1.6337+000	4.4559+001	-1.7223+002

F100 LINEAR MODEL 1.2/0K 83 3/3/76

UNNORMALIZED FIGENSYSTEM.

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-1.78950+002)+J(0.00000)	0.000000	1.000000	1 (-7.91008-001)+J(0.00000) 2 (-2.47503-001)+J(0.00000) 3 (-3.50281-003)+J(0.00000) 4 (0.00000)+J(0.00000) 5 (1.00000+000)+J(0.00000)	-7910078 -2475032 -0035028 0.000000 1.000000	0.0000 0.0000 0.0000 0.0000 0.0000
(-7.325 1+000)+J(3.91242+000)	8.30439+000	.68207	1 (1.00000+000)+J(0.00000) 2 (-1.46220-001)+J(1.32151-001) 3 (2.10281-003)+J(-4.85283-003) 4 (0.00000)+J(0.00000) 5 (2.16465+002)+J(8.65264+003)	1.000000 .1970891 .0052888 0.000000 .0233110	0.0000 137.89328 -66.57214 0.0000 21.78780
(-5.14 43+000)+J(0.00000)	0.000000	1.000000	1 (1.00000+000)+J(0.00000) 2 (4.04920-001)+J(0.00000) 3 (5.60560-003)+J(0.00000) 4 (0.00000)+J(0.00000) 5 (5.66937-002)+J(0.00000)	1.000000 .4049200 .0056056 0.000000 .0566937	0.0000 0.0000 0.0000 0.0000 0.0000
(-1.00 00+001)+J(0.00000)	0.000000	1.000000	1 (-6.49369-001)+J(0.00000) 2 (-3.72070-002)+J(0.00000) 3 (-3.08719-003)+J(0.00000) 4 (1.00000+000)+J(0.00000) 5 (-1.19333-002)+J(0.00000)	-6493690 -0372070 -0030672 1.000000 -0119333	0.0000 0.0000 0.0000 0.0000 0.0000

LAMBDA2 INVERSE

[illegible]

LAMBDA2 INVERSE

	11	12
1	0.0000	0.0000
2	0.0000	0.0000
3	0.0000	0.0000
4	0.0000	0.0000
5	0.0000	0.0000
6	0.0000	0.0000
7	0.0000	0.0000
8	0.0000	0.0000
9	0.0000	0.0000
10	0.0000	0.0000
11	-4.7138-002	0.0000
12	0.0000	-5.1145-002

GR	WFMH	ANMIX	CIVV	RCVV	BLC
SNFAN	-4.5863-002	-2.0634-002	5.4584-001	-8.3852-004	3.8575+000
SNCOM	7.5670-001	6.5218-001	1.4455-001	1.2479-002	1.0508+000
PT7M	-5.5146-001	-7.1030+000	-1.6960-001	2.1771-002	-2.2471+000
WFCOM	1.0000+001	0.0000	0.0000	0.0000	0.0000
PT3	-1.3047+001	-8.6748+000	-7.3204+000	-5.3116-001	-1.9004+002

H*	FNMV	WEAN	TT4	SMAF	SMHC
SNFAN	1.2473-003	2.5041-002	-6.2133-003	-6.0532-003	1.4435-004
SNCOM	-1.2032-001	-6.2353-001	-4.6693-003	1.9038-002	1.2563+000
PT7M	4.9619-001	-5.9555-001	3.1370-001	-2.7155-001	2.6922-002
WFCOM	4.4362-001	-8.5128-001	4.5735-001	-4.1288-001	2.3566-002
PT3	2.6193-001	2.9064-001	3.7783-001	-4.5357-001	-4.7509-003
FTIT	-1.8679-001	-4.3694-001	2.4580-001	1.8758-001	5.1381-003
PT4	-4.6810-001	-2.8109-001	9.3120-001	-4.1299-001	-8.1110-002
TT25H	-1.5711-001	-4.3286-001	2.1235-001	2.1723-001	-2.9974-002
TT25C	-1.7074-001	-5.3391-001	2.9746-001	1.9016-001	-1.2551-002
TT3	-6.7288-002	-3.5985-002	8.7336-002	3.8099-002	-3.9688-003
TT4PH1	-5.6859-001	-7.4061-001	6.9410-001	7.0343-002	1.5373-002
TT7M	2.8645-001	-1.3557+000	1.0253+000	-1.2844+000	3.2177-002

HR	FTIT	PT5	TT25H	TT25C	TT3
FNMV	-4.6361-001	-3.3353+000	1.7443+000	-9.0779-001	2.0028+000
WFCOM	4.5010-001	3.1824-002	-1.0544-002	2.1996-002	-2.6899-003
TT4	-1.5711-001	-4.3286-001	2.1235-001	2.1723-001	-2.9974-002
SMAF	4.9420-001	2.4317+000	-9.6180-001	5.3245-001	-2.4314-001
SMHC	1.8002+000	3.1096+001	-1.6547+000	1.8999+000	-7.1314+000

F100 LINEAR MODEL 1.2/OK A3 3/3/76

D*	FMX	MEAN	TY4	SHAF	SMHC
SNEAN	3.4713-001	-8.3120-003	1.1928-002	1.4610-003	4.6723-001
SNCOM	8.0608-003	1.5483-002	1.5371-002	1.0498-003	5.1744-001
PT7M	2.0972-001	1.7785-001	-4.1645-003	1.2191-003	2.5168-001
WFCOM	3.2720-001	2.5382-001	-1.4803-002	1.7645-003	3.0138-001
PT3	3.6112-001	2.3720-001	2.4209-003	6.6017-004	9.3503-002
FTIT	1.5256-001	2.2234-001	2.8969-002	1.7856-003	4.9086-001
PT45	5.5358-001	6.4522-001	6.1385-002	3.5287-004	6.8479-001
TT25H	1.4463-001	1.7354-001	2.5500-002	1.8207-003	5.1497-001
TT25C	1.7424-001	2.4450-001	1.0451-002	1.9033-003	5.3975-001
TT3	2.0439-001	7.7944-002	1.8368-002	1.4126-003	5.0682-001
TT4PHI	2.4313-001	4.8185-001	5.9783-002	2.1520-003	8.7763-001
TT7M	1.0693+000	6.7461-001	7.5326-003	2.3133-003	7.3640-001

DP	WFCRM	ANMTX	CIVV	RCVV	BLC
FMX	7.4790-001	6.7865-001	6.7122-002	7.1723-003	1.9478+000
MEAN	-4.4180-003	9.5704-003	-8.4685-002	-7.9919-005	2.1605-002
TY4	1.4463-001	1.7354-001	2.5500-002	1.8207-003	5.1497-001
SHAF	-3.9951-001	-3.1185-001	3.8840-001	-7.4984-003	-4.0818-001
SMHC	-1.7220+000	-1.3046+000	-3.8477-001	-1.0885-002	-8.0923-001

PROCESSED BY UNIVAC 1100 SERIES ELT PROCESSOR LEVEL WB AT 11:32:49 AM ON WEDNESDAY, MARCH 3, 1976 (CREATING CYCLE 0)

		REDUCED MATRICES		1.2/OK 83	FIFTH ORDER
1.	F				
2.		-.9048+01	-.6953+00	-.5895+03	.3614+00
3.		-.1911+01	-.6431+01	.1613+03	-.1955+00
4.		-.4140+02	-.3886+01	-.9029+01	.1125+01
5.		.0000	.0000	.0000	.0000
6.		.5158+01	-.1047+02	-.1545+02	.1770+01
7.	G				
8.		-.1175+01	-.4505+02	-.3220+03	.5037+01
9.		.6003+00	-.2567+04	-.1002+03	-.9450+02
10.		-.2316+02	-.1345+03	.5657+00	-.7936+00
11.		.1000+02	.0000	.0000	.0000
12.		-.5184+00	-.1555+04	.2309+03	.1831+03
13.	HY				
14.		-.8363+00	-.3334+01	.3622+03	-.7918+00
15.		.3377+01	.1003+02	-.6902+01	.6047+03
16.		-.4510+01	-.9456+01	.1004+02	.4316+01
17.		.2487+04	.6247+04	.4408+02	.1025+04
18.		.2510+04	.3439+03	-.3801+02	.1833+04
19.	DY				
20.		.6524+00	.2670+04	-.4649+02	-.5429+02
21.		-.1147+03	-.1187+01	.1849+01	-.1907+01
22.		.3271+01	.1555+03	-.4023+01	-.3139+01
23.		-.7690+05	-.2708+01	-.5936+02	.1253+02
24.		-.1662+04	-.5679+01	.2948+02	.9115+03

THE REDUCED MATRICES PROGRAMS WILL BE SAVED FOR OPTSYS ON FILE 12
INTERMEDIATE DATA WILL BE READ FROM RECORD NO. 10 OF FILE 10

CASE 5

THERE WILL BE 10 EIGENVALUES ELIMINATED. THE TOLERANCE LEVEL FOR ELIMINATION IS .100
3 OF THESE EIGENVALUES ARE COMPLEX. TO BE ELIMINATED ARE--

(-.250000+.000000)
(-.480300+.000000)
(-.509000+.000000)
(-.574000+.000000)
(-.442000+.000000)
(-.093000+.000000)
(-.170000+.000000)
(-.194000+.000000)
(-.205000+.000000)
(-.190000+.000000)

THE IDENTIFYING TITLE FOR PR,GR,HR,DR ON OPTSYS OUTPUT REDUCED MATRICES .9730K 20 FIFTH ORDER

F100 LINEAR MODEL .9/304 20 3/9/76

LAMBDAI

	1	2	3	4	5
1	-1.1929+002	0.0000	0.0000	0.0000	0.0000
2	0.0000	-1.1609+000	3.0200+001	0.0000	0.0000
3	0.0000	-3.0200+001	-1.1599+000	0.0000	0.0000
4	0.0000	0.0000	0.0000	-4.5333+000	0.0000
5	0.0000	0.0000	0.0000	0.0000	-1.0000+001

XTI

	1	2	3	4	5
1	-9.2074+003	3.2000+001	-2.5190+001	7.6977+002	-5.4524+002
2	-1.3046+003	0.1600+002	2.3454+002	1.5555+002	-2.5226+002
3	-2.3755+002	2.5257+001	-2.2505+001	1.0000+000	-5.0762+001
4	0.0000	0.0000	0.0000	0.0000	1.0000+000
5	9.1558+001	2.3013+001	2.7629+003	1.9710+001	2.8700+002

XTI

	1	2	3	4	5
1	7.1557+001	1.3300+000	-2.0755+000	-1.1847+001	-1.5517+002
2	1.4612+000	2.1172+000	4.8290+002	3.3867+002	-4.5746+000
3	2.1111+000	5.8536+001	8.5720+002	3.2629+001	-5.2994+000
4	5.0527+000	-6.4595+000	-1.4969+001	1.4443+001	-4.5592+000
5	1.0000+001	0.0000	0.0000	0.0000	0.0000

T21

	1	2	3	4	5
1	-1.0149-005	2.4555-003	4.7787-003	-1.0365-003	-6.7289-003
2	1.0000+000	2.6550-001	8.1975-002	4.5560-001	8.8115-002
3	8.4321-004	7.6209-002	7.1209-002	8.3916-002	-6.3033-002
4	1.0217-003	8.2579-002	9.4066-002	1.8252-001	1.2910-001
5	-4.4818-002	8.0303-002	3.1637-003	8.5927-002	-5.5705-002
6	5.5623-003	3.7143-002	3.1922-003	-1.7955-002	5.9284-001
7	7.1917-004	1.9908-002	2.1509-002	-6.1566-004	4.2360-002
8	-3.4656-003	-4.6739-002	3.7783-003	-2.3877-002	5.1847-001
9	9.0717-003	3.0342-002	2.8847-002	5.5114-002	5.4868-001
10	3.8884-003	-6.4691-002	2.4409-002	7.7169-003	1.3652-001
11	4.1310-002	-4.7406-002	5.1556-002	2.1291-001	7.5305-001
12	-1.0993-004	8.4980-002	1.0004-001	2.7149-001	-2.5720-001
13	-1.2886-001	2.4002-002	-6.0423-003	3.2642-001	3.8751-001

T22

	1	2	3	4	5	6	7	8	9	10
1	1.0000+000	6.8138-006	8.1262-004	-2.1206-003	2.9327-003	2.1161-002	4.8366-003	8.0324-003	-1.0717-004	
2	0.0000	1.0000+000	2.9502-002	-4.8513-002	2.2032-001	-1.3223-001	3.8449-001	-9.2085-001	-4.6189-001	8.6123-002
3	0.0000	1.0005-003	2.8780-004	1.5566-003	7.4071-003	-4.5069-003	8.7126-002	1.5799-001	-2.1275-001	-1.0287-002
4	0.0000	1.7311-004	3.4402-004	1.5468-003	8.0325-003	-4.0331-003	8.6624-002	1.5284-001	-5.4009-001	3.0483-002
5	0.0000	-1.0982-004	-7.0995-004	5.4786-003	-6.4710-003	8.3190-003	1.0356-001	-5.3343-001	-4.9702-001	1.8614-002
6	0.0000	3.7786-005	-1.4364-003	3.0382-001	-1.3043+000	-2.6175-001	-4.6843-002	-7.1238-001	-8.4202-001	-1.5415-003
7	0.0000	4.8971-006	-2.2432-004	3.7414-002	-1.5699-001	-3.0861-002	1.0000+000	-7.5240-002	-7.9429-002	-1.6475-004
8	0.0000	-2.7457-004	1.4689-004	-0.9325-002	-1.3625-001	-7.5511-002	-5.8706-002	-4.1705-001	-6.0181-001	-2.4870-003
9	0.0000	-2.7004-002	3.4849-001	1.0000+000	2.3073+000	-1.1637+000	-7.0253-002	-8.5130-001	-1.0159+000	1.7002-002
10	0.0000	-1.0733-002	-1.1084-001	3.7236-001	8.5725-001	-4.3536-001	-9.3744-002	-2.8685-001	-3.1633-001	5.6380-003
11	0.0000	-3.5681-003	-3.2494-002	1.8025-001	3.1610-002	-9.9640-002	-1.1106-001	-3.1950+000	-1.3342+000	-3.5737-001
12	0.0000	-3.9997-006	-1.9092-004	-7.4092-004	-6.4479-003	2.6670-003	8.8933-002	-1.2786+000	-2.5154+000	1.0000+000
13	0.0000	-1.8620-002	1.0000+000	-5.8146-001	7.4510-002	-5.4161-001	-6.7669-002	-3.9147+000	-2.3562+000	3.5809-001

T22

	11	12	13
1	5.2145-003	2.0774-003	-7.9104-003
2	-5.1020-001	-8.0413-001	-1.1219-001
3	3.1258-001	6.1223-002	-6.2966-002
4	3.4655-001	3.4728-001	-9.5817-002
5	-1.2141+000	-2.6251-001	-3.1096-002
6	-1.2214+000	-1.5121-001	1.7538-002
7	-1.2750-001	-1.4986-002	-4.4707-002
8	-6.7644-001	-8.5515-002	1.7738-002
9	-8.4501-001	-4.1312-001	7.8056-003
10	-2.9654-001	-1.1041-001	1.0000+000
11	1.0227+001	6.8203+000	3.9256-002
12	-2.3578+000	-1.1335+001	-7.0337-002
13	8.1214+000	-2.9178+000	-3.5707-002

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LAMR42

	1	2	3	4	5	6	7	8	9	10
1	-2.5000-001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
2	0.0000	-4.4013+002	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
3	0.0000	0.0000	-5.0981+001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4	0.0000	0.0000	0.0000	-5.7419+001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000	0.0000	-4.4454+001	1.6038+000	0.0000	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.0000	0.0000	-1.6038+000	-4.4454+001	0.0000	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-6.9357-001	0.0000	0.0000	0.0000
8	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-1.7078+001	2.6636+000	0.0000
9	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-2.6636+000	-1.7078+001	0.0000
10	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-1.9390+001
11	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
12	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
13	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

197

LAMR42

	11	12	13
1	0.0000	0.0000	0.0000
2	0.0000	0.0000	0.0000
3	0.0000	0.0000	0.0000
4	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.0000
8	0.0000	0.0000	0.0000
9	0.0000	0.0000	0.0000
10	0.0000	0.0000	0.0000
11	-2.6585+001	3.0423-001	0.0000
12	-3.0423-001	-2.6585+001	0.0000
13	0.0000	0.0000	-1.3416+000

T12

	1	2	3	4	5	6	7	8	9	10
1	0.0000	-2.1400-003	2.4200-003	-6.2482-003	-2.4620-002	1.1192-002	4.0737-001	6.7213-002	3.2461-002	-4.3502-003
2	0.0000	7.2982-004	2.1500-004	-2.3134-003	1.4994-002	1.9108-003	6.0188-002	1.6858-003	7.6875-003	1.0252-003
3	0.0000	-5.5491-003	5.7993-003	7.2863-003	2.3246-002	-2.7012-002	2.3247-001	1.6744-001	2.7635-002	-6.4198-003
4	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	5.0985-004	2.4006-003	-5.2947-002	-3.4967-002	-2.3127-003	2.9905-001	-4.2420-001	1.0110-001	4.2479-002

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T12	11			12			13		
	1	2	3	1	2	3	1	2	3
1	0.1421-002	0.1324-002	-2.0476-001						
2	3.1930-002	-5.6357-003	-2.0481-003						
3	-4.1574-001	-4.9590-002	-2.8700-001						
4	0.0000	0.0000	0.0000						
5	-1.1540-000	-3.8308-001	-8.2080-002						

M1	1			2			3			4			5		
	1	2	3	1	2	3	1	2	3	1	2	3	1	2	3
1	-1.1647-000	-6.1874-000	3.7113-000	6.0284-001	3.5373-001										
2	1.1079-000	2.0425-001	-7.4454-002	-6.4548-003	-5.9165-004										
3	0.0000	0.0000	0.0000	0.0000	0.0000										
4	0.0773-000	4.2288-000	-1.4554-000	-1.7709-001	-7.5753-003										
5	2.0776-000	1.0032-001	9.6353-001	3.4919-001	-4.5223-000										
6	4.1241-001	1.0257-001	-4.0907-001	-6.6441-002	1.3550-002										
7	2.0347-001	4.3041-002	-1.1735-001	-1.4284-002	2.8018-003										

M2	1			2			3			4			5			6			7			8			9			10		
	1	2	3	1	2	3	1	2	3	1	2	3	1	2	3	1	2	3	1	2	3	1	2	3	1	2	3	1	2	3
1	0.0000	3.0656-000	3.0223-000	-5.0626-001	-4.0458-001	3.1123-001	-8.5742-002	-1.9913-000	-1.3573-001	-1.4748-001																				
2	0.0000	2.1541-003	-1.1324-001	-5.2341-002	2.3498-003	2.3011-003	2.3988-003	2.3498-003	2.3986-003	2.3982-003																				
3	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000																				
4	0.0000	4.2854-002	-2.7385-000	-1.0240-000	4.6942-002	4.5565-002	4.7321-002	4.6412-002	4.7318-002	4.7768-002																				
5	0.0000	-2.8202-002	-7.2342-000	6.7861-001	-3.1379-002	-3.0019-002	-3.1246-002	-3.1250-002	-3.1574-002	-3.1249-002																				
6	0.0000	1.4798-002	-4.1339-002	-4.3747-002	1.5857-002	1.5823-002	1.5855-002	1.6028-002	1.5855-002	1.6212-002																				
7	0.0000	3.1036-003	1.0398-002	1.4680-002	3.3476-003	3.5054-003	3.3983-003	3.3981-003	3.3977-003	3.4098-003																				

M2	11			12			13		
	1	2	3	1	2	3	1	2	3
1	1.5163-000	1.0332-000	-1.1572-001						
2	1.9091-003	-2.0376-003	2.1992-003						
3	0.0000	0.0000	0.0000						
4	3.7933-002	-5.4704-002	4.7307-002						
5	-2.0896-002	3.7733-002	-3.1374-002						
6	1.2550-002	-2.0240-002	1.5856-002						
7	2.4700-003	-4.0720-003	3.1945-003						

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XT2

	1	2	3	4	5
1	3.7307-002	-5.4303-003	9.0749-004	3.0948-003	8.2070-002
2	2.2382+000	6.4117+000	-7.3715-001	4.4571+000	2.9500+002
3	3.0115+001	5.7379+000	-1.0040+000	-1.8117+001	-2.5769+002
4	3.2125+001	4.3209+000	-2.1524+000	-1.5578+001	-2.2081+002
5	5.2866+000	8.2323-001	-1.0533-001	-1.5367+000	-2.1437+001
6	3.1624+001	3.9145+000	-1.4530+000	-1.1270+001	-1.6913+002
7	1.4030-001	-3.3375-002	2.0342-003	9.2060-003	4.0485-001
8	1.6032+000	6.8787-001	6.5220-002	1.4453-001	-1.1322-001
9	-5.6127-001	-1.5747+000	-2.3233-001	-1.4022-001	2.6772+000
10	9.7312-001	1.2537+000	-2.7795+000	1.6647+000	2.4640+001
11	-3.0278-001	4.4550-002	5.1902-002	1.4347-001	2.4077+000
12	-4.0378-002	1.0302-001	-1.4532-001	1.1210-001	8.3503-001
13	7.0829-001	1.0555-001	2.2100-002	6.1811-002	2.2572-001

TT1 INVERSE

	1	2	3	4	5
1	-2.2941-001	-3.2805+000	-1.4413-001	-2.0770-001	1.0795+000
2	1.7001+000	1.2424+001	-3.3075-001	2.7710-001	3.3507-002
3	-2.0186+000	1.6377+001	-1.0303-001	3.0578-001	1.0307+002
4	-9.8949-001	5.0140-001	1.0569+000	5.0170-001	1.9496+002
5	0.0000	0.0000	0.0000	1.0000+000	0.0000

FP

	SUFAT	SUCOM	PTTX	WFCOM	PT3
SUFAT	-1.1653+000	-4.2561-001	-6.3737-001	1.1481-001	1.1705+000
SUCOM	-2.8040-002	-1.8174+000	-1.1730-001	1.0529-001	2.3386-001
PTTX	4.8613+000	-9.1546+000	-7.2911+000	1.2631+000	2.9298+000
WFCOM	0.0000	0.0000	0.0000	-1.0000+001	0.0000
PT3	2.6542+001	3.5547+002	1.4463+001	2.1730+001	-1.1794+002

FIG 00 LINEAR MODEL .9/30K 20 3/9/76

UNNORMALIZED EIGENSYSTEM.

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-1.19293+0.021+J(0.00000)	0.00000	1.00000	1 (1.00000+0.000+J(0.00000)	1.0000000	.00000
			2 (3.18410-0.011+J(0.00000)	.3184100	.00000
			3 (3.23108-0.033+J(0.00000)	.0032311	.00000
			4 (0.00000)+J(0.00000)	.0000000	.00000
			5 (-9.27943-0.011+J(0.00000)	-.9279431	.00000
(-6.53325+0.001+J(0.00000)	0.00000	1.00000	1 (1.00000+0.000+J(0.00000)	1.0000000	.00000
			2 (3.18455-0.011+J(0.00000)	.3184547	.00000
			3 (1.62622-0.021+J(0.00000)	.0162622	.00000
			4 (0.00000)+J(0.00000)	.0000000	.00000
			5 (2.39005-0.021+J(0.00000)	.0239005	.00000
(-1.18998+0.001+J(3.91995-0.011)	1.25279+0.000	.94979	1 (1.00000+0.000+J(0.00000)	1.0000000	.00000
			2 (5.93854-0.021+J(1.82448-0.011)	.1920253	71.82853
			3 (1.02139-0.033+J(-7.66909-0.05)	.0010243	-4.29396
			4 (0.00000)+J(0.00000)	.0000000	.00000
			5 (4.07890-0.033+J(3.20660-0.03)	.0051884	38.17242
(-1.00000+0.011+J(0.00000)	0.00000	1.00000	1 (-4.19044-0.011+J(0.00000)	-.4190443	.00000
			2 (-3.40319-0.011+J(0.00000)	-.3403189	.00000
			3 (-4.88381-0.033+J(0.00000)	-.0048838	.00000
			4 (1.00000+0.000+J(0.00000)	1.0000000	.00000
			5 (1.91492-0.033+J(0.00000)	.0019149	.00000

LEAPD12 INVERSE

1	2	3	4	5	6	7	8	9	10
1 -4.0000+0.00	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
2 0.0000	-2.0819-0.01	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
3 0.0000	0.0000	-1.0615-0.02	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4 0.0000	0.0000	0.0000	-1.7418-0.02	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5 0.0000	0.0000	0.0000	0.0000	-2.2266-0.02	-7.9614-0.04	0.0000	0.0000	0.0000	0.0000
6 0.0000	0.0000	0.0000	0.0000	7.9614-0.04	-2.2266-0.02	0.0000	0.0000	0.0000	0.0000
7 0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-1.2418+0.00	0.0000	0.0000	0.0000
8 0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-5.7163-0.02	-8.9151-0.03	0.0000
9 0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	8.9151-0.03	-5.7163-0.02	0.0000
10 0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-5.1573-0.02
11 0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
12 0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
13 0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

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LAMBDA2 INVERSE

	11	12	13
1	0.0000	0.0000	0.0000
2	0.0000	0.0000	0.0000
3	0.0000	0.0000	0.0000
4	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.0000
8	0.0000	0.0000	0.0000
9	0.0000	0.0000	0.0000
10	0.0000	0.0000	0.0000
11	0.0000	0.0000	0.0000
12	0.0000	0.0000	0.0000
13	0.0000	0.0000	0.0000

Go	WFCM	AMTX	CIVV	RCVV	HLC
SVFAN	-0.2440-002	3.8226-002	1.0843-002	9.2905-003	8.4126-001
SNCOM	-0.3101-002	2.9113-003	8.8403-003	3.5871-002	-1.2394-001
PT7M	-2.1254-001	-6.0509-000	-9.1662-002	2.8669-001	-1.8874-000
WFCOM	1.0000-001	0.0000	0.0000	0.0000	0.0000
PT3	-5.9642-000	-2.8133-000	-2.5565-000	-1.0032-001	-1.2615-002

He	F14X	WFCM	TTU	SPAF	SMHC
SVFAN	-0.1973-003	1.1123-001	-2.0547-003	-5.0497-003	1.0729-004
SNCOM	-1.8545-002	-1.1037-000	2.8228-001	-1.8493-002	1.0465-000
PT7M	1.0876-001	-1.8539-001	7.0582-002	-2.1756-002	4.3924-003
WFCOM	1.6843-001	-4.4535-001	1.7520-001	-4.3804-002	6.4621-003
PT3	7.7191-002	1.1423-000	7.1324-002	1.8420-002	-4.6222-002
PT1Y	-0.1645-002	-5.4527-001	-7.1300-003	5.7134-001	4.3706-003
PT45	-9.7486-003	5.9705-001	-9.0791-003	5.3954-002	1.6418-003
TT25M	-0.8561-002	-6.3419-001	-9.6595-003	4.9334-001	-6.0086-003
TT25C	-4.8733-002	-8.2522-001	6.0523-002	5.5753-001	1.0502-002
TT3	-6.7511-002	-1.2230-000	3.1561-002	1.1404-001	1.9180-003
TT4PHI	-1.7607-001	-1.4740-000	2.3975-001	8.2195-001	4.8689-002
TT4PLU	1.0544-001	-4.6230-001	2.6719-001	-1.2820-001	6.9942-003
TT4	-2.8770-001	1.7387-001	3.7221-001	5.8928-001	-1.3364-001

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Mo	FTT	PT45	TT25H	TT25C	TT3
FMY	-5.7874-001	-1.2107+001	5.2561+000	4.0972-001	3.6590+000
MEAN	1.4697+000	2.3608-001	-9.3001-002	6.4094-003	6.9113-004
TT4	-4.8541-002	-6.3419-001	-9.0095-003	4.9334-001	-6.0086-003
SWAF	1.3218+000	5.0549+000	-1.7494+000	7.6129-002	1.4322-002
SWMC	1.1789+000	1.1170+001	5.5155-001	3.7828-001	-4.5763+000
Dp25Q1	5.4534-001	4.6583-002	-5.0001-001	-1.2047-002	2.7148-002
Dp25SC	2.0550-001	2.5475-002	-1.1219-001	-4.2374-003	5.9606-003

De	FMY	MEAN	TT4	SWAF	SWMC
SWAFN	1.0951-001	-2.8407-002	3.5110-003	1.2161-002	3.5836-001
SWCMH	-2.8978-002	5.7447-002	6.4595-003	2.9534-002	6.3415-001
PT7H	1.6021-002	2.5015-002	5.0353-003	5.4465-003	8.3007-003
MFCCM	3.3450-002	6.2248-002	1.3096-003	1.3541-002	2.5059-002
PT3	-4.8766-003	3.0141-002	1.6928-003	-6.0477-003	-2.3464-001
FTT	-2.0711-001	3.0447-002	1.0997-002	3.3074-002	2.9508-001
PT45	1.7605-001	-4.5158-002	5.1417-003	1.6416-002	6.0105-001
TT25H	-1.0026-001	3.1226-002	1.1432-002	3.5217-002	3.7575-001
TT25C	-1.6019-001	5.8433-002	1.3100-002	4.0224-002	4.6923-001
TT3	3.2429-001	6.8398-002	1.0059-002	4.4603-002	2.9312-001
TT4PH1	-4.6717-001	1.1630-001	1.0413-002	5.8474-002	6.2242-001
TT4PH2	1.0138-001	1.4410-001	3.6623-003	1.8670-002	6.8733-002
TT4	-3.4442-001	1.6445-001	1.3412-002	2.8471-003	1.1420-001

De	FMY	MEAN	CTV	RCV	RLC
FMY	-0.9531-001	-2.6503-002	9.1726-002	3.8402-001	2.1600+000
MEAN	-6.1537-003	-6.4445-003	-3.4795-002	-8.0508-003	1.3425-002
TT4	-1.0026-001	3.1226-002	1.1432-002	3.5217-002	3.7575-001
SWAF	-1.2047-001	-2.5203-001	4.8218-001	-1.7330-001	-3.6235-001
SWMC	-7.0353-002	2.0653-002	9.8355-002	3.7771-001	-7.3514-001
Dp25Q1	-1.4176-002	2.5344-002	-2.5045-003	-2.0094-003	1.4264-001
Dp25SC	-2.0048-003	6.8531-003	-5.1154-003	-7.0646-004	3.2454-002

0EIT,II KENEF100ALT,SRB83-09-10
 PROCESSED BY UNIVAP 1100 SERIES FLY PROCESSOR LEVEL 4B AT 5:01:29 PM ON TUESDAY, MARCH 9, 1976 (CREATING CYCLE 0)

1.	F	REDUCED MATRICES	.9/30K	20	FIFTH ORDER
2.		-.115+01	-.2701+00	-.5692+03	-.5623+00
3.		-.4220+01	-.1417+01	-.1477+03	-.2002+01
4.		-.5052+02	-.7273+02	-.7281+01	-.1215+01
5.		.0000	.0000	.0000	.0000
6.		.2387+00	-.2106+01	-.1078+03	-.1552+01
7.	G				
8.		-.4709+00	-.7701+02	-.4432+01	-.2920+01
9.		-.5220+00	-.0201+01	-.3386+01	-.1777+02
10.		-.2045+02	-.1535+02	-.2788+01	-.1049+00
11.		.1000+02	.0000	.0000	.0000
12.		-.4277+00	-.5317+02	-.5620+01	-.2902+02
13.	HY				
14.		-.3443+01	-.4238+00	-.2427+03	-.2620+00
15.		.1004+01	-.1606+02	-.7546+00	-.5055+03
16.		-.1272+01	-.1054+00	-.1402+01	-.9933+00
17.		.1152+03	.1114+03	-.4989+01	-.2031+00
18.		.3549+04	.2144+03	.1334+01	.8600+04
19.		.9614+04	.9043+05	-.0574+01	-.1636+04
20.		.3362+04	.2861+05	-.1475+01	-.5360+05
21.	UY				
22.		-.2201+00	-.3230+01	-.1341+01	-.6884+01
23.		-.4553+03	-.1350+00	-.176+01	-.2590+01
24.		-.2019+00	.1656+02	-.7276+00	-.2698+01
25.		-.3219+04	-.1843+01	-.4066+02	.1880+02
26.		-.1617+04	-.1266+02	.7235+03	-.3498+02
27.		-.2076+04	.8449+02	.1027+03	.1030+03
28.		-.3042+05	.2264+02	.2046+03	.3654+04

END FLT. TIME: 2.2494 SECONDS.

0FTN

CASE 6

THE REDUCED MATRICES FR,GR,HR,DR WILL BE SAVED FOR OPTSYS ON FILE 12
INTERMEDIATE DATA WILL BE READ FROM RECORD NO. 6 OF FILE 10

THERE WILL BE 10 EIGENVALUES ELIMINATED. THE TOLERANCE LEVEL FOR ELIMINATION IS .100
2 OF THESE EIGENVALUES ARE COMPLEX. TO BE ELIMINATED ARE--

(-.250000+000. 000000)
(-.830700+003. 000000)
(-.868000+002. 000000)
(-.498700+002. 120000+000)
(-.201000+001. 000000)
(-.28--00+002. 537900+001)
(-.240100+002. 000000)
(-.195100+002. 000000)
(-.212300+002. 000000)
(-.204000+002. 000000)

THE IDENTIFYING TITLE FOR FR,GR,HR,DR ON OPTSYS OUTPUT =REDUCED MATRICES 0/OK 20 FIFTH ORDER

F100 LINEAR MODEL 0/OK 20 2/17/76

LAMRDA1	1	2	3	4	5
1	-1.4442+002	0.0000	0.0000	0.0000	0.0000
2	0.0000	-7.5659-001	0.0000	0.0000	0.0000
3	0.0000	0.0000	-5.1471+000	2.2711+000	0.0000
4	0.0000	0.0000	-2.2711+000	-5.1471+000	0.0000
5	0.0000	0.0000	0.0000	0.0000	-1.0000+001

T11	1	2	3	4	5
1	-1.2653+002	9.0600-001	9.1467-001	-2.8565-001	-6.4656-002
2	-5.6634-003	2.1906-001	-3.9552-002	2.3859-002	-2.6611-002
3	-2.1300+002	1.2738-001	1.6089-001	-1.2082-001	1.0109-001
4	0.0000	0.0000	0.0000	0.0000	9.2743-001
5	1.0000+000	1.0000+000	-2.0934-001	3.7969-001	1.0026-001

X11	1	2	3	4	5
1	1.0950+001	9.5944+000	-3.4374+000	-3.4801+001	-1.0593+002
2	9.6567-001	1.8744-001	6.6648-003	-1.1622-002	-1.8668+000
3	1.0520+000	6.4615-001	1.1316-001	-3.4974-001	-2.7781+000
4	3.4617+000	2.1597+000	1.8548-001	-4.5862-001	-5.9970+000
5	1.0782+001	0.0000	0.0000	0.0000	0.0000

T21

	1	2	3	4	5
1	-9.6752-005	1.0646-001	-9.0366-003	8.4137-003	-8.2872-003
2	4.8155-001	4.9355-001	1.5770-002	9.0041-002	1.2976-001
3	-5.0691-003	1.4524-001	3.1690-001	-3.9728-001	-2.2067-002
4	-7.1068-003	1.3119-001	3.5640-001	-4.9749-001	-5.3393-003
5	-1.3322-002	2.8735-001	7.2173-002	-1.8718-001	2.0511-002
6	2.3557-002	-2.6732-001	1.2235-001	-3.8635-001	4.2600-001
7	-4.0904-002	-2.0940-001	1.5177-001	-3.5304-001	5.4302-001
8	1.0816-001	-3.7941-001	2.1007-001	-4.8800-001	8.3721-001
9	4.2426-002	-5.1633-001	-5.6167-002	-1.1121-001	1.5989-001
10	5.4601-002	-4.7166-001	2.4043-001	-6.8714-001	1.0000+000
11	1.3700-003	1.3423-001	3.6087-001	-7.1986-001	-1.0487-002
12	-1.0701-001	-1.4690-001	-3.1120-002	-6.2948-001	8.0029-001

T22

	1	2	3	4	5	6	7	8	9	10
1	1.0000+000	2.7497-004	-7.1767-005	2.3779-003	2.7350-004	-6.6215-003	-7.0342-004	-5.8002-003	7.4963-004	8.6388-005
2	0.0000	1.0000+000	4.5690-001	1.7052-004	-1.6926-003	-3.9499-002	1.6235-003	-2.7685-001	-7.1633-002	-6.1368-002
3	0.0000	-6.3849-004	-3.4196-002	2.0876-003	-1.7189-003	-2.9971-002	-1.2748-001	1.4510-001	-5.0646-002	7.1348-003
4	0.0000	-7.0431-004	-5.0000-002	-4.7545-004	1.5058-003	-2.1562-002	-1.5032-001	1.8380-001	-6.5183-002	2.4131-002
5	0.0000	5.4048-004	-3.4121-002	-1.2194-004	3.2761-004	-1.5102-002	1.3505-001	1.9488-002	9.5580-002	-1.7419-002
6	0.0000	-1.6301-004	-1.7152-001	-9.6563-001	9.0772-001	-7.8166-003	5.7638-001	8.5323-001	-3.1214-002	6.0949-004
7	0.0000	2.9298-003	1.4159-001	-5.3631-003	-5.5117-004	-6.8463-003	1.5062-001	5.7184-001	-2.5586-002	1.8797-003
8	0.0000	-1.7725-002	4.8338-002	-9.1884-001	-1.0303-001	-1.6194-002	5.1121-001	1.0605+000	-1.3907-001	-1.3315-002
9	0.0000	-7.0636-003	1.8452-002	-3.4447-001	-3.8582-002	1.0000+000	1.9886-001	3.6637-001	-4.8108-002	-4.4113-003
10	0.0000	-1.9426-003	4.5741-002	-4.3677-002	-2.0707-003	-3.1416-002	1.1819+000	-6.6022-001	5.3506-001	-5.5169-001
11	0.0000	-2.5391-004	1.1675-002	-2.2039-003	1.9027-003	-2.1697-002	4.7593-001	8.7178-002	3.1508-001	1.0000+000
12	0.0000	-2.2478-004	-4.1728-001	-6.4283+000	7.3952+000	6.4925-002	1.4037+000	-1.7776+000	1.0000+000	-2.3577-002

T22

	11	12
1	-4.3432-004	-2.0354-004
2	1.0049-002	-6.6215-002
3	-4.8455-002	4.1059-003
4	-6.4344-002	-2.0561-002
5	1.7888-001	1.5741-002
6	1.6858-001	5.1470-002
7	8.3956-002	3.1743-002
8	1.0400-001	3.2055-002
9	3.5157-002	1.0748-002
10	-4.0217-001	-2.7433-001
11	1.0000+000	1.0000+000
12	1.1224-001	4.2315-002

LAMDA2

	1	2	3	4	5	6	7	8	9	10
1	-2.5000-001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
2	0.0000	-8.1070+002	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
3	0.0000	0.0000	-8.6902+001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4	0.0000	0.0000	0.0000	-4.9880+001	1.4080-001	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000	-1.4080-001	-4.9880+001	0.0000	0.0000	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.0000	0.0000	0.0000	-2.0184+000	0.0000	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-2.4687+001	8.3792+000	0.0000	0.0000
8	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-8.3792+000	-2.4687+001	0.0000	0.0000
9	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-2.4016+001	0.0000
10	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-1.9518+001
11	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
12	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

LAMDA2

	11	12
1	0.0000	0.0000
2	0.0000	0.0000
3	0.0000	0.0000
4	0.0000	0.0000
5	0.0000	0.0000
6	0.0000	0.0000
7	0.0000	0.0000
8	0.0000	0.0000
9	0.0000	0.0000
10	0.0000	0.0000
11	2.1236+001	0.0000
12	0.0000	-2.0402+001

T12

	1	2	3	4	5	6	7	8	9	10
1	0.0000	-4.4267-003	-7.7850-003	1.5017-002	8.7290-004	-2.8398-001	-4.7296-002	-3.9265-002	-1.3888-002	-1.0547-003
2	0.0000	8.3155-004	-8.2083-003	2.4378-004	-1.4393-004	-1.6060-003	-6.5575-003	-5.4374-003	-5.4658-003	-1.1043-003
3	0.0000	-6.7584-003	-2.6736-002	4.4273-003	-4.6109-003	-4.6235-002	-2.4249-001	-8.4341-002	-2.5241-001	-9.4347-002
4	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	-2.3001-002	1.0000+000	-8.1174-003	4.6362-003	-1.1788-002	2.7071-001	-6.2925-001	1.5641-001	-3.1979-002

T12

	11	12
1	-2.1121-002	-4.4996-003
2	-6.4402-003	-2.4330-003
3	-1.1146-001	-1.1538-001
4	0.0000	0.0000
5	1.6215-001	-2.0058-002

Find Linear Model O/K 20 2/17/76

H1	1	2	3	4	5	6	7	8	9	10
1	4.9947-001	-2.1214+000	4.2398+000	3.5081-001	1.1361-001	6.4364-001	-1.0757+000	-7.9507-002	-8.1457-002	2.4483-001
2	9.0297-001	2.1150-001	-2.6958-001	2.1503-001	-6.6778-002	4.1082-001	-5.2544-001	-5.1405-002	-5.1190-002	-8.9442-002
3	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.0000+000	0.0000	0.0000	0.0000
4	-1.4418+000	5.2548+000	-6.1130+000	4.8339+000	-1.5141+000	9.3198+000	-1.1911+001	-1.1650+000	-1.1607+000	-1.1195+000
5	7.2648+000	1.3004+002	8.1094+000	-2.9858+000	-1.3783+001	-1.2379+001	1.5837+001	1.5480+000	1.5421+000	1.4912+000
6	9.8666-002	-4.9151-002	-5.4347-001	4.1866-001	-1.0737-001	8.3175-001	-1.0643+000	-1.0389-001	-1.0404-001	-1.0020-001
7	5.8398-002	-1.1075-002	-1.1500-001	8.8020-002	-2.1244-002	1.7691-001	-2.2629-001	-2.2082-002	-2.2060-002	-2.1185-002

H2	1	2	3	4	5	6	7	8	9	10
1	0.0000	1.0278+000	1.0368+000	-1.2261-001	-1.8846-001	6.4364-001	-1.0757+000	-7.9507-002	-8.1457-002	2.4483-001
2	0.0000	-4.3330-002	-2.3340-001	-7.5807-002	-9.2379-002	4.1082-001	-5.2544-001	-5.1405-002	-5.1190-002	-8.9442-002
3	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.0000+000	0.0000	0.0000	0.0000
4	0.0000	-5.8159-001	-5.2935+000	-1.7189+000	-2.0994+000	9.3198+000	-1.1911+001	-1.1650+000	-1.1607+000	-1.1195+000
5	0.0000	1.3071+000	-6.8987+001	2.2853+000	2.7896+000	-1.2379+001	1.5837+001	1.5480+000	1.5421+000	1.4912+000
6	0.0000	-8.8413-002	-1.4872-001	-7.5097-002	-1.8807-001	8.3175-001	-1.0643+000	-1.0389-001	-1.0404-001	-1.0020-001
7	0.0000	-1.1880-002	2.4514-003	-5.9414-004	-4.0024-002	1.7691-001	-2.2629-001	-2.2082-002	-2.2060-002	-2.1185-002

H2	11	12
1	7.9014-002	-8.1993-002
2	-5.7018-002	-5.1320-002
3	0.0000	0.0000
4	-1.2923+000	-1.1642+000
5	1.7175+000	1.5515+000
6	-1.1591-001	-1.0387-001
7	-2.4872-002	-2.2074-002

X12	1	2	3	4	5	6	7	8	9	10
1	-3.8078-002	-2.1578-002	7.6091-005	1.1536-002	2.4225-001	6.4364-001	-1.0757+000	-7.9507-002	-8.1457-002	2.4483-001
2	-2.3502-001	-2.5710+000	6.1212-002	8.3197+000	7.2764+001	4.1082-001	-5.2544-001	-5.1405-002	-5.1190-002	-8.9442-002
3	-1.3377+001	-8.9114+000	1.2261+000	1.1774+001	4.6052+001	0.0000	1.0000+000	0.0000	0.0000	0.0000
4	-2.4490+000	-8.6806-001	-1.0701-001	1.0233-003	-5.0187-001	9.3198+000	-1.1911+001	-1.1650+000	-1.1607+000	-1.1195+000
5	-3.3057+000	-9.1990-001	-9.9482-003	1.6899-001	3.3374+000	-1.2379+001	1.5837+001	1.5480+000	1.5421+000	1.4912+000
6	1.1162+000	5.4827-002	1.4690-002	7.3252-002	-3.5732-001	8.3175-001	-1.0643+000	-1.0389-001	-1.0404-001	-1.0020-001
7	-1.2032+001	-5.5285+000	1.3676-001	2.5335+000	-2.2491+000	1.7691-001	-2.2629-001	-2.2082-002	-2.2060-002	-2.1185-002
8	-2.1172-001	4.7293+000	2.2746-001	1.7375+000	8.6832+000	6.4364-001	-1.0757+000	-7.9507-002	-8.1457-002	2.4483-001
9	1.4147+001	1.8341+001	2.5678-001	-1.9967+000	7.7179+000	4.1082-001	-5.2544-001	-5.1405-002	-5.1190-002	-8.9442-002
10	3.4426-001	1.2014+000	-3.6421-001	7.6336-001	7.0553+000	0.0000	1.0000+000	0.0000	0.0000	0.0000
11	1.4545+000	-1.5817+000	-2.3027-001	-2.6604+000	-2.8850+001	9.3198+000	-1.1911+001	-1.1650+000	-1.1607+000	-1.1195+000
12	1.7567+000	-1.8376+000	5.0035-001	8.7314-001	1.6259+001	-1.2379+001	1.5837+001	1.5480+000	1.5421+000	1.4912+000

F100 LUMP SUM MODEL 0/OK 20 2/17/76

TII INVERSE

	1	2	3	4	5
1	-6.455-001	-4.468+000	3.090+000	-7.187+001	1.048+000
2	3.381-002	3.402+000	7.929+001	2.081-002	3.885-002
3	1.887+000	-3.263+000	-5.457+000	6.439-001	-1.107-001
4	2.661+000	4.869-001	-1.538+001	1.908+000	-2.913-001
5	0.000	0.000	0.000	1.072+000	0.000

FR

	SNEAN	SNECM	PTM	WECOM	PT3
SNEAN	5.795-001	4.119+000	-2.589+001	3.527+000	1.305+000
SNECM	-8.210-001	-5.440+000	5.523+000	-6.139-001	8.965-001
PTM	-4.182-001	-1.245+001	-2.258+001	-1.775+000	2.597+000
WECOM	0.000	0.000	0.000	-1.000+001	0.000
PT3	8.772+001	6.497+002	-5.289+002	9.820+001	-1.507+002

LAMRDP INVERSE

	11	12
1	0.0000	0.0000
2	0.0000	0.0000
3	0.0000	0.0000
4	0.0000	0.0000
5	0.0000	0.0000
6	0.0000	0.0000
7	0.0000	0.0000
8	0.0000	0.0000
9	0.0000	0.0000
10	0.0000	0.0000
11	-4.7090-002	0.0000
12	0.0000	-4.9015-002

GR

	MEMH	ANMTX	CTVV	RCVV	BLC
SNEAN	-2.0941-000	-4.0165-000	-6.2944-002	-1.0614-001	-3.6998-000
SNCOM	5.3593-001	1.0345-000	3.5363-002	1.3068-001	6.2265-001
PT7M	1.4252+000	5.4264-002	2.4043-002	3.9505-001	1.9109+000
WFCOM	1.0000+001	0.0000	0.0000	0.0000	0.0000
PT3	-6.2085+001	-9.4925+001	-4.2002+000	-2.1185+001	-1.4623+002

H*

	FMMX	MEAN	TT4	SMAF	SMHC
SNEAN	9.0141-003	4.3880-001	3.8212-003	3.5875-003	2.5838-003
SNCOM	-2.4734-002	-3.7991-001	8.0214-001	-1.3922-002	4.9614-001
PT7M	-4.5151-001	-6.4878-001	4.4823+000	-5.7124-001	8.1019-002
WFCOM	-6.4288-001	-8.7222-001	5.7897+000	-7.1791-001	1.0314-001
PT3	-3.2715-001	9.1751-001	2.5751+000	-2.5745-001	2.2095-002
TT1	-7.4290-001	-1.7424+000	5.0552+000	9.4831-003	1.1146-001
PT45	-6.7425-001	-1.5952+000	4.1923+000	3.5598-002	2.7244-002
TT25H	-9.4584-001	-2.4729+000	6.4872+000	-1.9477-001	2.1779-001
TT25C	-4.4690-001	-2.0320+000	1.7740+000	-1.1725-001	6.3050-002
TT3	-1.4267+000	-3.1671+000	9.1033+000	-1.2736-001	2.1251-001
TT4PH1	-1.2315+000	-1.0049+000	9.2267+000	-1.1508+000	1.7663-001
TT4	-1.6694+000	-2.6350-001	9.3220+000	-2.8462-001	6.8938-002

HR	FTT	PT45	TT25H	TT25C	TT3
FMX	1.3119-001	-3.0953+000	8.7756+000	-2.2454-001	7.7094-001
MFAN	1.4002+000	9.8248-001	-4.0329+000	5.1497-001	-4.2412-001
TT4	-0.1325-001	-1.5952+000	4.1923+000	3.5596-002	2.7244-002
SMAF	9.8312+000	2.2272+001	-9.1439+001	1.1634+001	-2.8137+000
SMHC	2.6504-001	1.5673+002	-2.1916+002	1.1401+001	-1.8213+001
DP25C	0.0981-001	1.1635+000	-4.2041+000	7.8533-001	-1.8449-001
DP25SC	2.0163-001	1.9519-001	-1.0906+000	1.3573-001	-3.4442-002

D*	FMX	MFAN	TT4	SMAF	SMHC
SNFAN	-1.5318-001	-8.4669-002	3.3769-004	4.5925-002	9.6916-001
SNCOM	2.3813-002	5.0589-002	1.4879-003	1.2688-002	1.4125-001
PT7M	0.1068-001	7.4690-001	2.2591-002	1.7436-002	5.3745-001
MFCCM	5.2176-001	9.9197-001	2.8331-002	2.3410-002	6.7997-001
PT3	2.1196-001	4.5062-001	1.4356-002	-4.4759-003	5.5230-002
FTT	2.6156-001	9.1090-001	3.3964-002	7.3932-002	6.2189-001
PT45	2.8914-001	7.5082-001	2.8167-002	6.9465-002	6.1692-001
TT25H	4.0803-001	1.1470+000	4.3279-002	1.1061-001	8.9448-001
TT25C	6.2327-001	1.5139-001	1.9418-002	7.2371-002	9.3582-002
TT3	2.9605-001	1.6143+000	5.9990-002	1.1897-001	1.0286+000
TT4PHI	8.8304-001	1.4227+000	5.0555-002	2.7110-002	8.9561-001
TT4	3.1165-001	1.6339+000	6.5485-002	1.4433-002	9.1240-001

DR	FMX	ANMIX	CIVV	RCVV	BLC
FMX	2.3656-001	6.3526-001	-1.6741-003	1.0317-001	1.3099-001
MFAN	-3.1341-001	-6.6421-001	-5.6215-002	-2.7556-002	-6.5124-001
TT4	2.8914-001	7.5082-001	2.8167-002	6.9465-002	6.1692-001
SMAF	-5.5821+000	-1.5056+001	5.0317-001	-6.2535-001	-1.4872+001
SMHC	-2.1140+001	-3.7743+001	-1.2822+000	-3.5041+000	-2.6123+001
DP25C	-5.0405-001	-1.0200+000	-2.9192-002	-2.9686-002	-1.0921+000
DP25SC	-8.5266-002	-1.7568-001	-8.1267-003	-4.4399-003	-1.9959-001

[illegible]

CASE 7

THE REDUCED MATRICES FR.G.O.W.D.B WILL BE SAVED FOR OPTSYS ON FILE 12
INTERMEDIATE DATA WILL BE READ FROM RECORD NO. 3 OF FILE 10

THESE VALUES ARE COVERED BY THE TOLERANCE LEVEL FOR ELIMINATION IS .100

[illegible]

THE IDENTIFYING TITLE FOR FD-302, P. 1, ON OPTSYS OUTPUT REDUCED MATRICES 0/OK 52 FIFTH ORDER

F100 LINEAR MODEL O/OX 52 2/13/76

LAMBDA1

1	-1.4008+002	0.0000	0.0000	0.0000	0.0000
2	0.0000	-4.0281+000	3.0526+000	0.0000	0.0000
3	0.0000	-3.0622+000	-4.0281+000	0.0000	0.0000
4	0.0000	0.0000	0.0000	-2.7039+000	0.0000
5	0.0000	0.0000	0.0000	0.0000	-1.0000+001

T11

1	-1.7544+002	-1.5403+001	5.1112+001	5.4259+001	-2.1340+001
2	-4.3448+003	-5.4549+002	4.6092+002	4.0303+001	-1.0644+001
3	-2.4126+002	5.4549+001	7.2897+001	1.0000+000	-2.6655+001
4	0.0000	0.0000	0.0000	0.0000	1.0000+000
5	7.1808+001	-1.8043+001	2.4600+001	7.5649+001	1.8372+001

X11

1	-4.1740+000	-2.9379+000	-7.3442+000	1.5679+001	-3.2875+002
2	-9.1215+001	-7.7878+000	-8.2956+001	5.6668+003	9.9560+001
3	1.1124+000	-1.8082+000	8.0983+002	-3.2790+002	-2.1590+000
4	1.4685+000	-7.8290+001	-7.3502+002	2.7356+002	-2.0151+000
5	1.0000+001	0.0000	0.0000	0.0000	0.0000

T21

1	1.1256-005	3.4195-004	1.5421-003	2.0575-002	-1.1436-002	5
2	1.0000-000	-8.7559-002	3.8291-001	8.3546-001	1.2950-001	
3	-7.0057-004	4.7127-002	3.4120-001	3.3690-001	-2.5404-001	
4	-2.7229-003	1.7117-001	2.9409-001	2.8745-001	-2.4376-001	
5	-2.3231-002	2.2152-002	2.1541-001	3.6947-001	-2.3347-001	
6	5.4978-003	2.0678-002	-2.3187-001	-3.3584-001	6.4723-001	
7	7.1542-004	1.0441-002	-2.0087-001	5.0353-002	4.4113-002	
8	-1.0094-002	2.7773-002	-1.4729-001	3.7459-001	5.8052-001	
9	-1.3014-002	5.4553-002	-5.5331-002	3.3444-001	6.1524-001	
10	-5.1218-003	1.3301-002	-3.6531-002	4.3293-001	1.5415-001	
11	4.4690-002	2.4095-001	4.5901-002	3.4019-001	8.5751-001	
12	4.3527-004	2.7773-001	3.1182-001	-3.3752-001	-4.8456-001	
13	-7.0099-002	3.4617-001	-3.0592-002	-2.3246-002	5.4922-001	

T22

1	1.0000-000	5.5519-004	-3.2777-003	-9.7020-004	2.6512-003	7	-6.7297-003	2.0627-003	-1.3779-003	9	-1.3779-003	-1.5333-003
2	0.0000	1.0000-000	-1.4997-001	-2.0726-001	-7.5918-002	5	1.1600-001	1.6428-001	4.3126-002	8	4.3126-002	-1.7984-001
3	0.0000	-4.4933-005	1.8900-003	-9.1897-003	-1.1355-002		-1.8365-002	7.9377-003	-1.7149-002		-1.7149-002	1.2165-001
4	0.0000	-2.4221-004	-1.9094-003	-1.3089-002	-9.7382-003		-3.8365-002	-1.0231-001	-1.0455-001		-1.0455-001	1.9329-001
5	0.0000	-2.2646-004	1.7826-002	5.5652-002	4.1340-002		5.1336-001	-1.7644-001	1.3357-001		1.3357-001	5.0277-002
6	0.0000	-5.4553-005	2.7450-001	7.0273-001	-2.7390-002		7.2940-001	-3.5715-001	1.7446-001		1.7446-001	8.5674-002
7	0.0000	-7.1285-004	3.4366-002	8.5046-002	-4.5061-003		7.4570-002	-4.2986-002	1.8443-002		1.8443-002	8.2281-003
8	0.0000	5.1741-004	-3.4784-002	4.0055-002	6.3363-002		4.5994-001	-1.5555-001	9.4903-002		9.4903-002	5.8521-002
9	0.0000	-2.3249-002	1.0000-000	4.0907-001	1.5477-000		6.9244-001	-3.7890-001	1.6404-001		1.6404-001	1.3375-001
10	0.0000	-9.2514-003	3.7784-001	1.5720-001	5.7727-001		2.2861-001	-1.3773-001	5.5802-002		5.5802-002	4.2144-002
11	0.0000	-2.1043-003	1.5772-001	1.1258-001	8.4819-002		-4.8716-003	-1.9544-000	-8.0939-001		-8.0939-001	5.5739-001
12	0.0000	-5.5473-004	7.7618-004	7.5985-003	7.1189-003		-4.8593-001	1.9709-001	1.0000-000		1.0000-000	1.0000-000
13	0.0000	-2.0647-002	-9.0107-001	1.1229-000	-3.2925-001		-1.5990-000	-2.0723-000	-4.7761-001		-4.7761-001	9.9464-001

216

T22

1	-1.4213-002	5.3503-002	-4.5926-004	13
2	-1.4447-001	1.5026-001	-1.2957-001	
3	-4.0316-003	4.7219-002	5.4226-002	
4	-1.2743-003	2.6500-002	-1.5408-002	
5	-5.0244-002	4.2648-002	-2.1249-002	
6	1.4043-002	-8.5975-002	2.4233-002	
7	-4.3483-003	1.0000-000	2.4740-003	
8	1.2645-002	-6.7642-002	1.7791-002	
9	2.7249-002	-1.2870-001	0.7501-002	
10	1.0300-000	1.4330-001	1.5965-002	
11	1.9230-002	1.5133-001	1.0000-000	
12	-2.2791-003	2.6410-002	-3.7566-001	
13	-1.4575-002	-5.8601-002	4.3542-001	

LAMRD22

	1	2	3	4	5	6	7	8	9	10
1	-2.5000+001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
2	0.0000	-5.0120+002	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
3	0.0000	0.0000	-5.6303+001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4	0.0000	0.0000	0.0000	-4.7263+001	4.8166+000	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000	0.0000	-4.7263+001	0.0000	0.0000	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.0000	0.0000	0.0000	-4.2482+001	0.0000	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-2.0338+001	4.1714+000	0.0000	0.0000
8	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-2.0338+001	0.0000	0.0000
9	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-2.2035+001	0.0000
10	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-1.6169+001
11	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
12	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
13	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

LAMRD22

	11	12	13
1	0.0000	0.0000	0.0000
2	0.0000	0.0000	0.0000
3	0.0000	0.0000	0.0000
4	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.0000
8	0.0000	0.0000	0.0000
9	0.0000	0.0000	0.0000
10	0.0000	0.0000	0.0000
11	-1.0244+000	0.0000	0.0000
12	0.0000	-7.1572+001	0.0000
13	0.0000	0.0000	-1.9156+001

T12

	1	2	3	4	5	6	7	8	9	10
1	0.0000	-5.0945+001	-1.7383+002	3.8444+003	-3.9780+002	2.4997+002	-4.4033+002	1.2485+002	-1.1767+002	1.6828+002
2	0.0000	2.0314+001	-8.0224+003	-2.5838+002	-5.0141+003	-0.0967+002	-5.7435+002	1.6087+002	-1.2962+002	-4.2340+003
3	0.0000	-7.4225+001	4.6438+003	1.6815+002	2.3502+002	-1.9043+003	1.4264+001	2.4423+001	7.3679+002	-1.3112+001
4	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	3.0183+002	-1.12530+001	-2.2621+001	-1.6149+001	4.7466+003	1.1122+001	3.6043+001	2.9952+002	-3.1311+001

T12

	11	12	13
1	-1.3226-002	1.1056-001	9.7485-003
2	-5.8395-002	1.1684-001	1.5829-004
3	-8.5187-002	8.7689-002	-1.1967-001
4	0.0000	0.0000	0.0000
5	-1.5055-001	1.5644-001	-1.0424-001

H1

	1	2	3	4	5
1	1.4877-001	-5.6332-001	5.6446-001	-1.0176-001	1.4360-001
2	1.5026+000	1.0624-001	-8.6387-002	3.5320-002	-1.6562-002
3	0.0000	0.0000	0.0000	0.0000	0.0000
4	7.0803+000	2.2705+000	-1.8513+000	8.6165-001	-3.5535-001
5	6.4147+000	3.1073+001	2.3386+000	-2.0551-001	-7.0037+000

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H2

	1	2	3	4	5	6	7	8	9	10
1	0.0000	6.0615-001	4.9374-001	-4.3216-002	-2.7979-002	9.9535-002	2.8779-002	-3.3021-001	2.1031-002	2.1137-002
2	0.0000	-5.0105-001	0.5586-002	-3.7026-002	-5.4661-003	-5.3311-003	-5.4830-003	-5.7543-003	-5.5305-003	-5.2613-003
3	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.0000+000	0.0000	0.0000
4	0.0000	-1.0688-001	-2.0503+000	-7.9359-001	-1.1725-001	-1.1419-001	-1.1808-001	-1.2360-001	-1.1840-001	-1.1298-001
5	0.0000	1.3491-001	-1.6817+001	1.0059+000	1.4939-001	1.4561-001	1.5051-001	1.5774-001	1.5158-001	1.4424-001

H3

	11	12	13
1	3.7251-001	1.6029-001	2.2027-002
2	-5.7882-003	-8.2938-003	-5.4831-003
3	0.0000	0.0000	0.0000
4	-1.2432-001	-1.7718-001	-1.1803-001
5	1.5461-001	2.2621-001	1.5033-001

X12				
	1	2	3	5
1	5.3609-002	5.5520-003	2.3801-003	-8.0211-004
2	7.8410-000	1.7137+001	5.0707-001	-5.0938-001
3	2.4901+001	7.8089+000	-5.4541+000	-2.8062-001
4	1.3435+001	5.6384+000	-2.6385+000	-1.5240-001
5	-3.6575+001	-1.0319+001	5.4334+000	3.8954-001
6	-2.4429+001	7.8597+000	3.4121+000	2.7189-001
7	4.6330+000	3.7844+000	-3.1525-001	-8.8480-002
8	7.6633+000	4.1555+000	-7.4681-001	5.2408-002
9	-3.8132+000	-7.1008+000	9.4211-001	-4.6697-002
10	1.0732+001	1.1353+001	-4.0041-001	-3.7264-003
11	-0.7811-002	2.8319-001	3.0710-002	-1.7310-002
12	1.5541-001	1.4405-002	8.7598-003	-2.6643-003
13	1.5061+000	3.0577-002	4.0475-001	2.0068-002

T11 INVERSE				
	1	2	3	5
1	-0.0971-001	1.0210+000	8.1761-002	-5.4427-001
2	-1.8811-000	-4.4009-001	1.2402+000	-1.1428-001
3	1.9183+000	-3.2716+000	2.1333-001	1.1170-001
4	-0.0900-001	2.8244+000	1.5065-001	2.2237-001
5	0.0000	0.0000	0.0000	1.0000+000

FB				
	SVEAN	SUCOM	PTM	PT3
SVEAN	-0.2541+000	-1.4287+000	-1.4806+000	-1.8004-001
SUCOM	-1.0035-001	-3.4324+000	-7.7641-002	3.2176-001
PTM	4.4831+000	-6.8745+000	-6.1415+000	-4.6859-002
WFCOM	0.0000	0.0000	0.0000	-1.0000+001
PT3	7.7350+001	2.4905+002	-1.1303+001	7.0259+001

F100 LINEAR MODEL 0/0K 52 2/13/76

UNNORMALIZED EIGENSYSTEM.

EIGENVALUE		NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR		MAGNITUDE	PHASE (DEG)

(-1.8092+002i)+J(0.00000)	0.00000	1.00000	1.00000	1 (-9.04893-001)+J(0.00000))	-.9048926	.00000
				2 (-2.66467-001)+J(0.00000)			
				3 (-3.92242-003)+J(0.00000)			
				4 (0.00000)+J(0.00000)			
				5 (1.00000+000)+J(0.00000)			

(-4.0290+000)+J(3.04256+000)	5.06054+000	.79612	1.00000	1 (1.00000+000)+J(0.00000))	1.0000000	.00000
				2 (1.54443-001)+J(9.99823-002)			
				3 (3.53315-003)+J(-4.43996-003)			
				4 (0.00000)+J(0.00000)			
				5 (1.46654-002)+J(5.13314-003)			

(-2.7038+000)+J(0.00000)	0.00000	1.00000	1.00000	1 (1.00000+000)+J(0.00000))	1.0000000	.00000
				2 (9.49536-001)+J(0.00000)			
				3 (5.60922-003)+J(0.00000)			
				4 (0.00000)+J(0.00000)			
				5 (3.63472-002)+J(0.00000)			

(-1.0000+001)+J(0.00000)	0.00000	1.00000	1.00000	1 (-3.67535-001)+J(0.00000))	-.3675351	.00000
				2 (-2.42935-001)+J(0.00000)			
				3 (-1.44872-003)+J(0.00000)			
				4 (1.00000+000)+J(0.00000)			
				5 (8.55311-003)+J(0.00000)			

LAMBDA2 INVERSE

	2	3	4	5	6	7	8	9	10
1	-4.0000+000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
2	0.0000	-1.9952-003	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
3	0.0000	0.0000	-1.7761-002	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4	0.0000	0.0000	0.0000	-2.1341-003	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	0.0000	-2.0940-002	2.1341-003	0.0000	0.0000	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.0000	0.0000	-2.3539-002	0.0000	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.0000	0.0000	0.0000	-4.7184-002	0.0000	0.0000	0.0000
8	0.0000	0.0000	0.0000	0.0000	0.0000	9.6778-003	-4.7183-002	0.0000	0.0000
9	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-4.5382-002	0.0000
10	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-6.1846-002
11	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
12	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
13	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

F100 LINEAR MODEL O/K 52 2/13/76

LAMBDA2 INVERSE

	11	12	13
1	0.0000	0.0000	0.0000
2	0.0000	0.0000	0.0000
3	0.0000	0.0000	0.0000
4	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.0000
8	0.0000	0.0000	0.0000
9	0.0000	0.0000	0.0000
10	0.0000	0.0000	0.0000
11	-5.0553+001	0.0000	0.0000
12	0.0000	-1.3972+000	0.0000
13	0.0000	0.0000	-5.2202+002

GR

	MEMB	ANMTX	CTVV	RCVV	BLC
SNEAN	-1.2322+001	4.6841+001	2.4571+001	-9.2303+003	4.1756+000
SNECM	-1.3847+001	1.8557+001	5.3437+002	7.8178+003	6.9730+001
PTW	-1.7379+001	-5.0914+000	-2.0065+001	-8.6536+005	4.8896+000
WFCM	1.0000+001	0.0000	0.0000	0.0000	0.0000
PT3	-1.0357+001	-3.0300+001	-5.6315+000	2.9550+001	-2.7785+002

H*

	ENRX	MEAN	TT4	SMAF	SMHC
SNEAN	-1.3075+004	5.4016+002	-1.3406+003	-6.1284+003	2.9660+004
SNECM	-1.2780+001	-8.0551+001	1.7589+001	-1.9102+001	1.3906+000
PTW	3.6034+001	-2.0670+001	2.0738+001	-1.4634+001	1.3473+002
WFCM	1.0000+001	-2.3415+001	3.1971+001	-1.6358+001	7.9809+003
PT3	2.0115+001	3.5919+001	1.2702+001	-1.1449+001	-2.0978+002
PT15	-1.2784+001	-5.2452+001	-5.2217+002	5.5230+001	-3.9667+004
PT15	-1.0384+002	1.6666+001	-6.8925+003	5.7940+002	1.2983+003
TT25H	-1.3911+001	-5.0755+001	-5.4537+002	4.8324+001	-2.8169+002
TT25C	-1.1436+001	-4.2009+001	-1.1591+003	5.2899+001	-2.4719+002
TT3	-2.5816+001	1.2418+000	4.0409+002	2.5338+001	-3.9768+003
TT25H1	-8.0946+001	-9.0498+001	2.3382+001	7.2339+001	2.0710+002
TT25L0	-8.9528+002	-2.0737+001	4.6188+001	-4.0495+001	1.2667+002
TT4	-7.0023+001	3.3594+002	4.0064+001	5.8476+001	-1.1234+001

F100 LINEAR MODEL OXK S2 2/13/76

HD
 ENMX 6.804E-001 PT45 TT25H TT3
 ENAN 1.474E+000 -1.400E+000 9.364E-001 -1.453E-001 1.0095E+000
 TTU 1.391E-001 -5.075E-001 -1.287E-001 4.260E-002 -2.429E-002
 SNAF 7.379E+000 3.116E+000 -2.718E+000 1.017E+000 -5.202E-001
 SMHC 3.787E-001 3.401E+001 -5.443E-001 2.440E+000 -7.054E+000

D*
 ENMX 2.239E-001 ENAN 2.054E-002 TTU 9.714E-003 SHAF SMHC
 ENAN 2.237E-002 1.695E-001 1.887E-002 -2.144E-003 1.229E+000
 TTU 9.825E-002 1.010E-001 -1.203E-003 -1.416E-004 1.282E-001
 SNAF 1.005E-001 1.427E-001 -7.302E-003 3.714E-004 1.472E-001
 PT3 1.315E-001 7.030E-002 6.233E-004 -2.390E-003 -2.815E-001
 PT4 1.021E-001 2.752E-002 1.830E-002 3.577E-004 2.051E-001
 PT5 1.072E-001 2.530E-002 1.825E-002 -3.765E-003 5.352E-001
 TT25H -4.621E-003 2.732E-002 1.872E-002 -2.548E-004 2.760E-001
 TT25C -7.183E-002 6.075E-002 1.046E-002 -7.584E-004 3.011E-001
 TT3 -1.494E-001 1.751E-001 2.792E-002 -6.832E-003 9.112E-001
 TT4H 1.010E-001 1.708E-001 3.622E-002 -6.667E-004 5.752E-001
 TT4L 3.100E-001 3.235E-001 5.490E-003 -5.523E-004 2.354E-001
 TTU -2.753E-001 2.660E-001 5.140E-002 -1.156E-003 2.130E-001

DR
 ENMX 2.504E-002 ENAN 1.688E-001 CIVV 0.376E-002 HLC
 ENAN 1.233E-002 -0.215E-002 -1.027E-001 2.453E-004 1.185E+000
 TTU -4.621E-003 2.732E-002 1.872E-002 -2.548E-004 2.760E-001
 SNAF -2.651E-001 -3.943E-001 -3.277E-002 5.584E-003 -1.692E+000
 SMHC -1.473E+000 -1.244E+000 -2.594E-001 1.336E-001 -2.098E+000

	F	REDUCED MATRICES	0/0K	52	FIFTH ORDER
1.	-	1230+01	-	3310+00	1515+02
2.	-	426+01	-	5354+03	-
3.	-	108+01	-	3362+01	5159+02
4.	-	1418+01	-	7345+00	-
5.	-	0000	-	2115+01	6924+00
6.	-	201+01	-	6111+01	-
7.	-	1369+01	-	2507+03	0000
8.	-	2134+00	-	-1000+02	0000
9.	-	316+00	-	9684+02	1700+03
10.	-	9046+03	-	3289+01	-
11.	-	4002+02	-	REDUCED MATRICES	0/0K 52 FIFTH ORDER
12.	-	108+02	-	1369+00	0000
13.	-	6121+00	-	9307+02	3256+05
14.	-	3047+01	-	7179+03	8093+04
15.	-	3844+01	-	4811+02	3510+02
16.	-	1644+03	-	5519+02	0231+03
17.	-	6493+05	-	3213+00	0231+03
18.	-	4000+03	-	0000	0000
19.	-	4417+03	-	5339+02	6576+05
20.	-	3975+01	-	2301+04	REDUCED MATRICES
21.	-	4410+03	-	9935+00	0/0K 52 FIFTH ORDER
22.	-	314+02	-	2649+03	1250+00
23.	-	119+00	-	2200+02	3358+02
24.	-	4339+04	-	1129+00	1851+01
			-	4708+01	2809+00
			-	5066+01	2276+00
			-	4400+03	4882+03
			-	3186+02	4826+04
			-	0000+03	4862+04
			-	4417+03	7207+00
			-	REDUCED MATRICES	0/0K 52 FIFTH ORDER
			-	4417+03	3178+02
			-	2594+01	6186+01
			-	2146+02	1712+01
			-	2434+01	1793+01
			-	6209+01	2361+00
			-	4339+04	4779+03
			-	4417+03	7764+02
			-	3975+01	3700+00
			-	4410+03	3150+00

D.4 EXAMPLE OF TRANSFER FUNCTION DATA ON 16TH ORDER LINEAR MODEL

PLA = 52°
 ALTITUDE = 0
 MACH NUMBER = 0

ELEMENT	UNITS	VARIABLE	SYMBOL
Y(1)	rpm	Fan Speed	N ₁
Y(2)	rpm	Compressor Speed	N ₂
Y(3)	psia	Compressor Discharge Pressure	P _{T3}
Y(4)	psia	Interturbine Pressure	P _{T4.5}
Y(5)	psia	Augmentor Pressure	P _{T7M}
Y(6)	°R	Fan Inside Temperature	T _{T2.5H}
Y(7)	°R	Duct Temperature	T _{T2.5C}
Y(8)	°R	Compressor Discharge Temperature	T _{T3}
Y(9)	°R	Burner Exit Fast Temperature	T _{T4HI}
Y(10)	°R	Burner Exit Slow Temperature	T _{T4LO}
Y(11)	°R	Burner Exit Total Temperature	T _{T4}
Y(12)	°R	Fan Inlet Fast Temperature	T _{T45HI}
Y(13)	°R	Fan Inlet Slow Temperature	T _{T45LO}
Y(14)	°R	Fan Turbine Exit Temperature	T _{T5}
Y(15)	°R	Duct Exit Temperature	T _{T6C}
Y(16)	°R	Augmentor Temperature	T _{T7M}
U(1)	lbm/hr	Fuel Flow	WFMB
U(2)	ft ²	Nozzle Area	A _J
U(3)	deg	CIVV	CIVV

TRANSFER FUNCTION PROGRAM

8 100 ENGINE TRANSFER FUNCTIONS

 1 7800S OF THE TRANSFER FUNCTION 1

ZERES OF THE TRANSFER FUNCTION BETWEEN Y(1) AND U(1) =

```

1 (-2.48938+003) + J( 0.00000 )
2 ( 0.00000+000) + J( 0.00000 )
3 (-8.00141+001) + J( 2.85164+001)
4 (-8.00141+001) + J(-2.85164+001)
5 (-4.03529+001) + J( 0.00000 )
6 (-3.78744+001) + J( 0.00000 )
7 (-2.76457+001) + J( 0.00000 )
8 (-2.04135+001) + J( 0.00000 )
9 (-1.84309+001) + J( 1.87440+000)
10 (-1.84309+001) + J(-1.87440+000)
11 (-1.75667+001) + J( 0.00000 )
12 (-3.43711+000) + J( 2.85164+001)
13 (-3.43711+000) + J(-2.85164+001)
14 (-1.06753+000) + J( 0.00000 )
15 (-7.56530+001) + J( 0.00000 )
  
```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

225 7.40570+019 1.95190+020 6.81682+019 1.61763+019 2.32134+018 2.10085+017 1.22824+016
    4.63352+014 1.08092+013 1.33042+011 2.16460+008 -1.66321+007 -2.04068+005 -8.22113+002 -2.98400+001
  
```

RESIDUES OF THE TRANSFER FUNCTION

POLE LOCATION	RESIDUE AT THE POLE	COMBINED RESIDUES=MAG* $\cos(\omega_0 T + \phi)$	PHI(DEG)
-5.03241+002	1.94792+000	1.00950+001	-157.70925
-5.60011+001	3.73026+000	9.02390+001	86.08156
-1.80644+002	-2.15896+000	8.87548+001	-4.57179
(-4.72435+001) + J(0.81644+000)	(-4.67030+000) + J(1.91455+000)		
(-4.28220+001) + J(4.17172+000)	(-3.67475+000) + J(-4.50140+001)		
(-2.03379+001) + J(4.17172+000)	(-3.08330+002) + J(-4.50140+001)		
(-2.24350+001) + J(4.17172+000)	(-9.30195+002) + J(-4.50140+001)		
(-1.61601+001) + J(3.04256+000)	(-1.91896+001) + J(3.53724+002)		
(-4.02906+000) + J(3.04256+000)	(-4.92162+001) + J(3.53724+002)		
(-2.70385+000) + J(3.04256+000)	(-1.17058+000) + J(3.53724+002)		
(-1.94643+000) + J(3.04256+000)	(-1.78991+003) + J(3.53724+002)		
(-7.15716+001) + J(3.04256+000)	(-2.73074+002) + J(3.53724+002)		

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZEROS OF THE TRANSFER FUNCTION BETWEEN Y(2) AND U(1) =

```

1 (-3.2327+002) + 11.00000
2 (-8.4062+001) + 11.721855+001
3 (-8.6462+001) + 10.718855+001
4 (-3.3990+001) + 10.00000
5 (-5.1095+001) + 10.00000
6 (-4.177+001) + 10.00000
7 (-2.3525+001) + 10.00000
8 (-1.9124+001) + 10.00000
9 (-2.0438+001) + 10.00000
10 (-1.4692+001) + 10.00000
11 (-1.5565+001) + 10.00000
12 (-3.403+000) + 10.2891+000
13 (-3.403+000) + 10.2891+000
14 (-1.0730+000) + 10.00000
15 (-7.4700+001) + 10.00000

```

Coefficients of the numerator polynomial in ascending powers of s =

```

5.4500+019 1.0952+020 1.1188+020 9.1347+018 1.1754+018 9.0995+016 4.0689+015
8.1512+013 -1.0768+012 -1.0758+011 -2.80515+009 -3.81523+007 -2.89320+005 -1.16013+003 -1.7200+000

```

RESIDUES OF THE TRANSFER FUNCTION=

POLE LOCATION

RESIDUE AT THE POLE
MAGNITUDE

COMBINED RESIDUES=MAG*COSS(MD*PI+PHI)
PHI(DEG)

```

-5.0201+002 (-4.7635+001) + J( 0.8164+000) -8.7058+001
-5.6001+001 (-2.0339+001) + J( 4.1710+000) 2.5714+000
(-4.7635+001) + J( 0.8164+000) -7.0181+001
-4.2850+001 (-2.0339+001) + J( 4.1710+000) ( 2.0151+000) + J( 3.8255+000) 8.6504+000
-2.2350+001 (-4.0906+000) + J( 3.0426+000) (-7.9694+000) + J(-7.8618+001) 1.57361+000
-1.0540+001 (-4.0906+000) + J( 3.0426+000) (-1.3514+001) + J( 3.1443+002) 1.63590+001
-1.4601+001 (-4.0906+000) + J( 3.0426+000) -4.9767+004 6.0048+002
(-4.0906+000) + J( 3.0426+000) ( 6.0048+002) + J( 4.97055+002) 1.1406+000
-2.7355+000 (-4.0906+000) + J( 3.0426+000) 1.1406+000
-1.04603+000 (-4.0906+000) + J( 3.0426+000) 1.0447+002
-7.15710+001 (-4.0906+000) + J( 3.0426+000) 3.85663+002

```


TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZEROES OF THE TRANSFER FUNCTION BETWEEN Y(3) AND U(1) =

```

1  (5.35810+002) + J( 0.00000 )
2  (-8.46649+001) + J( 0.00000 )
3  (-5.17977+001) + J( 0.00000 )
4  (-4.23580+001) + J( 0.00000 )
5  (-3.19707+001) + J( 0.00000 )
6  (-2.25957+001) + J( 0.00000 )
7  (-2.10701+001) + J( 0.00000 )
8  (-1.88882+001) + J( 0.00000 )
9  (-1.44280+001) + J( 7.80849+000 )
10 (-1.44280+001) + J( 7.80849+000 )
11 (-6.69885+000) + J( 0.00000 )
12 (-4.01024+000) + J( 2.42856+000 )
13 (-4.01024+000) + J( 2.42856+000 )
14 (-1.97554+000) + J( 0.00000 )
15 (-1.40226+001) + J( 0.00000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

4.53265+018  1.21854+019  1.15461+019  5.54200+018  1.59220+018  2.95538+017  3.69706+016  3.20318+015
1.95160+014  8.38881+012  3.52037+011  5.16468+009  6.89009+007  5.48872+005  2.17979+003  2.54700+000

```

RESIDUES OF THE TRANSFER FUNCTION=

POLE LOCATION RESIDUE AT THE POLE COMBINED RESIDUES=MAG* $\cos(\phi D^*+PHI)$
MAGNITUDE PHI(DEG)

```

-5.01201+002  -2.65119-001  1.92177+000  177.40058  3.69706+016
-5.61011+001  7.26587-001  2.01027-001  -23.86276  3.20318+015
-1.80980+002  (-1.45458+001) + J( 9.49809+001)  1.92177+000  -98.70688  2.54700+000
(-4.72635+001) + J( 4.81644+000)  1.88723-002  2.01027-001  177.40058  2.17979+003
(-2.01339+001) + J( 4.17102+000)  (-1.00410+001) + J(-4.55855+003)  1.37905-002  -23.86276  2.95538+017
-2.20350+001  6.40430+003  1.24764+002  1.37905-002  2.17979+003
-1.91544+001  9.65140+002  6.30581+003  4.28745-002  3.69706+016
-1.41691+001  (-4.02900+000) + J( 3.04258+000)  5.83451-004  1.05359-003  3.20318+015
-2.70380+000  7.15716-001

```

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZERES OF THE TRANSFER FUNCTION BETWEEN Y(4) AND U(1) =

```

1 (1.0887+002) + J( 0.0000 )
2 (-1.0386+002) + J( 0.0000 )
3 (-5.1184+001) + J( 0.0000 )
4 (-4.0778+001) + J( 0.0000 )
5 (-5.2230+001) + J( 0.0000 )
6 (-2.3200+001) + J( 0.0000 )
7 (-1.4407+001) + J( 0.0000 )
8 (-1.6407+001) + J( 0.0000 )
9 (-2.0045+001) + J( 0.0000 )
10 (-1.8735+001) + J( 0.0000 )
11 (-7.3075+000) + J( 0.0000 )
12 (-4.1430+000) + J( 0.0000 )
13 (-4.1430+000) + J( 0.0000 )
14 (-1.9710+000) + J( 0.0000 )
15 (-7.4327+001) + J( 0.0000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

1.2200+018 3.2430+018 1.4214+018 3.9480+017 7.0234+016 8.3404+015 6.7781+014
1.8102+013 1.0807+012 1.8753+010 5.9220+006 1.3995+004 -1.9763+002 -1.1910+000

```

RESIDUES OF THE TRANSFER FUNCTION =

POLE LOCATION	RESIDUE AT THE POLE	COMBINED RESIDUES=MAG* $\cos(\phi)$ MAGNITUDE PHI(DEG)
-5.0120+002	-2.2913+000	
-5.6131+001	2.2710+001	
-1.8000+002	6.6742+001	
(-4.7235+001) + J(0.0000)	(3.8712+002) + J(1.8649+001)	3.8485+001 -78.39413
(-4.2030+001) + J(0.0000)	(-7.8815+002) + J(3.7351+003)	2.7989+002 -164.52047
(-2.0137+001) + J(0.0000)	(-1.3481+002) + J(2.4051+003)	
(-2.2050+001) + J(0.0000)	2.1526+003	
(-1.9154+001) + J(0.0000)	1.4073+002	
(-1.6101+001) + J(0.0000)	2.3003+003	
(-4.0200+000) + J(0.0000)	1.2345+002	
(-2.7030+000) + J(0.0000)	1.0970+004	
(-1.9443+000) + J(0.0000)	2.8010+004	
(-7.1516+001)		

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZEROES OF THE TRANSFER FUNCTION BETWEEN Y(S) AND U(1) =

```

1 (-1.2822+0.02i) + J( 3.11241+0.02i)
2 (-1.2822+0.02i) + J(-3.11241+0.02i)
3 (-5.64817+0.01i) + J( 0.00000 )
4 (-5.64817+0.01i) + J( 0.00000 )
5 (-4.21846+0.01i) + J( 0.00000 )
6 (-2.52341+0.01i) + J( 2.1366+0.01i)
7 (-2.52341+0.01i) + J(-2.1366+0.01i)
8 (-2.81049+0.01i) + J( 0.00000 )
9 (-2.8931+0.01i) + J( 0.00000 )
10 (-1.41174+0.01i) + J( 0.00000 )
11 (-1.89224+0.01i) + J( 0.00000 )
12 (-4.24624+0.00i) + J( 2.17951+0.00i)
13 (-4.24624+0.00i) + J(-2.17951+0.00i)
14 (-1.97007+0.00i) + J( 0.00000 )
15 (-7.32076+0.01i) + J( 0.00000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

4.58564+0.17 1.17470+0.18 1.00419+0.18 9.58087+0.16 1.37025+0.16 1.27062+0.15 7.94249+0.13
3.42673+0.12 1.03722+0.11 2.11856+0.09 2.90390+0.07 2.47130+0.05 1.16069+0.03 2.65758+0.00 4.83000+0.03

```

RESIDUES OF THE TRANSFER FUNCTION=

POLE LOCATION

RESIDUE AT THE POLE

COMBINED RESIDUES=MAG* $\cos(\mu\theta+T+PHI)$
MAGNITUDE PHI(DEG)

```

-5.07201+0.02 7.41126+0.03 2.30345+0.02 63.39317 2.30345+0.02 1.75970+0.02 -169.46257
-5.47311+0.01 -3.17095+0.03 -9.35241+0.03 J(-1.02976+0.02) J( 1.60905+0.03) 5.03612+0.03 46.91678
-1.80804+0.02 J( 5.15419+0.03) -8.83816+0.04 1.83803+0.03 8.97165+0.04 4.71860+0.03
-4.24624+0.01 + J( 4.81644+0.00) -8.65010+0.03 + J( 1.60905+0.03) 1.71999+0.03 + J(-1.83910+0.03)
(2.07379+0.01) + J( 4.17122+0.00) 1.83803+0.03 8.97165+0.04 4.71860+0.03 6.61454+0.03 3.43809+0.05 6.89461+0.05
-2.20350+0.01 1.83803+0.03 8.97165+0.04 4.71860+0.03 1.71999+0.03 + J( 1.04256+0.00)
-1.61601+0.01 -1.61544+0.01 1.61601+0.01 1.61544+0.01 1.61601+0.01 1.61544+0.01
-4.05966+0.00 + J( 1.04256+0.00) 1.61601+0.01 1.61544+0.01 1.61601+0.01 1.61544+0.01
-2.76356+0.00 1.61601+0.01 1.61544+0.01 1.61601+0.01 1.61544+0.01
-1.94443+0.00 1.61601+0.01 1.61544+0.01 1.61601+0.01 1.61544+0.01
-7.18716+0.01 1.61601+0.01 1.61544+0.01 1.61601+0.01 1.61544+0.01

```

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZERES OF THE TRANSFER FUNCTION BETWEEN Y(6) AND U(1) =

```

1  (5.11774+002) + I( 0.0000 )
2  (-1.65331+002) + I( 0.0000 )
3  (-6.05927+001) + I( 8.45758+000)
4  (-6.05927+001) + I( 8.45758+000)
5  (-9.72186+001) + I( 0.0000 )
6  (-1.81853+001) + I( 0.0000 )
7  (-3.11605+001) + I( 0.0000 )
8  (-2.02823+001) + I( 1.79661+000)
9  (-2.02823+001) + I( -1.79661+000)
10 (-2.14249+001) + I( 0.0000 )
11 (-1.87972+001) + I( 0.0000 )
12 (-3.78417+000) + I( 2.31683+000)
13 (-3.78417+000) + I( -2.31683+000)
14 (-1.96714+000) + I( 0.0000 )
15 (-7.48541+001) + I( 0.0000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

2.93834+018  7.22503+018  5.80955+018  2.16078+018  4.32874+017  4.67030+016  2.46531+015  1.22691+013
-6.3321+012  -4.31207+011  -1.41786+010  -2.75134+008  -3.19122+006  -2.08665+004  -6.60353+001  -6.95400+002

```

RESIDUES OF THE TRANSFER FUNCTION=

POLE LOCATION	RESIDUE AT THE POLE	COMBINED RESIDUES=MAG* $\cos(\text{WDT}+\text{PHI})$ MAGNITUDE PHI(DEG)
-5.01241+002	1.63722-003	
-5.61011+001	-3.16140-002	
-1.80944+002	-7.25510-003	
(-4.72635+001) + J(4.81644+000)	7.12739-002) + J(6.42372-002)	1.91900-001 -42.02745
(-2.03379+001) + J(4.17142+000)	-1.29415-001 -7.02963-003) + J(1.56335-003)	1.44027-002 -167.46181
-2.21340+001	-1.05208-002	
-1.91544+001	-9.99934-003	
-1.61601+001	-1.07458-001	
(-4.03946+001) + J(1.04256+000)	2.06000-002) + J(-8.88386-003)	4.48680-002 23.32832
-2.70346+000	5.48334-002	
-1.94623+000	5.17953-005	
-7.15716+001	9.13010-004	

F 100 ENGINE TRANSFER FUNCTIONS

ZEROS OF THE TRANSFER FUNCTION BETWEEN Y(7) AND U(1) =

1 (5.20345+002) + 1(0.0000)
 2 (-1.51312+002) + 1(0.0000)
 3 (-6.91528+001) + 1(0.0000)
 4 (5.15005+001) + 1(0.0000)
 5 (-2.50000+000) + 1(0.0000)
 6 (-4.45543+001) + 1(0.0000)
 7 (1.91807+001) + 1(5.22057+000)
 8 (-1.91807+001) + 1(-5.22057+000)
 9 (-2.00444+001) + 1(0.0000)
 10 (-1.02447+001) + 1(0.0000)
 11 (1.16317+001) + 1(0.0000)
 12 (-3.96716+000) + 1(2.18536+000)
 13 (-3.96716+000) + 1(-2.18536+000)
 14 (-1.96644+000) + 1(0.0000)
 15 (-7.37413+001) + 1(0.0000)

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

2.45555+018 6.03567+018 0.75881+018 1.68457+018 3.04585+017 2.53507+016 1.38567+014 -1.63362+014
 -1.40744+013 -8.04400+011 -2.44553+010 -4.65974+008 -5.44031+006 -3.62064+004 -1.17159+002 -1.23900+001

RESIDUES OF THE TRANSFER FUNCTION=

POLE LOCATION POLE RESIDUE AT THE POLE COMBINED RESIDUES=MAG* $\cos(\omega DT + \phi)$ MAGNITUDE PHI(DEG)

-5.01241+002 6.69454+003 3.17260+002 3.33380+001 -97.03283
 -5.63031+001 -2.59165+002 (-2.04092+002) + J(1.65436+001) 1.66811+001 .80722
 -1.81984+002 (-1.10132+001) (8.33072+002) + J(-1.17503+003) 4.38086+002 42.39920
 (-2.72615+001) + J(0.81644+000) -5.40005+002 (1.61750+002) + J(-1.47699+002) 1.33000+005 5.19058+004
 (-2.01379+001) + J(0.17142+000) 2.64239+003 -1.70482+001
 -2.21350+001 (-0.05966+000) + J(1.04254+000) 4.67020+002
 -1.91564+001 -2.70358+000
 -1.61691+001 -1.94423+000
 -7.15716+001 -7.15716+001

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZEROES OF THE TRANSFER FUNCTION BETWEEN Y(8) AND U(1) :

```

1  (-1.09193+003) + j( 0.00000 )
2  (-8.38607+001) + j( 0.00000 )
3  (-5.30252+002) + j( 0.00000 )
4  (-5.20702+001) + j( 0.00000 )
5  (-4.37601+001) + j( 0.00000 )
6  (-2.15300+001) + j( 0.00000 )
7  (-3.05203+001) + j( 0.00000 )
8  (-1.91200+001) + j( 0.00000 )
9  (-1.66333+001) + j( 0.00000 )
10 (-6.56203+000) + j( 9.82086+000 )
11 (-6.56203+000) + j( 9.82086+000 )
12 (-3.87506+000) + j( 2.08970+000 )
13 (-3.87506+000) + j( 2.08970+000 )
14 (-1.97300+000) + j( 0.00000 )
15 (-7.50512+001) + j( 0.00000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S :

```

7.33070+019  1.84470+019  6.88311+018  1.73290+018  2.79167+017  3.05460+016  2.33314+015
1.20060+014  4.54200+013  1.11598+011  1.59683+007  7.40197+004  1.20522+002  5.20000+002

```

RESIDUES OF THE TRANSFER FUNCTION:

POLE LOCATION

RESIDUE AT THE POLE

COMBINED RESIDUES=MAG* $\cos(\phi+1+\phi\phi)$
MAGNITUDE PHI(DEG)

```

-5.07201+002  1.08304+002
-5.51031+001  -5.57093+001
-1.50904+002  -4.10225+001
(-4.12635+001) + j( 4.81644+000 )  (-1.95138+001) + j( -1.26124+000 )  2.55250+000  81.20500
-4.20800+001  4.02055+001  (-1.06192+002) + j( 7.79949+001 )  1.56004+000  -90.78151
(-2.03379+001) + j( 4.17102+000 )  1.53010+001  5.20792+002  18.06970
-1.51540+001  7.35039+003
-1.61691+001  -8.35703+002
(-4.05900+000) + j( 3.04256+000 )  (-2.49055+002) + j( -8.13884+003 )  1.12020+001
-2.70300+000  1.04099+003
-1.90003+000  2.27521+003
-7.15716+001

```

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZERES OF THE TRANSFER FUNCTION BETWEEN Y(9) AND U(1) =

1	(-7.79999+003) + j(0.00000)
2	(-5.03307+002) + j(0.00000)
3	(-1.87575+002) + j(0.00000)
4	(-5.10458+001) + j(0.00000)
5	(-4.60129+001) + j(0.00000)
6	(-2.33607+001) + j(0.00000)
7	(-1.96762+001) + j(0.00000)
8	(-2.00822+001) + j(0.00000)
9	(-1.87302+001) + j(0.00000)
10	(-1.51052+001) + j(0.00000)
11	(-3.92041+000) + j(3.04118+000)
12	(-3.92041+000) + j(-3.04118+000)
13	(-1.98000+000) + j(0.00000)
14	(-6.66627+001) + j(0.00000)
15	(-1.84449+000) + j(0.00000)

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

1.57271+019	4.90570+019	5.70586+019	3.23936+019	1.04468+019	2.10593+018	2.70133+017	2.25635+016
1.24011+015	4.04500+015	1.03239+012	1.45321+010	1.13194+008	4.04412+005	4.83848+002	5.56200-002

RESIDUES OF THE TRANSFER FUNCTION=

POLE LOCATION	RESIDUE AT THE POLE	COMBINED RESIDUES=MAG*COSEC(WD*1+PHI) MAGNITUDE PHI(DEG)
-5.01201+002	4.15559-003	
-5.01031+001	-1.41082+001	
-1.84984+002	1.59001-001	
(-4.72535+001) + j(4.81664+000)	(-1.04624+001) + j(-1.80903+001)	4.17957+001 120.04274
(-2.03379+001) + j(3.17112+000)	(2.29842-001) + j(1.88004+000)	3.78807+000 -63.02995
-2.20335+001	3.24092-001	
-1.91544+001	-1.35090-002	
-1.41601+001	-2.20870-001	
(-4.02945+000) + j(3.06254+000)	(-2.60727-002) + j(1.45837-003)	5.22268-002 -176.79849
-2.70356+000	-1.65477-001	
-1.96603+000	-4.47160-004	
-7.115715-001	-5.04008-003	

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZEROES OF THE TRANSFER FUNCTION BETWEEN Y(10) AND U(1) =

```

1 (-7.797e2+003) + j( 0.00000 )
2 (-5.033e7+002) + j( 0.00000 )
3 (-1.87575+002) + j( 0.00000 )
4 (-5.100e6+001) + j( 0.00000 )
5 (-4.5012+001) + j( 0.00000 )
6 (-2.338e6+001) + j( 0.00000 )
7 (-2.0081e4+001) + j( 0.00000 )
8 (-1.946e3+001) + j( 0.00000 )
9 (-1.5107+001) + j( 0.00000 )
10 (-1.872e7+001) + j( 0.00000 )
11 (-3.02053+000) + j( 3.04131+000 )
12 (-3.02053+000) + j( 3.04131+000 )
13 (-4.09508+000) + j( 0.00000 )
14 (-1.9801+000) + j( 0.00000 )
15 (-1.844e9+000) + j( 0.00000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

1.70455+010 3.27751+012 2.53011+018 1.06985+018 2.79518+017 4.75963+016 5.39749+015 0.11938+014
2.11957+013 7.27739+011 1.62217+010 2.22530+008 1.70284+006 6.02225+003 7.17173+000 6.24200-004

```

RESIDUES OF THE TRANSFER FUNCTION=

POLE LOCATION	RESIDUE AT THE POLE	COMBINED RESIDUES=MAG* COS(WD*T+PHI)	PHI(DEG)
-5.012e1+002	6.10397-005		
-5.61011+001	-1.92730-001		
-1.809e4+002	2.29896-003		
(-4.72615+001) + j(0.17644+000)	r(-1.43290-001) + j(-2.41886-001)	5.62284-001	120.64201
-4.24820+001	4.59608-001		
(-2.01379+001) + j(0.17102+000)	(3.93210-003) + j(2.19331-002)	4.43687-002	-79.79057
-2.21350+001	3.83226-003		
-1.91544+001	-1.53809-004		
-1.61691+001	-2.65593-003		
(-4.039e6+000) + j(1.04256+000)	r(-1.00931-004) + j(2.53979-004)	5.46598-004	-111.67288
-2.713e6+000	2.76007-003		
-1.946e3+000	1.53844-005		
-7.15716-001	6.51362-003		

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZEROES OF THE TRANSFER FUNCTION BETWEEN Y(1) AND U(1) =

```

1 (-5.03158+002) + J( 0.00000 )
2 (-1.86814+002) + J( 0.00000 )
3 (-5.14549+001) + J( 0.00000 )
4 (-4.86810+001) + J( 1.01593+000 )
5 (-9.86410+001) + J( 1.01593+000 )
6 (-2.31877+001) + J( 0.00000 )
7 (-1.98529+001) + J( 7.05108+001 )
8 (-1.98529+001) + J( 7.05108+001 )
9 (-1.89002+001) + J( 0.00000 )
10 (-1.52355+001) + J( 0.00000 )
11 (-1.90888+000) + J( 3.03281+000 )
12 (-3.90888+000) + J( 3.03281+000 )
13 (-1.97759+000) + J( 0.00000 )
14 (-1.74768+000) + J( 0.00000 )
15 (-6.59325+001) + J( 0.00000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

1.85534+019 6.00720+019 7.02369+019 4.09576+019 1.36857+019 2.85857+018 3.86475+017 3.46628+016
2.09773+015 8.41661+013 2.38790+012 4.35532+010 4.98510+008 3.27171+006 1.03148+004 1.08800+001

```

RESIDUES OF THE TRANSFER FUNCTION=

POLE LOCATION	RESIDUE AT THE POLE	COMBINED RESIDUES=MAG* $\cos(\phi D+T+\phi H)$ MAGNITUDE $\phi H(\text{DEG})$
-5.01201+002	-4.59495+002	
-5.61031+001	2.33358+000	
-4.72613+001	-4.73714+001	
(-4.72613+001) + J(4.81644+000)	(1.44265+000) + J(-2.32473+000)	58.17767
-4.24820+001	6.50862+000	
(-2.01379+001) + J(4.17102+000)	(-2.42768+002) + J(1.30844+000)	-91.06293
-2.20350+001	2.05120+001	
-1.91544+001	-1.15575+002	
-1.61691+001	-1.82446+001	
(-4.05900+000) + J(3.04256+000)	(-3.05553+002) + J(9.03906+004)	-178.47963
-2.70386+000	-2.14738+001	
-1.94603+000	-7.03207+004	
-7.15710+001	-6.61205+003	

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZEROES OF THE TRANSFER FUNCTION BETWEEN Y(12) AND U(1) =

```

1 ( 2.04295+002) + J( 1.66883+003)
2 ( 2.04295+002) + J( 1.66883+003)
3 (-1.74515+002) + J( 0.00000 )
4 (-4.97093+001) + J( 0.00000 )
5 (-2.36774+001) + J( 0.00000 )
6 (-3.95559+001) + J( 0.00000 )
7 (-2.00730+001) + J( 1.67835+001)
8 (-2.00730+001) + J( 1.67835+001)
9 (-1.46339+001) + J( 0.00000 )
10 (-1.87304+001) + J( 0.00000 )
11 (-3.84015+001) + J( 3.07849+000)
12 (-3.84015+000) + J( 3.07849+000)
13 (-1.99904+000) + J( 0.00000 )
14 (-1.57094+000) + J( 0.00000 )
15 (-5.51328+001) + J( 0.00000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

1.22739+019 3.92705+019 0.06473+019 2.54465+019 8.23779+018 1.65717+018 2.13462+017 1.79385+016
9.92427+014 3.59524+013 8.29512+011 1.14479+010 8.24047+007 2.16133+005 -3.42773+000 7.95300+002

```

RESIDUES OF THE TRANSFER FUNCTIONS

POLE LOCATION	RESIDUE AT THE POLE	COMBINED RESIDUES=MAG* COS(WD*T+PHI) MAGNITUDE PHI(DEG)
-5.01211+002	1.32000+000	
-5.41011+001	-3.75459+001	
-1.20984+002	-2.80211+001	
(-0.72635+001) + J(0.81644+000)	(2.60530+001) + J(-2.39707+001)	7.08060+001 42.6159
(-0.20620+001) + J(0.17112+000)	(2.11469+001) + J(1.34607+000)	2.72522+000 -81.06344
-2.22350+001	2.27072+001	
-1.91544+001	-1.97466+002	
-1.41631+001	-2.67067+001	
(-0.02945+000) + J(0.04256+000)	(-1.53034+002) + J(-5.11412+003)	3.22706+002 161.52128
-2.76358+000	-1.22788+001	
-1.94693+000	-6.45735+004	
-7.15715+001	-5.35482+003	

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZERES OF THE TRANSFER FUNCTION BETWEEN Y(13) AND U(1) =

```

1 ( 2.1134E+002) + J( 1.4698E+003)
2 ( 2.1134E+002) + J( 1.4698E+003)
3 (-1.7463E+002) + J( 0.0000E+000)
4 (-4.0700E+001) + J( 0.0000E+000)
5 (-3.3554E+001) + J( 0.0000E+000)
6 (-2.3674E+001) + J( 0.0000E+000)
7 (-2.0072E+001) + J( 1.4797E+001)
8 (-2.0072E+001) + J( 1.4797E+001)
9 (-1.8734E+001) + J( 0.0000E+000)
10 (-1.4635E+001) + J( 0.0000E+000)
11 (-3.9400E+000) + J( 3.0789E+000)
12 (-3.9400E+000) + J( 3.0789E+000)
13 (-4.9874E+000) + J( 0.0000E+000)
14 (-1.8717E+000) + J( 0.0000E+000)
15 (-6.5137E+000) + J( 0.0000E+000)

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

1.1613E+018 3.0470E+018 1.8736E+018 1.4809E+018 5.3795E+017 9.7701E+016 1.1620E+016 9.1963E+014
4.2691E+013 1.7001E+012 3.8341E+010 5.1940E+008 3.6887E+006 9.5949E+003 -1.6264E+001 3.5190E+003

```

RESIDUES OF THE TRANSFER FUNCTION

POLE LOCATION

RESIDUE AT THE POLE

COMBINED RESIDUES=MAG* $\cos(\theta+T+\phi)$
MAGNITUDE ϕ (DEG)

```

-5.0120E+002 5.8489E-002 -1.5770E+000 2.9402E+000 43.04413
-5.5101E+001 -1.2288E-002 -1.2288E-002 2.9402E+000 43.04413
(-4.7243E+001) + J( 4.8164E+000) + J(-1.0034E+000) 1.0238E-001 -78.68103
-4.2482E+001 ( 1.0047E-002) + J( 5.0194E-002) 1.2576E-003 -147.79440
(-2.0337E+001) + J( 4.1717E+000) 1.2576E-003 -147.79440
-2.2035E+001 5.8574E-003 1.2576E-003 -147.79440
-1.6154E+001 -7.2455E-004 1.2576E-003 -147.79440
-1.6160E+001 -9.3246E-003 1.2576E-003 -147.79440
(-4.0290E+000) + J( 3.0425E+000) 1.2576E-003 -147.79440
-2.7139E+000 (-5.3245E+004) + J( 3.3512E-004) 1.2576E-003 -147.79440
-1.0403E+000 1.7640E-002 1.2576E-003 -147.79440
-7.1571E+001 -2.6309E-003 1.2576E-003 -147.79440
-7.1571E+001 -7.9207E-004 1.2576E-003 -147.79440

```

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZPACES OF THE TRANSFER FUNCTION BETWEEN Y(14) AND U(1) =

```

1 (-9.02158+003) + J( 0.00000 )
2 (-8.80828+002) + J( 0.00000 )
3 (-4.90116+001) + J( 0.00000 )
4 (-2.29289+002) + J( 0.00000 )
5 (-4.19514+001) + J( 0.00000 )
6 (-4.19514+001) + J( 0.00000 )
7 (-2.37887+001) + J( 0.00000 )
8 (-2.03440+001) + J( 0.00000 )
9 (-1.84233+001) + J( 0.00000 )
10 (-1.42000+001) + J( 0.00000 )
11 (-2.93246+000) + J( 0.00000 )
12 (-2.93246+000) + J( 0.00000 )
13 (-1.98537+000) + J( 0.00000 )
14 (-2.33652+001) + J( 0.00000 )
15 (-1.85708+000) + J( 0.00000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

1.06406+019 3.42052+019 3.86058+019 2.13998+019 6.68398+018 1.28646+018 1.56519+017 1.28529+016
6.29400+014 2.04332+013 0.33188+011 5.47927+009 3.73938+007 1.08380+005 8.98236+001 8.67500+003

```

RESIDUES OF THE TRANSFER FUNCTION=

POLE LOCATION

```

-5.01201+002 1.12471+001
-5.61031+001 -5.56048+000
-1.20984+002 4.18400+001
(-4.72615+001) + J( 0.81644+000) ( 4.49290+001) + J(-2.88303+000) 5.83566+000 81.14231
-4.24822+001 -1.17947+001 ( 3.46317+000) + J(-2.60952+001) 6.94598+000 4.30912
(-2.01379+001) + J( 0.17142+000) -1.05319+000 -3.91122+001
-2.02035+001 -1.04425+000 -1.56505+002) + J(-3.05860+002) 6.88982+002 117.39441
-1.91544+001 (-1.56505+002) + J(-3.05860+002)
-1.61601+001 -1.31213+001 -4.28373+004
(-4.02900+000) + J( 3.04254+000)
-2.71385+000
-1.94503+000
-7.15716+001

```

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZEROES OF THE TRANSFER FUNCTION BETWEEN Y(15) AND U(1) =

```

1 (-5.8359+002) + JC 0.0000
2 (-1.28701+002) + JC 0.0000
3 (-4.4027+002) + JC 0.0000
4 (-5.9802+001) + JC 0.0000
5 (-5.3765+001) + JC 0.0000
6 (-2.5835+001) + JC 0.0000
7 (-0.9016+001) + JC 0.0000
8 (-1.9233+001) + JC 0.0025+000
9 (-1.9233+001) + JC 0.0025+000
10 (-1.9257+001) + JC 0.0000
11 (-1.1863+001) + JC 0.0000
12 (-3.97743+000) + JC 2.19282+000
13 (-3.97743+000) + JC -2.19282+000
14 (-1.9682+000) + JC 0.0000
15 (-7.3859+001) + JC 0.0000

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

2.51510+018 0.05500+018 4.57401+018 1.50300+018 2.39874+017 1.47009+016 -5.09275+014 -1.38448+014
-9.72135+012 -3.69404+011 -8.43746+009 -1.16871+008 -9.47011+005 -4.11686+003 -8.19056+000 -5.82000+003

```

RESIDUES OF THE TRANSFER FUNCTION=

POLE LOCATION	RESIDUE AT THE POLE	COMBINED RESIDUES=MAG* $\cos(\omega D+T+PHI)$	PHI(DEG)
-5.01201+002	1.40291+004	2.06132+001	75.05080
-5.01071+001	-1.29596+002	8.04637+001	92.32858
-1.80940+002	0.06828+003		
(-4.72635+001) + JC (0.81640+000)	(2.65871+002) + JC(-9.95775+002)		
(-2.0620+001)	9.77771+002		
(-2.01379+001) + JC (0.17102+000)	(-1.63463+002) + JC(-4.01986+001)		
-2.20350+001	0.15202+001		
-1.01544+001	0.93405+002		
-1.61501+001	-8.67504+001		
(-4.02966+000) + JC (3.06426+000)	(1.59090+002) + JC(-2.16994+002)	5.38608+002	53.68354
-2.70348+000	5.50760+002		
-1.94643+000	2.22187+005		
-7.15716+001	5.70288+004		

TRANSFER FUNCTION PROGRAM

R 100 ENGINE TRANSFER FUNCTION

ZEROES OF THE TRANSFER FUNCTION BETWEEN Y(14) AND U(1) =

```

1  (-0.3522E+000) + (0.0000E+000)
2  (-1.0527E+000) + (0.0535E+001)
3  (-1.4744E+000) + (0.0535E+001)
4  (-1.0527E+000) + (0.0000E+000)
5  (-1.1144E+000) + (0.0000E+000)
6  (-1.1144E+000) + (0.0000E+000)
7  (-1.1144E+000) + (0.0000E+000)
8  (-1.1144E+000) + (0.0000E+000)
9  (-1.1144E+000) + (0.0000E+000)
10 (-1.1144E+000) + (0.0000E+000)
11 (-1.1144E+000) + (0.0000E+000)
12 (-1.1144E+000) + (0.0000E+000)
13 (-1.1144E+000) + (0.0000E+000)
14 (-1.1144E+000) + (0.0000E+000)
15 (-1.1144E+000) + (0.0000E+000)

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

R 0.0000E+000 2.0000E+000 1.2000E+000 3.3730E+018
I 0.0000E+000 2.0000E+000 1.2000E+000 3.3730E+018

```

```

5.7653E+017 6.1477E+016 3.95733E+015
-2.8149E+005 -1.0032E+003 -8.4800E+001

```

RESIDUES OF THE TRANSFER FUNCTION

POLE LOCATION

```

-5.0201E+002
-5.0201E+002
-1.5000E+002
(-0.1565E+001) + (0.0000E+000)
(-0.1565E+001) + (0.0000E+000)
(-0.1565E+001) + (0.0000E+000)
(-0.1565E+001) + (0.0000E+000)
(-0.1565E+001) + (0.0000E+000)
(-0.1565E+001) + (0.0000E+000)
(-0.1565E+001) + (0.0000E+000)
(-0.1565E+001) + (0.0000E+000)
(-0.1565E+001) + (0.0000E+000)
(-0.1565E+001) + (0.0000E+000)
(-0.1565E+001) + (0.0000E+000)
(-0.1565E+001) + (0.0000E+000)
(-0.1565E+001) + (0.0000E+000)
(-0.1565E+001) + (0.0000E+000)

```

RESIDUE AT THE POLE

```

8.2110E+001
2.0126E+001
-1.2000E+000
(-1.2000E+001) + (0.0000E+000)
(-1.2000E+001) + (0.0000E+000)
(-1.2000E+001) + (0.0000E+000)
(-1.2000E+001) + (0.0000E+000)
(-1.2000E+001) + (0.0000E+000)
(-1.2000E+001) + (0.0000E+000)
(-1.2000E+001) + (0.0000E+000)
(-1.2000E+001) + (0.0000E+000)
(-1.2000E+001) + (0.0000E+000)
(-1.2000E+001) + (0.0000E+000)
(-1.2000E+001) + (0.0000E+000)
(-1.2000E+001) + (0.0000E+000)
(-1.2000E+001) + (0.0000E+000)

```

COMBINED RESIDUES = $\Delta G \cdot \cos(\Delta \theta + \phi)$
MAGNITUDE ϕ (DEG)

```

3.6890E+001 134.15228
6.4094E+000 17.90449
7.6022E+002 108.46645

```

TRANSFER FUNCTION PROGRAM

R 100 ENGINE TRANSFER FUNCTIONS

ZEROS OF THE TRANSFER FUNCTION BETWEEN Y(1) AND U(2) =

```

1 ( 2.0734+003) + J( 0.0000 )
2 (-8.8847+001) + J( 6.4762+001)
3 (-8.8847+001) + J( 6.4762+001)
4 (-9.2344+001) + J( 3.5718+001)
5 (-9.2344+001) + J( 3.5718+001)
6 (-5.0065+001) + J( 0.0000 )
7 (-2.4865+001) + J( 0.0000 )
8 (-3.8127+001) + J( 0.0000 )
9 (-1.6055+001) + J( 2.8649+000)
10 (-1.0555+001) + J( 2.8649+000)
11 (-1.9997+001) + J( 0.0000 )
12 (-1.9142+001) + J( 0.0000 )
13 (-2.5025+000) + J( 0.0000 )
14 (-1.9571+000) + J( 0.0000 )
15 (-7.1963+001) + J( 0.0000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

1.4649+023 4.2250+023 3.7895+024 1.5014+023 2.9885+022 3.4676+021 2.5619+020 1.2658+019
4.2801+017 1.0055+014 1.6388+014 1.7901+012 1.2717+010 5.2524+007 9.0238+004 -5.7270+001

```

RESIDUES OF THE TRANSFER FUNCTION=

POLE LOCATION

RESIDUE AT THE POLE

COMBINED RESIDUES=MAG* $\cos(\phi T + \phi I)$
MAGNITUDE PHI(DEG)

```

-5.0120+002 -3.1051+002
-5.0120+002 -3.9621+002
-1.2094+002 1.5041+002
(-4.7263+001) + J( 4.8164+000) ( 6.3143+002) + J( -2.8108+002) 1.3830+003 23.98270
-4.2882+001 -5.7345+002 -1.6765+002 + J( 3.3786+002) 7.5400+002 -116.30330
(-2.0337+001) + J( 0.1717+000) 2.4194+002 8.7342+001 5.5275+002
-2.2350+001 -1.6154+001 -1.3022+003
-1.6154+001 -1.6154+001 ( 3.2626+002) + J( -5.2551+003) 1.2487+004 87.00463
(-4.0396+000) + J( 3.0425+000) -1.0803+001 5.2902+000
-2.7638+000 -1.0803+001
-7.1571+001 -7.1571+001

```


TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZEROES OF THE TRANSFER FUNCTION BETWEEN Y(2) AND U(2) =

```

1 (-2.93342+002) + J( 0.0000 )
2 (-1.04503+002) + J( 0.70668+001)
3 (-1.04503+002) + J(-0.70668+001)
4 (-5.11281+001) + J( 0.0000 )
5 (-0.86634+001) + J( 0.0000 )
6 ( 7.33253+000) + J( 3.00718+001)
7 ( 7.33253+000) + J(-3.00718+001)
8 (-2.74952+001) + J( 0.0000 )
9 (-2.21013+001) + J( 0.0000 )
10 (-1.01541+001) + J( 0.0000 )
11 (-1.76044+001) + J( 0.0000 )
12 (-1.13449+001) + J( 0.0000 )
13 (-2.01971+000) + J( 0.0000 )
14 ( 1.24909+000) + J( 0.0000 )
15 (-0.74934+001) + J( 0.0000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

-8.70824+021 -1.30909+022 3.64482+021 7.03868+021 1.96948+021 2.55532+020 1.93721+019 9.79286+017
-1.73020+016 1.17329+015 3.09751+014 5.47238+011 6.57328+009 4.71376+007 1.79219+005 2.61700+002

```

RESIDUES OF THE TRANSFER FUNCTION=

POLE LOCATION	RESIDUE AT THE POLE	COMBINED RESIDUES=MAG*COS(MD*TI+PHI)	PHI(DEG)
-5.01201+002	1.39074+002	1.18517+003	119.39145
-5.61001+001	-2.69555+002	1.31484+003	-114.65342
-1.80904+002	4.93711+001	2.30165+003	54.15420
(-4.72515+001) + J(0.81644+000)	(-2.90225+002) + J(-5.16312+002)		
(-2.03379+001) + J(4.17102+000)	(-2.74229+002) + J(5.97496+002)		
-2.26350+001	1.24570+003		
-1.91524+001	3.56531+002		
-1.61001+001	1.86711+002		
(-4.02906+000) + J(1.04256+000)	(-6.73928+002) + J(-9.32852+002)		
-2.70385+000	-1.23432+003		
-1.94603+000	-6.42975+001		
-7.15716+001	7.41546+000		

TRANSFER FUNCTION PROGRAM

F 100 EIGHTY TRANSFER FUNCTIONS

ZEROS OF THE TRANSFER FUNCTION BETWEEN Y(3) AND U(2) =

```
(-5.56272+002) + J( 0.00000 )
(-1.14147+002) + J( 0.00000 )
(-5.28000+001) + J( 0.00000 )
(-3.65884+001) + J( 1.46672+001 )
(-3.65884+001) + J( 1.46672+001 )
(-4.23744+001) + J( 0.00000 )
(-2.36018+001) + J( 4.5321+000 )
(-2.36018+001) + J( 4.5321+000 )
(-2.14372+001) + J( 0.00000 )
(-1.91507+001) + J( 0.00000 )
(-7.43329+000) + J( 0.00000 )
(-1.80689+000) + J( 0.00000 )
(-2.06404+000) + J( 0.00000 )
(-6.61174+001) + J( 1.8903+001 )
(-6.61174+001) + J( 1.8903+001 )
```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```
2.08795+020 6.55835+020 5.95476+020 -2.12192+018 -1.66998+020 -5.96734+019 -9.60024+018 -8.93163+017
-5.29703+016 -2.00311+015 -5.59205+014 -1.00082+012 -1.15632+010 -7.95323+007 -2.73472+005 -2.92300+002
```

RESIDUES OF THE TRANSFER FUNCTIONS

POLE LOCATION RESIDUE AT THE POLE COMBINED RESIDUES=MAG* $\cos(\omega_0 T + \phi)$
MAGNITUDE PHI(DEG)

```
-5.01201+002 4.22417+001 2.63294+002 82.98507
-5.63031+001 -7.71953+001 1.67970+002 -24.98433
(-4.73635+001) + J( 4.81644+000 ) J(-1.30662+002) 1.94027+002 67.71366
(-2.03379+001) + J( 4.17142+000 ) J( 7.61258+001 ) 1.67970+002
-2.23350+001 J( 4.17142+000 ) J( 7.61258+001 ) 1.67970+002
-1.91544+001 -4.70125+001 -2.78010+002 1.94027+002 67.71366
(-4.03906+000) + J( 3.04256+000 ) J( 3.67910+001 ) + J(-8.97666+001) 1.94027+002 67.71366
-2.73472+000 -3.55214+000 2.02077+001
```

F 100 ENGINE TRANSFER FUNCTIONS

ZERES OF THE TRANSFER FUNCTION BETWEEN Y(4) AND U(2) =

```

1 ( 1.3551E+002) + J( 0.0000 )
2 (-1.4402E+002) + J( 0.0000 )
3 (-5.2475E+001) + J( 0.0000 )
4 (-4.4400E+001) + J( 0.0000 )
5 (-3.0378E+001) + J( 1.2779E+001)
6 (-3.0378E+001) + J( -1.2779E+001)
7 (-2.1860E+001) + J( 5.1343E+000)
8 (-2.1860E+001) + J( -5.1343E+000)
9 (-2.1753E+001) + J( 0.0000 )
10 (-1.9150E+001) + J( 0.0000 )
11 (-1.0465E+001) + J( 0.0000 )
12 (-1.2792E+000) + J( 0.0000 )
13 (-2.0489E+000) + J( 0.0000 )
14 (-8.8101E-001) + J( 9.8911E-002)
15 (-8.8101E-001) + J( -9.8911E-002)
    
```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

A.3251E+019 1.9712E+20 A.3814E+019 -7.6047E+019 -2.0673E+019 -2.8693E+018 -2.3794E+017
-1.2508E+016 -4.3487E+014 -0.6143E+011 -6.8029E+008 3.6931E+006 6.7780E+004 2.4100E+002
    
```

RESIDUES OF THE TRANSFER FUNCTION =

POLE LOCATION	RESIDUE AT THE POLE	COMBINED RESIDUES=MAG* COS(WO*T+PHI) MAGNITUDE PHI(DEG)
-5.0120E+002	3.6565E+002	
-5.6101E+001	-2.4128E+001	
-1.8094E+002	-6.0597E+001	
(-4.7203E+001) + J(4.8164E+000)	(-6.0604E+001) + J(-2.5656E+001)	5.2727E+001 103.29782
(-4.2820E+001) + J(4.1717E+000)	(-6.0604E+001) + J(1.4061E+000)	2.3386E+001 -6.90651
(-2.0337E+001) + J(4.1717E+000)	(-6.3174E+000)	
-2.2350E+001	-6.1448E-002	
-1.9154E+001	-4.1899E+001	
(-4.0366E+000) + J(3.0425E+000)	(-5.0270E+001) + J(-3.2426E+001)	6.4860E+001 90.89448
-2.7380E+000	-1.3649E+001	
-1.9454E+000	-4.4789E-001	
-7.1571E-001	5.3810E-002	

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZERES OF THE TRANSFER FUNCTION BETWEEN Y(5) AND U(2) =

```

1 (-4.92042+002) + J( 0.00000 )
2 (-1.62741+002) + J( 0.00000 )
3 (-5.65719+001) + J( 0.00000 )
4 (-4.69201+001) + J( 3.75201+000 )
5 (-4.69201+001) + J( 3.75201+000 )
6 (-4.25862+001) + J( 0.00000 )
7 (-2.17021+001) + J( 4.57815+000 )
8 (-2.17021+001) + J( 4.57815+000 )
9 (-2.11200+001) + J( 0.00000 )
10 (-1.91519+001) + J( 0.00000 )
11 (-1.43175+001) + J( 0.00000 )
12 (-2.50425+000) + J( 1.09746+000 )
13 (-2.30425+000) + J( 1.09746+000 )
14 (-1.99355+000) + J( 0.00000 )
15 (-7.13445+001) + J( 0.00000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

-8.37230+020 -2.47769+021 -2.65102+021 -1.42409+021 -4.29153+020 -7.57469+019 -8.36568+018 -6.08275+017
-3.00183+016 -1.01855+015 -3.36694+014 -3.69165+011 -3.69483+009 -2.16021+007 -6.42764+004 -6.60500+001

```

RESIDUES OF THE TRANSFER FUNCTION

POLE LOCATION	RESIDUE AT THE POLE	COMBINED RESIDUES=MAG* $\cos(\phi D+T+\phi H)$ MAGNITUDE PHI(DEG)
-5.01201+002	-1.21328+000	
-5.51031+001	3.76894+001	
-1.61994+002	6.32845+001	
(-4.72635+001) + J(4.81644+000)	(-6.64741+001) + J(1.43109+000)	3.15588+000 -114.91487
(-4.72635+001) + J(4.81644+000)	(-6.64741+001) + J(1.43109+000)	3.15588+000 -114.91487
(-2.01379+001) + J(4.17172+000)	(-2.01379+001) + J(4.17172+000)	1.47033+001 -11.84745
(-2.01379+001) + J(4.17172+000)	(-2.01379+001) + J(4.17172+000)	1.47033+001 -11.84745
-1.71544+001	-3.36126+002	
-1.61991+001	-1.35620+001	
(-4.02906+000) + J(3.06426+000)	(-2.65113+001) + J(-2.34785+001)	7.08561+001 138.49320
(-4.02906+000) + J(3.06426+000)	(-2.65113+001) + J(-2.34785+001)	7.08561+001 138.49320
-2.76356+000	-7.30333+000	
-1.94643+000	-2.21417+001	
-7.15716+001	1.32500+002	

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZEROES OF THE TRANSFER FUNCTION BETWEEN Y(6) AND U(2) =

```

1 (-5.05004+002) + J( 0.00000 )
2 (-1.78016+002) + J( 0.00000 )
3 ( 7.64703+001) + J( 0.00000 )
4 (-5.19605+001) + J( 2.07622+000)
5 (-5.10005+001) + J( 2.07622+000)
6 (-5.14806+001) + J( 0.00000 )
7 (-3.80613+001) + J( 0.00000 )
8 (-2.02672+001) + J( 4.03575+000)
9 (-2.02672+001) + J( 4.03575+000)
10 (-2.12970+001) + J( 0.00000 )
11 (-1.91507+001) + J( 0.00000 )
12 ( 0.14363+000) + J( 0.00000 )
13 (-2.22443+000) + J( 0.00000 )
14 (-1.95620+000) + J( 0.00000 )
15 (-7.20826+001) + J( 0.00000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

1.57040+021      8.81710+021      4.52182+021      1.68104+021      4.32659+019      -3.12399+019      -4.75498+018      -3.28158+017
-1.24657+014      -2.73621+014      -5.09097+012      1.77789+010      6.80383+008      6.44200+006      2.40147+004      2.72400+001

```

RESIDUES OF THE TRANSFER FUNCTION=

POLE LOCATION	RESIDUE AT THE POLE	COMBINED RESIDUES=MAG* COS(WD*7+PHI) MAGNITUDE PHI(DEG)
-5.01241+002	-2.60883+001	
-5.61031+001	3.35000+000	
-1.80984+002	5.06119+001	
(-4.72635+001) + J(4.81644+000)	(-1.00206+001) + J(-8.50876+000)	2.62916+001 134.66449
(-4.28820+001) + J(4.17102+000)	(2.02157+001) + J(1.02901+000)	1.20344+001 -9.84666
(-2.03379+001) + J(4.17102+000)	(3.76191+001) + J(3.76191+001)	
-2.23350+001	3.76191+001	
-1.91564+001	3.76191+001	
(-4.09206+000) + J(3.04256+000)	(-1.32018+002) + J(-2.86286+002)	6.31275+002 114.90475
-2.73185+000	-6.02554+001	
-1.94503+000	-3.15230+001	
-7.15716+001	1.75462+001	

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZEROES OF THE TRANSFER FUNCTION BETWEEN Y(7) AND U(2) =

```

1 (-5.07643+002) + J( 0.00000 )
2 (-1.78012+002) + J( 0.00000 )
3 (-6.24700+001) + J( 0.00000 )
4 (-5.72946+001) + J( 0.00000 )
5 (-4.77229+001) + J( 0.00000 )
6 (-9.84143+001) + J( 0.00000 )
7 (-3.96946+001) + J( 0.00000 )
8 (-2.04133+001) + J( 5.07493+000 )
9 (-2.04133+001) + J( -5.07493+000 )
10 (-2.00108+001) + J( 0.00000 )
11 (-1.91581+001) + J( 0.00000 )
12 (-2.02901+000) + J( 0.00000 )
13 (-1.94290+000) + J( 0.00000 )
14 (-4.15734+002) + J( 0.00000 )
15 (-7.33328+001) + J( 0.00000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

-4.40288+019 -1.15931+021 -2.85756+021 -2.43511+021 -9.02308+020 -1.54309+020 -1.44251+019 -7.97887+017
-2.27173+016 -0.61089+014 -1.51926+012 1.03334+011 2.11724+009 1.76191+007 6.24371+004 6.92300+001

```

RESIDUES OF THE TRANSFER FUNCTION=

POLE LOCATION

RESIDUE AT THE POLE

COMBINED RESIDUES=MAG* $\cos(\theta_D+T+\phi_H)$
MAGNITUDE PHI(DEG)

```

-5.07643+002 -1.06779+000
-5.63031+001 -3.37069+000
-1.80944+002 1.80794+000
(-4.72635+001) + J( 0.81644+000 ) ( 2.12570+000 ) + J( -2.27385+001 ) 4.56752+001 84.65912
-4.24820+001 1.71770+001 1.71770+001 1.39381+002 158.42233
(-2.03379+001) + J( 0.17102+000 ) (-6.48064+001) + J( -2.56295+001 ) 1.39381+002
-2.20350+001 1.88011+002
-1.91544+001 -1.07151+001
-1.41691+001 4.91450+002
(-4.02906+000) + J( 3.04254+000 ) (-2.13089+002) + J( -2.21781+002 ) 6.16369+002 133.97562
-2.70736+000 -5.35507+001
-1.94643+000 -8.15293+002
-7.15716+001 9.99248+002

```


TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZEROES OF THE TRANSFER FUNCTION BETWEEN Y(8) AND U(2) =

```

1  (-0.77879+002) + J( 0.00000 )
2  (-2.76717+002) + J( 0.00000 )
3  (-7.45023+001) + J( 0.00000 )
4  (-5.27175+001) + J( 0.00000 )
5  (-3.56482+001) + J( 0.00000 )
6  (-4.40272+001) + J( 0.00000 )
7  (-3.87020+001) + J( 2.16795+001 )
8  (-3.80200+000) + J( 2.16795+001 )
9  (-1.08299+001) + J( 0.00000 )
10 (-2.03348+001) + J( 0.00000 )
11 (-1.78955+001) + J( 0.00000 )
12 (-1.91535+001) + J( 0.00000 )
13 (-2.10330+000) + J( 0.00000 )
14 (-1.43200+000) + J( 0.00000 )
15 (-7.31059+001) + J( 0.00000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

3.62107+021  9.57140+021  7.99725+021  2.60920+021  2.88843+020  6.04123+018  -1.48471+018  -1.79156+017
-1.15124+016  -4.90007+014  -1.00000+013  -2.58690+011  -2.89199+009  -1.77395+007  -5.00051+004  -4.90200+001

```

RESIDUES OF THE TRANSFER FUNCTION =

POLE LOCATION	RESIDUE AT THE POLE	COMBINED RESIDUES=MAG* $\cos(\theta+7+PMI)$ MAGNITUDE PHI(DEG)
-5.01201+002	-1.72403+000	
-5.61011+001	5.92101+001	
-1.80984+002	2.90359+001	
(-0.72875+001) + J(0.81644+000)	(-2.16215+001) + J(1.73513+002)	3.49709+002 -97.10303
-4.24620+001	-6.27075+001	
(-2.03339+001) + J(0.17102+000)	(-2.56002+002) + J(-5.99201+002)	1.30351+003 66.83361
-2.24350+001	-0.04008+002	
-1.81544+001	-2.77253+001	
-1.61501+001	2.40725+002	
(-0.02905+001) + J(3.04254+000)	(-1.24122+002) + J(-3.47690+002)	7.38361+002 109.64612
-2.70386+000	-1.24401+002	
-1.94603+000	-6.36598+000	
-7.15716+001	0.37208+001	

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZEROES OF THE TRANSFER FUNCTION BETWEEN Y(1) AND U(3) =

```

1 (-5.07989+002) + J( 0.0000 )
2 (-7.8504+001) + J( 0.0000 )
3 (-4.93103+001) + J( 4.38106+001)
4 (-4.93103+001) + J( 4.38106+001)
5 (-4.93103+001) + J( 0.0000 )
6 (-3.77785+001) + J( 0.0000 )
7 (-2.64223+001) + J( 0.0000 )
8 (-1.99733+001) + J( 8.12111+001)
9 (-1.99733+001) + J( 8.12111+001)
10 (-1.70799+001) + J( 3.09742+000)
11 (-1.70799+001) + J( 3.09742+000)
12 (-1.24412+001) + J( 0.0000 )
13 (-2.37893+000) + J( 0.0000 )
14 (-7.26740+001) + J( 0.0000 )
15 (-1.95784+000) + J( 0.0000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

-2.9905+021 -8.14224+021 -7.56928+021 -3.29305+021 -7.65797+020 -1.07567+020 -9.85378+018 -6.15811+017
-2.69112+016 -2.31054+014 -1.81160+013 -2.74958+011 -2.81138+009 -1.80343+007 -6.16286+004 -6.92400+001

```

RESIDUES OF THE TRANSFER FUNCTION=

249

POLE LOCATION	RESIDUE AT THE POLE	COMBINED RESIDUES=MAG* COS(Phi)+PHI MAGNITUDE	PHI(DEG)
-5.07201+002	1.25163+000		
-5.47011+001	-3.32304+001		
-1.80244+002	-4.51116+001		
(-4.73635+001) + J(4.81644+000)	(3.96992+001) + J(-1.47239+001)	8.45521+001	20.38208
(-4.24820+001)	-2.98742+001		
(-2.93179+001) + J(4.17102+000)	(-7.98108+001) + J(6.44831+000)	1.29950+001	-97.05562
-2.20350+001	3.88292+000		
-1.91344+001	-1.38204+000		
-1.41501+001	3.53891+000		
(-4.02300+000) + J(3.04256+000)	(-7.01427+001) + J(7.19085+001)	1.55957+002	-112.75604
-2.76346+000	(.44837+001		
-1.94603+000	1.83957+001		
-7.14716+001	-2.61777+001		

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZERES OF THE TRANSFER FUNCTION BETWEEN Y(2) AND U(3) =

```

1 (-9.87646+002) + J( 0.00000 )
2 (-9.59704+001) + J( 0.00000 )
3 ( 3.78198+001) + J( 4.85733+001)
4 ( 3.78198+001) + J(-4.85733+001)
5 (-5.07100+001) + J( 0.00000 )
6 (-8.82032+001) + J( 0.00000 )
7 (-2.63009+001) + J( 0.00000 )
8 (-2.02682+001) + J( 0.00000 )
9 (-1.91849+001) + J( 0.00000 )
10 (-1.73800+001) + J( 0.00000 )
11 (-1.32613+001) + J( 0.00000 )
12 (-9.16587+000) + J( 0.00000 )
13 (-2.04289+000) + J( 0.00000 )
14 (-2.91735+001) + J( 1.31272+001)
15 (-2.91735+001) + J(-1.31272+001)

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

-2.25464+019 -1.49051+020 -2.35610+020 -6.60322+014 -9.71350+018 -8.37950+017 -4.42770+016
-1.43407+015 -2.81275+013 -3.61478+011 -5.51317+009 -1.15179+008 -1.49338+006 -8.23795+003 -1.15200+001

```

RESIDUES OF THE TRANSFER FUNCTION=

250

POLE LOCATION	RESIDUE AT THE POLE	COMBINED RESIDUES=MAG* $\cos(\phi D+T+\phi H)$ MAGNITUDE PHI(DEG)
-5.01201+002	-5.63100+001	
-5.63101+001	-2.26009+001	
-1.20000+002	-1.08037+001	
(-4.75635+001) + J(0.81644+000)	(-1.57417+001) + J(-3.26180+001)	7.24531+001 115.79082
(-2.03379+001) + J(4.17152+000)	(-1.06702+000) + J(1.12801+001)	2.26610+001 -95.40573
-2.20330+001	5.66916+000	
-1.91544+001	-2.97029+002	
-1.61691+001	-1.18037+000	
(-4.02906+000) + J(3.04256+000)	(-1.18400+001) + J(8.11877+000)	2.87454+001 -145.60648
-2.70344+000	1.37528+001	
-1.94603+000	1.08578+000	
-7.15716+001	-3.66678+001	

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZERES OF THE TRANSFER FUNCTION BETWEEN Y(3) AND U(3) =

```

1 (-5.02355+002) + J( 0.0000 )
2 (-4.60727+001) + J( 1.93546+001)
3 (-4.60727+001) + J( 1.93546+001)
4 (-5.23123+001) + J( 0.0000 )
5 (-4.23064+001) + J( 0.0000 )
6 (-2.33844+001) + J( 3.4750+000)
7 (-2.33844+001) + J( 3.4750+000)
8 (-2.05455+001) + J( 3.4294+001)
9 (-2.05455+001) + J( 3.4294+001)
10 (-1.37602+001) + J( 0.0000 )
11 (-2.06478+000) + J( 0.0000 )
12 (-6.16279+000) + J( 0.0000 )
13 (-5.39175+001) + J( 1.2873+000)
14 (-5.39175+001) + J( 1.2873+000)
15 (-5.78594+001) + J( 0.0000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

6.08408+018 1.98200+019 5.45759+019 1.92387+019 9.21640+018 2.48753+018 3.97079+017 4.00209+016
2.66495+015 1.20550+014 1.72548+012 7.76670+010 1.06481+009 8.82835+006 3.73388+004 4.66300+001

```

RESIDUES OF THE TRANSFER FUNCTION=

POLE LOCATION	RESIDUE AT THE POLE	COMBINED RESIDUES=MAG* $\cos(\phi)$ MAGNITUDE PHI(DEG)
-5.01201+002	-1.70423+001	
-5.44021+001	-6.47245+000	
-1.20344+002	4.99103+001	
(-4.72635+001) + J(4.81644+000)	(1.48259+000) + J(-7.91027+000)	1.60960+001 79.38445
(-2.03379+001) + J(4.17102+000)	(1.44021+000) + J(1.44683+001)	2.89492+000 -5.73668
(-2.23350+001	-2.67433+001	
-1.91544+001	7.44359+001	
-1.61601+001	-1.77889+000	
(-4.09005+000) + J(1.04234+000)	(-8.11463+001) + J(8.99735+001)	2.42322+000 -132.04702
-2.7395+000	5.26440+001	
-1.94603+000	5.99844+002	
-7.16716+001	-1.00120+002	

TRANSFER FUNCTION PROGRAM

R 100 ENGINE TRANSFER FUNCTIONS

ZEROES OF THE TRANSFER FUNCTION BETWEEN Y(4) AND U(3) =

```

1 (-5.32150+002) + J( 0.0000 )
2 (-5.12288+001) + J( 0.0000 )
3 (-5.12288+001) + J( 0.0000 )
4 (-5.12288+001) + J( 0.0000 )
5 (-5.12288+001) + J( 0.0000 )
6 (-5.12288+001) + J( 0.0000 )
7 (-5.12288+001) + J( 0.0000 )
8 (-5.12288+001) + J( 0.0000 )
9 (-5.12288+001) + J( 0.0000 )
10 (-5.12288+001) + J( 0.0000 )
11 (-5.12288+001) + J( 0.0000 )
12 (-5.12288+001) + J( 0.0000 )
13 (-5.12288+001) + J( 0.0000 )
14 (-5.12288+001) + J( 0.0000 )
15 (-5.12288+001) + J( 0.0000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

3.24018+017 2.73447+016 5.85499+015 2.96965+014 7.86516+017 1.22503+017 1.21505+016
2.40082+014 3.46073+013 1.14020+012 2.42229+010 3.37501+008 2.85038+006 1.21930+004 1.48100+001

```

RESIDUES OF THE TRANSFER FUNCTION =

POLE LOCATION

RESIDUE AT THE POLE

COMBINED RESIDUES=MAG* $\cos(\omega\sigma t+\phi)$
MAGNITUDE PHI(DEG)

```

-5.01281+002 -1.47425+000 -2.02304+000 3.22340+000 99.69723
-5.01281+002 -2.02304+000 1.81584+001 4.03064+001 12.34042
(-4.722615+001) + J( 4.81644+000) + J(-1.58867+000) 8.10048+001 -108.86620
(-4.28320+001) + J( 4.17142+000) 1.96876+001 4.03064+001
-2.20350+001 -1.00465+001 1.28475+001
-1.01544+001 -2.66676+001
-1.61631+001 -1.30665+001 + J( 3.83265+001)
(-4.09983+000) + J( 3.04254+000) 1.51231+001
-2.70386+000 1.12786+002
-1.94603+000 -2.66180+003
-7.15716+001

```

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZEROES OF THE TRANSFER FUNCTION BETWEEN Y(5) AND U(3) =

```

1  (-4.93049+002) + Y( 0.00000 )
2  (-2.64974+002) + Y( 0.00000 )
3  (-5.4808+001) + Y( 0.00000 )
4  (-4.9816+001) + Y( 8.77373+000 )
5  (-3.8221+001) + Y( 8.77373+000 )
6  (-3.2387+001) + Y( 0.00000 )
7  (-2.3253+001) + Y( 0.00000 )
8  (-1.87856+001) + Y( 1.57788+000 )
9  (-1.87856+001) + Y( 1.57788+000 )
10 (-1.7175+001) + Y( 3.20125+000 )
11 (-1.7175+001) + Y( 3.20125+000 )
12 (-2.1233+000) + Y( 0.00000 )
13 (-1.59025+000) + Y( 0.00000 )
14 (-4.92388+001) + Y( 0.00000 )
15 (-9.42330+001) + Y( 0.00000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

1.20071+018  5.44244+018  8.87233+018  6.48738+018  2.54567+018  5.12047+017  6.10702+016  4.65682+015
2.1655+014  8.10300+012  7.69420+011  2.92279+009  2.84197+007  1.58776+005  4.25361+002  4.03200+001

```

RESIDUES OF THE TRANSFER FUNCTION=

POLE LOCATION.

RESIDUE AT THE POLE

COMBINED RESIDUES=MAG* $\cos(\omega D T + \text{PHI})$

PHI(DEG)

MAGNITUDE

```

-5.01241+002  4.89440+003  1.92929+001  1.92929+001  2.53408+001  7.40024  -61.26747
-5.63011+001  2.82069+002  (-4.60519+002) + J( 8.47622+002)  1.92929+001  2.53408+001  7.40024  -61.26747
-1.86984+002  (-4.60519+002) + J( 8.47622+002)  1.92929+001  2.53408+001  7.40024  -61.26747
(-4.72435+001) + J( 0.81744+000 )  1.92929+001  2.53408+001  7.40024  -61.26747
(-2.20820+001) + J( 0.17102+000 )  1.92929+001  2.53408+001  7.40024  -61.26747
(-2.20350+001)  1.92929+001  2.53408+001  7.40024  -61.26747
-1.91544+001  1.92929+001  2.53408+001  7.40024  -61.26747
-1.61601+001  1.92929+001  2.53408+001  7.40024  -61.26747
(-3.02906+000) + J( 3.04256+000 )  1.92929+001  2.53408+001  7.40024  -61.26747
-2.70358+000  1.92929+001  2.53408+001  7.40024  -61.26747
-1.94603+000  1.92929+001  2.53408+001  7.40024  -61.26747
-7.15715+001  1.92929+001  2.53408+001  7.40024  -61.26747

```


F 100 ENGINE TRANSFER FUNCTIONS

TRANSFER FUNCTION PROGRAM

ZERES OF THE TRANSFER FUNCTION BETWEEN Y(6) AND U(3) =

```

1  (-5.0049+02i) + J( 0.0000 )
2  (-1.88246+02i) + J( 0.0000 )
3  (-5.43100+01i) + J( 4.92352+00i)
4  (-5.43100+01i) + J( 4.92352+00i)
5  (-4.80669+01i) + J( 0.0000 )
6  (-3.72179+01i) + J( 0.0000 )
7  (-2.01740+01i) + J( 3.97223+00i)
8  (-2.01740+01i) + J( 3.97223+00i)
9  (-2.00662+01i) + J( 7.00276+00i)
10 (-2.00662+01i) + J( 7.00276+00i)
11 (-1.20474+01i) + J( 0.0000 )
12 (-5.28505+00i) + J( 0.0000 )
13 (-2.31070+00i) + J( 0.0000 )
14 (-1.95752+00i) + J( 0.0000 )
15 (-7.30370+01i) + J( 0.0000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

-4.45158+019  -1.60704+020  -1.23497+020  -3.49181+019  -1.50775+018  8.82875+017  1.87864+017  1.85227+016
1.09924+015  4.21530+013  1.06024+012  1.77550+010  1.85650+008  1.12587+006  3.35459+003  3.43600+000

```

RESIDUES OF THE TRANSFER FUNCTION =

POLE LOCATION	RESIDUE AT THE POLE	COMBINED RESIDUES=MAG* COS(WD*+PHI) MAGNITUDE PHI(DEG)
-5.01241+002	1.05167-003	
-5.61011+001	2.81435-001	
-1.81984+002	-1.51231-001	
(-4.72615+001) + J(4.81644+000)	(-5.78714-001) + J(-5.57612-001)	1.60728+000 136.06387
(-4.20820+001)	1.05114+000	
(-2.01339+001) + J(4.17112+000)	(1.02112-001) + J(-1.69395-002)	2.07409+001 9.40100
-2.20350+001	4.39167-001	
-1.91544+001	-5.96690-001	
-1.61601+001	1.98541+000	
(-4.02906+000) + J(3.04256+000)	(3.53443-001) + J(3.92614+000)	7.88404+000 -84.85593
-2.70334+000	6.73282-001	
-1.94643+000	5.32123-003	
-7.15716+001	-8.67619-003	

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZERES OF THE TRANSFER FUNCTION BETWEEN Y(7) AND U(3) =

```

1 (-5.00924+002) + J( 0.00000 )
2 (-1.92468+002) + J( 0.00000 )
3 (-5.90010+001) + J( 0.00000 )
4 (-5.03068+001) + J( 0.00000 )
5 (-4.54875+001) + J( 0.00000 )
6 (-5.77235+001) + J( 0.00000 )
7 (-2.09419+001) + J( 5.34825+000 )
8 (-2.09419+001) + J( 5.34825+000 )
9 (-1.99213+001) + J( 0.00000 )
10 (-1.89193+001) + J( 0.00000 )
11 (-1.14378+001) + J( 0.00000 )
12 (-2.04011+000) + J( 0.00000 )
13 (-1.90242+000) + J( 0.00000 )
14 (-8.40105+001) + J( 0.00000 )
15 (-5.38717+001) + J( 0.00000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

1.45840+019  6.39889+019  1.00150+020  7.41312+019  2.81564+019  5.80505+018  7.16762+017  5.67759+016
3.0012+015  1.07707+010  2.42106+012  4.23901+010  4.35569+008  2.60831+006  7.68922+003  7.82400+000

```

RESIDUES OF THE TRANSFER FUNCTION=

255

POLE LOCATION

RESIDUE AT THE POLE

COMBINED RESIDUES=MAG* $\cos(\text{WD}*\text{T}+\text{PHI})$
MAGNITUDE PHI(DEG)

```

-5.0+241+002  4.31100-003  2.79227+000  2.40219+000  7.69789+000  -65.78505
-5.63031+001  -2.82415-001  81.05850  177.67002
-1.80984+002  -5.42365-001  2.79227+000  2.40219+000  7.69789+000  -65.78505
(-4.75635+001) + J( 0.81644+000 )  2.79227+000  2.40219+000  7.69789+000  -65.78505
-4.20820+001  8.94438-001  2.79227+000  2.40219+000  7.69789+000  -65.78505
(-2.03393+001) + J( 0.17102+000 )  2.79227+000  2.40219+000  7.69789+000  -65.78505
-2.20350+001  2.67153+000  2.79227+000  2.40219+000  7.69789+000  -65.78505
-1.01344+001  1.69584-001  2.79227+000  2.40219+000  7.69789+000  -65.78505
-1.61601+001  3.14768+000  2.79227+000  2.40219+000  7.69789+000  -65.78505
(-4.02945+000) + J( 3.04254+000 )  2.79227+000  2.40219+000  7.69789+000  -65.78505
-2.70364+000  1.57869+000  2.79227+000  2.40219+000  7.69789+000  -65.78505
-1.94603+000  5.73047-001  2.79227+000  2.40219+000  7.69789+000  -65.78505
-7.15716+001  1.37477-003  2.79227+000  2.40219+000  7.69789+000  -65.78505
-4.94105+003  -4.94105+003

```

TRANSFER FUNCTION PROGRAM

F 100 ENGINE TRANSFER FUNCTIONS

ZEROES OF THE TRANSFER FUNCTION BETWEEN Y(8) AND U(3) =

```

1  (+5.01401+002) + J( 0.00000 )
2  (-7.73000+001) + J( 2.99726+001)
3  (-7.73000+001) + J( -2.99726+001)
4  (+5.23100+001) + J( 0.00000 )
5  (-5.26745+001) + J( 0.00000 )
6  (+3.7248+001) + J( 0.00000 )
7  (+1.91140+000) + J( 1.09755+001)
8  (+1.91140+000) + J( -1.09755+001)
9  (-2.04225+001) + J( 0.00000 )
10 (+1.94077+001) + J( 0.00000 )
11 (-1.70022+001) + J( 0.00000 )
12 (-2.18935+000) + J( 0.00000 )
13 (-1.12847+001) + J( 0.00000 )
14 (-7.09200+001) + J( 0.00000 )
15 (-1.74693+000) + J( 0.00000 )

```

COEFFICIENTS OF THE NUMERATOR POLYNOMIAL IN ASCENDING POWERS OF S =

```

-8.46622+019  -2.32032+020  -8.49703+019  -1.73845+019  -2.29459+018  -2.35172+017  -1.95252+016
-1.22000+015  -5.40321+017  -3.15619+010  -3.91133+008  -2.86199+006  -1.06111+004  -1.24300+001

```

RESIDUES OF THE TRANSFER FUNCTION=

POLE LOCATION

RESIDUE AT THE POLE

COMBINED RESIDUES=MAG* $\cos(\omega D T + \text{PHI})$
MAGNITUDE PHI(DEG)

```

-5.01201+002  4.97013+003  2.13788+001  2.24657+001  9.22145+000  -90.11456
-5.61001+001  4.96415+000  (-1.96534+000) + J( 1.05034+001)  2.13788+001  -100.70366
-1.80984+002  (-8.71052+000)  (-1.96534+000) + J( 1.05034+001)  2.13788+001  -100.70366
(-4.72015+001) + J( 0.81644+000)  (-1.96534+000) + J( 1.05034+001)  2.13788+001  -100.70366
-4.28800+001  (-3.26675+000)  (-1.96534+000) + J( 1.05034+001)  2.13788+001  -100.70366
(-2.03359+001) + J( 0.17102+000)  (-1.96534+000) + J( 1.05034+001)  2.13788+001  -100.70366
-2.20350+001  (-6.42072+000)  (-1.96534+000) + J( 1.05034+001)  2.13788+001  -100.70366
-1.91584+001  4.39094+001  (-1.96534+000) + J( 1.05034+001)  2.13788+001  -100.70366
-1.51601+001  1.54119+000  (-1.96534+000) + J( 1.05034+001)  2.13788+001  -100.70366
(-4.02000+000) + J( 1.04254+000)  (-1.96534+000) + J( 1.05034+001)  2.13788+001  -100.70366
-2.70356+000  1.38450+000  (-1.96534+000) + J( 1.05034+001)  2.13788+001  -100.70366
-1.94601+000  1.07501+001  (-1.96534+000) + J( 1.05034+001)  2.13788+001  -100.70366
-7.15715+001  -2.16200+002  (-1.96534+000) + J( 1.05034+001)  2.13788+001  -100.70366

```

APPENDIX E

LINEAR QUADRATIC REGULATOR DESIGN DATA (OPTSYS PROGRAM)

Plant: $\dot{x} = Fx + Gu$

Outputs: $y = HY x + DY u$

Performance Index: $J = \frac{1}{2} \int_0^{\infty} [x^T A x + u^T B u] dt$

PARAMETER	VARIABLE	UNITS
x_1	Low Rotor Speed	RPM
x_2	High Rotor Speed	RPM
x_3	Augmentor Pressure	psia
x_4	Fuel Flow	lbm/hr
x_5	Burner Pressure	psia
u_1	Fuel Flow Command	lbm/hr
u_2	Nozzle Area	ft ²
u_3	CIVV	deg
u_4	RCVV	deg
u_5	Bleed Flow	Fraction Compressor Flow
y_1	Thrust	lbf
y_2	Airflow	lbm/sec
y_3	TT4	°R
y_4	Fan Surge Margin	Per cent
y_5	Compressor Surge Margin	Per cent
y_6	$\Delta p/p$ Parameter	---
y_7	$\Delta p/p$ Average	---

E.1 LQR BASELINE DESIGNS

DESIGN POINT	PLA (DEG)	ALT (FT)	Mn	PAGE
HPG1	83	45K	0.9	259
HPG2	83	30K	0.9	263
HPG3	83	0	0	267
HPG4	83	0	1.2	271
LPG1	20	30K	0.9	275
LPG2	20	0	0	279

MPG1

A3/0.9/45K OPTIMAL CONTROL DESIGN POINT

F

	1	2	3	4	5
1	-9.6060-001	-5.9660-001	-1.1110+003	1.3370+000	1.2970+002
2	-7.9550-001	-1.6440+000	-2.6480+002	-1.9100-001	6.7730+001
3	2.5900-003	-5.1810-003	-8.8860+000	7.3940+003	5.7560-001
4	0.0000	0.0000	0.0000	-1.0000+001	0.0000
5	-2.4380-001	1.8160+000	6.5720+002	1.7250+000	-1.6970+002

G

	1	2	3	4	5
1	-2.3920-001	-3.6100+002	-2.7230+001	-8.0010+000	2.8000+003
2	-4.1130-002	-6.9880+001	1.7470+001	-1.4170+001	7.1940+003
3	-6.5480-004	-2.0770+001	9.1200-002	-7.4410-002	-3.7110+000
4	1.0000+001	0.0000	0.0000	0.0000	0.0000
5	-2.9390-001	-1.3160+002	-1.2390+001	1.4110+001	-1.9240+004

HV

	1	2	3	4	5
1	3.7000-001	-4.5590-001	-4.3170-002	-7.5150-002	4.3080+001
2	-4.3290-003	1.9050-006	-1.3180-002	-2.2210-004	4.3750-006
3	1.4950-001	-9.0040-002	-3.6140+001	4.1960-001	1.0590+000
4	2.0680-004	1.8620-006	-6.0210-002	1.1650-005	2.9390+004
5	6.2040-005	1.5240-004	-4.7990-002	8.3060-005	-1.1070-002
6	5.7050-005	-3.7290-005	-4.3920-002	-4.3720-005	7.9770-004
7	1.6770-005	3.3180-006	-1.1520-002	-8.7460-006	4.9380-005

SYSTEMS CONTROL, INC. (VT) •
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

M3/0.9/4SK OPTIMAL CONTROL METHOD POINT HPG1

DY

	1	2	3	4	5
1	5.2290-003	2.3820+002	9.0480+000	-3.0970+000	3.3790+003
2	6.3540-007	2.0900-001	1.7990-001	3.7430-004	1.5460+000
3	1.3790-002	5.1280+001	2.4430+000	-4.3940-001	1.9300+003
4	9.6070-007	2.5730-002	7.3550+004	1.4060-004	5.9090-001
5	2.5690-005	-1.9910-002	-1.0700-003	1.6210-003	-4.0190-001
6	1.4180-005	2.6580-002	1.9010-003	-2.3970-004	2.6330-001
7	2.6970-006	9.0870-003	6.7140-004	4.8670-005	6.0650-002

A

	1	2	3	4	5
1	5.0000-004	0.0000	0.0000	0.0000	0.0000
2	0.0000	5.0000-004	0.0000	0.0000	0.0000
3	0.0000	0.0000	5.0000-001	0.0000	0.0000
4	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000	0.0000	1.0000+000

B 260

	1	2	3	4	5
1	1.0000-004	0.0000	0.0000	0.0000	0.0000
2	0.0000	4.0000+002	0.0000	0.0000	0.0000
3	0.0000	0.0000	5.0000-001	0.0000	0.0000
4	0.0000	0.0000	0.0000	2.0000-001	0.0000
5	0.0000	0.0000	0.0000	0.0000	1.0000+004

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

83/0.9/45K OPTIMAL CONTROL DESIGN POINT MP61

1 OPTIMAL CLOSED LOOP EIGENSYSTEM 1

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-2.62414+002)+J(0.00000)	0.00000	1.00000	1 (-5.45051+001)+J(0.00000) 2 (-3.97221+001)+J(0.00000) 3 (-2.13960+003)+J(0.00000) 4 (-2.12184+001)+J(0.00000) 5 (1.00000+000)+J(0.00000)	-.5450507 -.3972211 -.0021396 -.2121841 1.0000000	.00000 .00000 .00000 .00000 .00000
(-1.00714+001)+J(1.98371+000)	1.02649+001	.98115	1 (-3.89151+001)+J(-2.92864+001) 2 (-3.55412+002)+J(1.10992+002) 3 (-2.23742+003)+J(-2.10709+003) 4 (1.00000+000)+J(0.00000) 5 (1.83738+003)+J(-2.39555+003)	.4870395 .0372339 .0030734 1.0000000 .0030190	.143.03590 162.65685 -136.71836 .00000 -52.51196
(-3.37406+000)+J(0.00000)	0.00000	1.00000	1 (1.00000+000)+J(0.00000) 2 (-1.32972+001)+J(0.00000) 3 (6.54331+004)+J(0.00000) 4 (-6.07342+001)+J(0.00000) 5 (-7.09095+003)+J(0.00000)	1.0000000 -.1329716 .0006543 -.6073425 -.0070909	.00000 .00000 .00000 .00000 .00000
(-1.48428+000)+J(0.00000)	0.00000	1.00000	1 (-1.35220+001)+J(0.00000) 2 (1.00000+000)+J(0.00000) 3 (-1.53291+003)+J(0.00000) 4 (-8.58619+001)+J(0.00000) 5 (-1.05962+003)+J(0.00000)	-.1352200 1.0000000 -.0015329 -.8586186 -.0010596	.00000 .00000 .00000 .00000 .00000

THE RICCATI MATRIX

SYSTEMS CONTROL, INC. (VT)
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

83/0.9/45K OPTIMAL CONTROL DESIGN POINT HPG1

	1	2	3	4	5
1	1.2347-004	2.3003-005	1.0213-002	1.0949-005	4.9772-005
2	2.3903-005	2.2058-004	1.0223-003	1.2319-005	1.1662-004
3	1.0213-002	1.0223-003	1.3754+000	3.6966-005	2.5986-003
4	1.0949-005	1.4319-005	3.6966-005	4.0809-006	2.7335-005
5	4.9772-005	1.1662-004	2.5986-003	2.7335-005	2.4066-003

-CONTROLLER FEEDBACK GAINS

	1	2	3	4	5
1	7.2998-001	1.1293+000	3.6698+000	3.4769-001	4.4277+000
2	3.9988-004	2.1573-005	6.3676-002	1.8154-003	1.3199-003
3	8.9853-003	3.3291-003	7.0699-001	7.8009-004	5.7799-002
4	6.7837-004	7.9746-003	1.5261-001	4.8977-004	1.5857-001
5	4.0205-005	5.8620-005	9.1052-003	3.9212-005	4.5335-003

F

	1	2	3	4	5
1	9.6060-001	5.9660-001	1.1110+003	1.3370+000	1.2970+002
2	7.9550-001	1.6440+000	2.6440+002	1.9100-001	6.7730+001
3	2.5900-003	5.1810-003	8.8860+000	7.3940-003	5.7560-001
4	0.0000	0.0000	0.0000	1.0000+001	0.0000
5	7.4380-001	1.8160+000	6.9720+002	1.7250+000	1.6970+002

G

	1	2	3	4	5
1	2.3920-001	3.6100+002	2.7230+001	0.0010+000	2.8000+003
2	4.1130-002	8.4880+001	1.7470+001	1.4170+001	7.1940+003
3	6.5480-004	2.0770+001	9.1200-002	7.4410-002	3.7110+000
4	1.0000+001	0.0000	0.0000	0.0000	0.0000
5	2.9390-001	1.9360+002	1.2390+001	1.4110+001	1.9240+004

HPG2

83/0.9/30K OPTIMAL CONTROL DESIGN POINT

F

1	5.3430-001	-3.3970+000	-6.6360+002	-1.5080+000	1.7160+002
2	-4.1430-001	-5.5810+000	-3.2320+002	1.2570+000	4.7780+001
3	-5.7600-004	-2.1260-003	-1.1400+001	1.6150+002	5.6250+001
4	0.0000	0.0000	0.0000	-1.0000+001	0.0000
5	-2.8310+000	4.9390+000	4.9750+002	2.7640+000	-2.0550+002

G

1	6.0930-001	1.4630+003	3.0170-001	-1.6070+001	3.9560+004
2	-5.1420-001	3.1150+002	5.7120+000	-2.7810+001	8.9070+002
3	-8.0090-003	-5.8200+001	7.2380-002	-7.1990+002	-7.7230+001
4	1.0000+001	0.0000	0.0000	0.0000	0.0000
5	-2.2060-001	-1.6390+003	-5.6990+001	2.9720+001	-6.0330+004

HV

1	1.0360+000	-1.2340+000	3.9160+001	-2.3980-001	5.231+001
2	-7.8610-003	-6.8940-005	-4.6250-003	1.4050-004	-1.000 003
3	2.0070-001	-1.1190-001	1.7880+000	2.2950-001	-8.0331 01
4	2.8730-004	-7.9550-005	-1.1700-002	1.0020-004	1.3330-003
5	-1.2830-004	-2.0640-004	1.1070-002	9.4240-005	-6.5960+003
6	1.3070-004	-1.0690-004	8.4650-003	-9.4120-005	1.5590-003
7	3.7140-005	-1.6370-005	-1.9240-003	-2.5820-005	3.1770-004

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

83/0.9/30K OPTIMAL CONTROL DESIGN POINT MPQ2

DY

	1	2	3	4	5
1	-1.0950-001	8.3780+002	2.5470+001	-7.2580+000	1.1850+004
2	2.5070-005	3.6060-001	3.5450-001	-2.9010-004	1.0670+000
3	-5.9120-002	1.3530+002	3.4250+000	-1.9050-001	2.5730+003
4	3.1670-005	9.4930-002	6.2020-003	-1.0310-004	1.3070+000
5	1.0660-005	9.0300-002	2.7010-003	-1.1250-003	-1.4060+000
6	2.2210-005	1.0380-001	3.7260-003	-3.9640-004	1.2570+000
7	7.3960-006	2.9790-002	1.1840-003	-4.0500-006	3.2490-001

A

	1	2	3	4	5
1	1.0000-003	0.0000	0.0000	0.0000	0.0000
2	0.0000	1.0000-003	0.0000	0.0000	0.0000
3	0.0000	0.0000	2.0000+000	0.0000	0.0000
4	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000	0.0000	4.0000+000

B

	1	2	3	4	5
1	1.0000-004	0.0000	0.0000	0.0000	0.0000
2	0.0000	1.0000+003	0.0000	0.0000	0.0000
3	0.0000	0.0000	1.0000+000	0.0000	0.0000
4	0.0000	0.0000	0.0000	8.0000-001	0.0000
5	0.0000	0.0000	0.0000	0.0000	8.0000+004

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

03/0.0/30K NATURAL CONTROL DESIGN POINT HPG2

CLOSED LOOP EIGENSYSTEM

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-5.042+3.042j)+j(0.0000)	0.00000	1.00000	1 (-7.21982-001)+j(0.00000) 2 (-1.11701-001)+j(0.00000) 3 (7.55761-004)+j(0.00000) 4 (-2.07994-001)+j(0.00000) 5 (1.00000+000)+j(0.00000)	-7219823 -1117007 0007558 -2079965 1.0000000	.00000 .00000 .00000 .00000 .00000
(-1.31777+001)+j(3.33441+000)	1.35891+001	.04937	1 (-5.34555-003)+j(-1.33037-001) 2 (-1.31589-001)+j(-1.32226-001) 3 (-8.66465-004)+j(-4.21916-003) 4 (1.00000+000)+j(0.00000) 5 (1.35632-003)+j(-1.78615-003)	.1331439 .1865459 .0043072 1.0000000 .0022428	-92.30097 -134.86171 -101.60515 .00000 -52.78872
(-2.47344+000)+j(0.00000)	0.00000	1.00000	1 (1.00000+000)+j(0.00000) 2 (-8.51196-001)+j(0.00000) 3 (3.67416-003)+j(0.00000) 4 (7.87826-001)+j(0.00000) 5 (-2.46840-003)+j(0.00000)	1.0000000 -.8511961 -.0036742 .7878260 -.0024684	.00000 .00000 .00000 .00000 .00000
(-4.13540+000)+j(0.00000)	0.00000	1.00000	1 (-2.54634-001)+j(0.00000) 2 (-5.83413-001)+j(0.00000) 3 (3.54267-004)+j(0.00000) 4 (1.00000+000)+j(0.00000) 5 (9.83289-004)+j(0.00000)	-.2596383 -.5639131 -.0003593 1.0000000 .0009833	.00000 .00000 .00000 .00000 .00000

THE RICCATI MATRIX

SYSTEM8 CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

R3/0.0/30X OPTIMAL CONTROL DESIGN POINT HPC2

	1	2	3	4	5
1	2.6676-004	-5.9451-005	-5.9069-003	-1.6594-005	1.5533-004
2	-5.4651-005	2.5551-004	-2.8424-004	3.4145-005	4.5905-005
3	-5.9069-003	-5.9069-004	3.9126-001	7.8270-004	9.5107-004
4	-1.6594-005	3.4145-005	7.8270-004	9.7516-006	2.3981-005
5	1.5533-004	4.5905-005	9.5107-004	2.3981-005	5.7571-003

CONTROLLED FEEDBACK GAINS

	1	2	3	4	5
1	-4.1529-001	-1.8100-000	-1.3411-001	-5.8288-001	9.6678-000
2	-4.6332-001	3.7160-005	3.2260-002	9.8500-005	9.2497-003
3	9.5332-003	1.5533-003	3.2757-002	1.1200-003	3.2772-001
4	-2.9728-003	5.2330-003	-1.0944-001	3.3147-005	-2.0907-001
5	-2.0414-005	9.0665-005	4.0257-003	2.6671-005	4.2652-003

	1	2	3	4	5
1	5.3430-001	-3.3070-000	-4.6360-002	-1.5080-000	1.7160-002
2	4.1430-001	-2.5411-000	-3.2320-002	1.2570-000	4.7780-001
3	-5.7206-004	-2.1440-003	-1.1400-001	1.8150-002	5.6250-001
4	0.0000	0.0000	0.0000	-1.0000-001	0.0000
5	-2.8510-000	4.4500-000	4.9750-002	2.7600-000	-2.0550-002

	1	2	3	4	5
1	4.0230-001	1.0000-003	3.0170-001	-1.6070-001	3.9560-004
2	-5.1420-001	3.1150-002	5.7120-000	-2.7810-001	8.8070-002
3	-8.0000-003	-5.2200-001	7.2350-002	-7.1990-002	-7.7230-001
4	1.0000-001	0.0000	0.0000	0.0000	0.0000
5	-2.2060-001	-1.6400-003	-5.6490-001	2.9720-001	-6.0330-004

PT/0/0X OPTIMAL CONTROL DESIGN PRINT MPG3

	1	2	3	4	5
1	-3.2450+000	-2.1580+000	-9.1550+002	5.7310-001	1.3420+002
2	1.8420+000	-5.9410+000	-2.8140+002	1.8970-001	5.7050+001
3	1.6860+002	-2.5500+002	-1.0030+001	7.9940-003	5.8070-001
4	0.0000	0.0000	0.0000	-1.0000+001	0.0000
5	-2.1630+000	6.4420+000	7.8850+002	1.1950+000	-1.7150+002

	1	2	3	4	5
1	1.4320+002	-3.5530+002	-9.9000+001	-1.5490+001	2.2200+004
2	2.8710-001	7.2240+002	2.5140+001	-6.4470+001	8.1220+003
3	-2.4690+003	-1.0300+002	6.3330-001	-3.2130-001	-7.4180+001
4	1.0000+001	0.0000	0.0000	0.0000	0.0000
5	-1.3110-001	3.2400+002	-2.5000+001	6.2570+001	6.4450+004

	1	2	3	4	5
1	1.4420+000	-1.7480+000	7.9900+001	-1.8900-001	3.7710+001
2	1.3430-002	3.1020+005	-1.0600+002	1.2890-004	-1.6390+007
3	1.5940-001	-1.1290-001	-0.9590+000	7.1860-002	-1.8350-001
4	7.5900+005	3.2490+006	-1.4770+002	2.2840+006	4.3150+005
5	-0.8590+005	1.3410+004	1.1400+002	1.9510+005	-2.6840+003
6	5.1770+005	-3.9100+005	-1.2300+002	-1.2280+005	2.0790+004
7	1.5700+005	2.2070+006	-3.2450+003	-2.6460+006	9.9150+006

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

12/0/74 OPTIMAL CONTROL DESIGN POINT WPG3

	1	2	3	4	5
1	1.3020-001	1.0020+002	4.8020+001	1.5030+001	1.0830+004
2	1.4490-007	3.8350-001	6.8080-001	2.8120-004	3.2040-004
3	2.9670-002	7.7270+001	2.5670+000	-7.6310-001	2.0660+003
4	1.0460-006	-7.7200-003	-5.8140-003	1.1570-004	6.6050-002
5	-4.3050-006	-7.2470-003	-6.8410-004	-9.6430-004	-2.8150-001
6	5.7270-006	4.0040-003	1.8330-003	-2.9020-004	1.8840-001
7	1.2840-006	2.3440-003	6.8810-004	4.6680-005	4.0650-002

	1	2	3	4	5
1	1.0000-003	0.0000	0.0000	0.0000	0.0000
2	0.0000	2.0000-003	0.0000	0.0000	0.0000
3	0.0000	0.0000	5.0000+000	0.0000	0.0000
4	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000	0.0000	2.0000+000

	1	2	3	4	5
1	1.0000-004	0.0000	0.0000	0.0000	0.0000
2	0.0000	2.0000+003	0.0000	0.0000	0.0000
3	0.0000	0.0000	2.0000+000	0.0000	0.0000
4	0.0000	0.0000	0.0000	1.0000+000	0.0000
5	0.0000	0.0000	0.0000	0.0000	1.0000+005

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

OPTIMAL CONTROL DESIGN POINT HPG3

OPTIMAL CLOSED LOOP EIGENSYSTEM

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-3.49254+0.021)*J(0.00000)	0.00000	1.00000	1 (-5.50266+0.011)*J(0.00000) 2 (-2.72969+0.011)*J(0.00000) 3 (-1.51009+0.031)*J(0.00000) 4 (-1.10023+0.011)*J(0.00000) 5 (1.00000+0.000)*J(0.00000)	-5502655 -2729695 -0015101 -1100233 1.0000000	.00000 .00000 .00000 .00000 .00000
(-1.00200+0.011)*J(2.94341+0.000)	1.04490+0.001	.95594	1 (-1.41786+0.011)*J(-3.36218+0.011) 2 (-6.55308+0.021)*J(-2.90665+0.021) 3 (-1.25673+0.031)*J(-2.35491+0.031) 4 (1.00000+0.000)*J(0.00000) 5 (3.37945+0.004)*J(-9.43296+0.004)	.3648920 .0710478 .0026643 1.0000000 .0010020	-112.86557 -156.08011 -118.08713 .00000 -70.24943
(-1.06434+0.011)*J(0.00000)	0.00000	1.00000	1 (-1.82264+0.011)*J(0.00000) 2 (-3.88293+0.021)*J(0.00000) 3 (1.43202+0.051)*J(0.00000) 4 (1.00000+0.000)*J(0.00000) 5 (2.14294+0.031)*J(0.00000)	-1822644 -0386293 -0000143 1.0000000 .0021429	.00000 .00000 .00000 .00000 .00000
(-2.13391+0.000)*J(0.00000)	0.00000	1.00000	1 (-9.38345+0.021)*J(0.00000) 2 (-3.14987+0.011)*J(0.00000) 3 (1.18750+0.031)*J(0.00000) 4 (1.00000+0.000)*J(0.00000) 5 (6.90898+0.004)*J(0.00000)	-0938345 -3149871 -0011875 1.0000000 .0006909	.00000 .00000 .00000 .00000 .00000

THE HICCATI MATRIX

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

43/0/0M OPTIMAL CONTROL DESIGN POINT WPG3

	1	2	3	4	5
1	9.5827-005	1.3722-005	-3.8434-003	3.9513-006	2.6971-005
2	1.4722-005	2.4402-004	1.3025-003	1.4631-005	1.5161-004
3	-3.8434-003	1.4025-003	7.6721-001	5.5453-004	7.3596-003
4	3.9513-006	1.4031-005	5.5453-004	2.3830-006	2.0219-005
5	2.6971-005	1.5141-004	7.3596-003	2.0216-005	3.9162-003

CONTROLLED FEEDBACK GAINS

	1	2	3	4	5
1	-5.1065-001	-1.2144-000	-3.0051-001	-2.4048-001	2.6550+000
2	-1.9072-000	-1.5335-005	3.7142-002	2.0599-005	-3.1661-004
3	4.1154-003	-2.5570-004	-3.5748-001	4.8901-005	4.6052-002
4	-0.8312-000	7.2399-003	-1.4902-001	-7.6411-005	-2.3242-001
5	-7.4937-006	7.5244-005	6.0598-003	1.1375-005	2.5111-003

	1	2	3	4	5
1	-3.2450+000	-2.1440+000	-0.1550+002	5.7310-001	1.3420+002
2	1.6420+000	-5.4110+000	-2.8140+002	1.8070-001	5.7050+001
3	1.6860+002	-2.5560-002	-1.0030+001	7.9940-003	5.8070-001
4	0.0000	0.0000	0.0000	-1.0000+001	0.0000
5	-2.1630+000	4.4420+000	7.4050+002	1.1950+000	-1.7150+002

	1	2	3	4	5
1	1.4320-002	-3.5430+002	-9.9080+001	-1.5490+001	2.2200+004
2	2.4710-001	7.2440+002	2.5140+001	-6.4870+001	8.1220+003
3	-2.4690-003	-1.0300+002	6.3330-001	-3.2130-001	-7.4180+001
4	1.0000+001	0.0000	0.0000	0.0000	0.0000
5	-1.3310-001	3.2850+002	-2.4500+001	6.2570+001	-6.4450+004

MPG4

AS/1-2/0K OPTIMAL CONTROL DESIGN POINT

1	-9.0420+000	-2.9530+001	-5.8950+002	3.6180+001	1.3220+002
2	-1.9110+000	-2.4310+000	1.6130+002	-1.9550+001	4.1260+001
3	4.1400+003	-3.4440+002	-9.0290+000	1.1250+002	5.8890+001
4	0.0000	0.0000	0.0000	-1.0000+001	0.0000
5	5.1540+000	1.0070+001	-1.5450+001	1.7700+000	-1.7220+002

1	-3.1750+002	-4.5050+001	-3.2200+002	5.0370+000	4.0620+004
2	4.0050+001	2.5470+003	-1.0020+002	-9.4500+001	1.3950+004
3	-2.3160+003	-1.3000+002	5.6570+001	-7.9360+001	-1.4360+002
4	1.0000+001	0.0000	0.0000	0.0000	0.0000
5	-5.1840+001	-1.5550+003	2.3090+002	1.8310+002	-1.1490+005

1	-8.1630+001	-3.1300+000	3.6220+002	-7.9180+001	4.3970+001
2	3.3770+002	1.0000+003	-6.9020+002	6.0470+004	-1.4610+003
3	-4.5100+002	-9.4540+002	1.0000+001	4.3140+002	-1.4990+001
4	2.9476+005	4.2070+005	-4.4080+003	1.0250+005	-1.1780+004
5	2.5100+005	3.3300+004	-3.4010+003	1.8330+005	-1.7320+003

SYSTEMS CONTROL, INC. (VT) •
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

AT/1.2/OK OPTIMAL CONTROL DESIGN POINT HPG4

CV

	1	2	3	4	5
1	6.5200-001	2.6700+003	-4.6490+001	-5.4290+001	2.5850+004
2	-1.1870-004	1.1870+000	1.6490+000	1.9070+002	9.0360+000
3	3.2710-002	1.5550+002	-4.0230+000	-3.1390+000	1.5570+003
4	-7.6000-006	-2.7080-002	-5.9360-003	1.2530-003	-1.1950-001
5	-1.6620-005	-5.6790-002	2.9480-003	9.1150-004	-1.1880-001

A

	1	2	3	4	5
1	0.0000-003	0.0000	0.0000	0.0000	0.0000
2	0.0000	2.0000-003	0.0000	0.0000	0.0000
3	0.0000	0.0000	3.0000+001	0.0000	0.0000
4	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000	0.0000	2.0000+000

B

	1	2	3	4	5
1	2.0000-004	0.0000	0.0000	0.0000	0.0000
2	0.0000	1.0000+003	0.0000	0.0000	0.0000
3	0.0000	0.0000	2.0000+001	0.0000	0.0000
4	0.0000	0.0000	0.0000	8.0000+000	0.0000
5	0.0000	0.0000	0.0000	0.0000	8.0000+005

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

R3/1.270K OPTIMAL CONTROL DESIGN POINT HPG4

OPTIMAL CLOSED LOOP EIGENSYSTEM 1

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-2.44272+002)+J(0.00000)	0.00000	1.00000	1 (-6.25582-001)+J(0.00000) 2 (-2.64835-001)+J(0.00000) 3 (-1.53083-003)+J(0.00000) 4 (-3.45999-001)+J(0.00000) 5 (1.00000+000)+J(0.00000)	.6255823 .2648347 .0015308 .3454989 1.0000000	.00000 .00000 .00000 .00000 .00000
(-1.22957+001)+J(4.12493+000)	1.29704+001	.94798	1 (-2.06020-001)+J(4.41336-001) 2 (3.51623+002)+J(1.07362-003) 3 (-2.31289-003)+J(-2.43879-003) 4 (1.00000+000)+J(0.00000) 5 (3.69024+003)+J(3.67563-003)	.4870541 .0351786 .0033611 1.0000000 .0052113	-115.02360 1.74888 -133.48229 .00000 -44.85532
(-8.12037+000)+J(3.35619+000)	8.97176+000	.92740	1 (-2.23303-001)+J(1.13771-001) 2 (-9.96760-002)+J(-1.86790-001) 3 (1.46656-003)+J(-2.22469-004) 4 (1.00000+000)+J(0.00000) 5 (-1.45989-003)+J(3.79956-003)	.2506157 .2117213 .0014833 1.0000000 .0040704	153.00159 -118.08552 -8.62570 .00000 -111.01803

THE HICCATI MATRIX

1	2	3	4	5
1 2.8900-004 1.5308-004 -6.4004-003 2.6270-005 2.8835-004				
2 1.5303-004 4.4452-004 -4.3565-003 4.2746-005 3.8312-004				
3 -4.4004-003 -4.3565-003 1.6186+000 1.5219-004 -3.0594-003				
4 2.6270-005 4.2746-005 1.5219-004 7.3302-006 5.6744-005				
5 2.8835-004 3.8312-004 -3.0594-003 5.6744-005 4.6924-003				

CONTROLLED FEEDBACK GAIN'S

	1	2	3	4	5
1	-1.100E+000	-2.451E+000	1.457E+001	-3.546E+001	8.070E+000
2	-9.451E+005	-1.415E+004	2.794E+002	8.788E+008	7.400E+004
3	2.283E+003	4.174E+004	-1.353E+001	-2.230E+005	-4.752E+002
4	-5.604E+003	-1.000E+003	1.831E+001	-7.952E+004	-1.033E+001
5	2.286E+005	3.452E+005	2.520E+004	6.287E+004	6.520E+004

	1	2	3	4	5
1	-9.048E+000	-6.953E+001	-5.895E+002	3.614E+001	1.322E+002
2	-1.911E+000	-4.331E+000	1.613E+002	-1.955E+001	4.126E+001
3	4.140E+003	-1.246E+002	-9.029E+000	1.125E+002	5.889E+001
4	0.000E+000	0.000E+000	0.000E+000	-1.000E+001	0.000E+000
5	5.154E+000	1.047E+001	-1.545E+001	1.770E+000	-1.722E+002

	1	2	3	4	5
1	-3.175E+002	-2.505E+001	-3.220E+002	5.037E+000	4.062E+004
2	6.603E+001	2.547E+003	-1.002E+002	-9.450E+001	1.395E+004
3	-2.310E+003	-1.304E+002	5.657E+001	-7.936E+001	-1.436E+002
4	1.000E+001	0.000E+000	0.000E+000	0.000E+000	0.000E+000
5	-5.184E+001	-1.545E+003	2.309E+002	1.831E+002	-1.149E+005

2070.9/30K OPTIMAL CONTROL DESIGN POINT

LPG1

F	1	1	-1.1650+000	-2.7010+001	-5.0920+002	8.8230+001	1.2540+002
	2	2	-0.4200+002	-1.2170+000	-1.0770+002	2.0020+000	3.9490+001
	3	3	5.0800+003	-7.2730+003	-7.2810+000	1.2150+002	3.9300+001
	4	4	0.0000	0.0000	0.0000	-1.0000+001	0.0000
	5	5	2.3870+001	2.1000+000	1.0780+002	1.5580+000	-1.1790+002
G	1	1	-4.7900+001	7.7910+001	-4.8320+000	-2.9200+000	5.1110+003
	2	2	-5.2200+001	9.2910+000	-3.3800+000	-1.7770+001	-1.1870+003
	3	3	-2.0500+003	-1.5350+001	2.7880+002	-1.0490+001	-1.4350+001
	4	4	1.0000+001	0.0000	0.0000	0.0000	0.0000
	5	5	-4.2770+001	-5.3170+001	5.8200+000	2.9420+001	-7.1520+003
H	1	1	-3.4830+002	-4.4380+001	2.5270+002	2.8200+001	2.4880+001
	2	2	1.0880+002	1.0000+003	-7.5060+001	5.0550+004	7.0000+004
	3	3	-1.2720+002	-1.0590+001	-1.0020+000	9.9330+001	-1.6870+001
	4	4	1.1540+004	1.1140+004	-4.9890+002	2.0310+005	5.3280+005
	5	5	3.5890+005	2.1040+004	1.3340+002	8.8000+005	-1.4850+002
	6	6	9.6340+005	9.0030+006	-6.5740+002	-1.6380+005	4.7880+004
	7	7	3.3820+005	2.4610+006	-1.4750+002	-5.3600+006	1.0510+004

20/0.9/30x OPTIMAL CONTROL DESIGN POINT LPI

DV	1	2	3	4	5
	-2.2910-001	-3.2300+000	-1.3410+000	-6.8840+000	7.8970+002
	-0.4530-004	-1.3500-001	9.1740-002	2.5940-002	8.6940+001
	-2.0190-001	1.6580+001	-7.2780-001	-2.8490+000	5.9800+002
	-3.2190-005	-1.4330-002	-4.0680-003	1.8800-003	-7.6420-002
	-1.6370-005	1.2440-003	7.2350-004	-3.4980-003	-1.3520-001
	-2.0440-005	3.4490-003	1.0270-004	1.0390-004	1.4270-001
	-1.0420-006	2.2440-003	2.0440-004	3.6540-005	3.2450-002
A	1	2	3	4	5
	2.0000-004	0.0000	0.0000	0.0000	0.0000
	0.0000	1.0000-005	0.0000	0.0000	0.0000
	0.0000	0.0000	2.0000-002	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	8.0000-001
B	1	2	3	4	5
	1.0000-004	0.0000	0.0000	0.0000	0.0000
	0.0000	2.0000-002	0.0000	0.0000	0.0000
	0.0000	0.0000	4.0000-002	0.0000	0.0000
	0.0000	0.0000	0.0000	4.0000-001	0.0000
	0.0000	0.0000	0.0000	0.0000	2.0000+004

20/0.0/30K OPTIMAL CONTROL DESIGN POINT LPGA
 SYSTEMS CONTROL, INC. (VT) -
 TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

 OPTIMAL CLOSED LOOP EIGENSYSTEM

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-1.41756+0.021)*J(0.00000)	0.00000	1.00000	1 (-9.22497-0.011)*J(0.00000) 2 (-2.65691-0.011)*J(0.00000) 3 (-2.52490-0.031)*J(0.00000) 4 (-7.79684-0.011)*J(0.00000) 5 (1.00000+0.000)*J(0.00000)	-.9224974 -.2656911 -.0025269 -.7796843 1.0000000	.00000 .00000 .00000 .00000 .00000
(-1.06811+0.011)*J(0.00000)	0.00000	1.00000	1 (-3.61898-0.011)*J(0.00000) 2 (-3.13014-0.011)*J(0.00000) 3 (-3.98029-0.031)*J(0.00000) 4 (1.00000+0.000)*J(0.00000) 5 (2.98780-0.031)*J(0.00000)	-.3618981 -.3130138 -.0039603 1.0000000 .0029878	.00000 .00000 .00000 .00000 .00000
(-2.28888+0.000)*J(1.01324+0.000)	2.51283+0.000	.91088	1 (1.00000+0.000)*J(0.00000) 2 (-3.04483+0.011)*J(7.51420-0.011) 3 (9.72923-0.041)*J(-2.37215-0.031) 4 (-1.63704-0.011)*J(-7.26008-0.011) 5 (-4.09269-0.031)*J(2.68796-0.031)	1.0000000 .8107665 .0025639 .7442359 .0048965	.00000 112.05830 -61.69932 -102.70684 146.70425
(-8.73305+0.000)*J(0.00000)	0.00000	1.00000	1 (-5.85583-0.011)*J(0.00000) 2 (-4.27102-0.011)*J(0.00000) 3 (-7.48562-0.031)*J(0.00000) 4 (1.00000+0.000)*J(0.00000) 5 (-2.16101-0.031)*J(0.00000)	-.5855833 -.4271019 -.0074856 1.0000000 -.0021610	.00000 .00000 .00000 .00000 .00000

THE RICCATI MATRIX

SYSTEMS CONTROL, INC. (VI) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

2070.9/30K OPTIMAL CONTROL DESIGN POINT LPG1

	1	2	3	4	5
1	6.3100-005	2.3427-005	-3.0085-003	1.2419-005	7.0594-005
2	2.3667-005	1.4095-005	-1.0187-003	2.1745-005	9.4460-005
3	-3.0085-003	-1.0187-003	2.1694-001	-3.2033-004	-5.5915-004
4	1.2419-005	2.1745-005	-3.2033-004	1.1039-005	5.7577-005
5	7.0594-005	9.4460-005	-5.5915-004	5.7577-005	3.2266-005

CONTROLLER FEEDBACK GAINS

	1	2	3	4	5
1	-5.7448-001	-1.4220+000	1.4240+001	-6.9112-001	8.8628+000
2	-2.3769-004	-7.4510-005	1.7711-002	-1.5095-005	7.8241-004
3	1.4615-003	-7.0275-003	-5.1806-001	-4.8133-003	-4.5255-001
4	-4.4644-003	-2.8453-003	3.1535-002	-3.2621-003	-2.3276-001
5	8.3441-006	2.9904-005	6.6044-004	1.8477-005	1.1410-003

	1	2	3	4	5
1	-1.1450+000	-2.7010-001	-5.0920+002	8.8230-001	1.2540+002
2	-4.4200-002	-1.8170+000	-1.4770+002	2.0020+000	3.9490+001
3	5.0440-003	-7.2730-003	-7.2410+000	1.2150-002	3.9300-001
4	0.0000	0.0000	0.0000	-1.0000+001	0.0000
5	2.3470-001	2.1060+000	1.0760+002	1.5540+000	-1.1790+002

	1	2	3	4	5
1	-4.7990-001	7.7410+001	-4.8320+000	-2.9200+000	5.1110+003
2	-5.2200-001	0.2010+000	-3.3460+000	-1.7770+001	-1.1870+003
3	-2.0450-003	-1.5350+001	2.7440-002	-1.0490-001	-1.4350+001
4	1.0000+001	0.0000	0.0000	0.0000	0.0000
5	-4.2770-001	-5.3170+001	5.8200+000	2.9420+001	-7.1520+003

LOG2

OPTIMAL CONTROL DESIGN POINT

20/0/00

P	1				
	1	2	3	4	5
1	5.7960+001	1.7450+000	-6.2470+003	1.2200+001	6.9370+001
2	-1.9380+000	-5.0010+000	3.1540+003	-5.0140+000	1.1230+002
3	-1.7280+003	-2.1780+002	-2.2580+001	-2.5370+002	6.5630+001
4	0.0000	0.0000	0.0000	-1.0000+001	0.0000
5	1.4540+000	5.3090+000	-2.4140+003	6.4060+000	-1.5080+002

S	1				
	1	2	3	4	5
1	-7.2510+000	-5.2160+003	9.8100+000	1.3620+001	-1.4420+004
2	4.3760+000	5.1720+003	-1.4110+001	-3.9600+001	5.7270+003
3	2.0370+002	2.7120+001	-1.8040+002	-2.0950+001	3.0760+001
4	1.0000+001	0.0000	0.0000	0.0000	0.0000
5	-4.0500+000	-2.3740+003	1.2340+001	5.1280+001	-1.0740+004

WY	1				
	1	2	3	4	5
1	1.8070+002	-3.4050+001	6.1650+002	-2.2540+001	1.1860+001
2	2.6490+002	7.5740+003	-1.8470+001	3.3700+002	-1.2450+001
3	-2.6550+001	-2.2600+001	4.5470+002	5.1540+002	6.0470+001
4	2.6270+004	2.5210+004	-5.9140+001	1.0750+003	-3.9470+003
5	7.1240+004	1.7740+003	-1.4210+000	2.9100+003	-2.5870+002
6	2.3340+004	1.2480+004	-3.8430+001	6.9720+004	-2.5800+003
7	5.1750+005	2.1220+005	-6.7750+002	1.2050+004	-4.6840+004

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

LP2

OPTIMAL CONTROL DESIGN POINT

20/2/04

1	2.3750-001	2.3990+002	7.5720-002	-1.8430+000	1.4800+002
2	-2.1890-002	-1.6320+001	1.6540-001	4.6930-002	-4.8010+001
3	4.1460-001	4.0310+002	-1.8370+000	-3.7320+000	1.0060+003
4	-7.0080-000	-5.2250-001	-2.0950-003	2.1450-003	-1.5480+000
5	-3.9590-003	-1.3170+000	5.8530-003	1.2050-002	-2.7270+000
6	-4.4750-004	-3.4000-001	1.1680-003	9.7800-004	-1.0420+000
7	-7.5700-005	-5.6560-002	3.2510-004	1.4630-004	-1.9960-001

1	1.0000-005	0.0000	0.0000	0.0000	0.0000
2	0.0000	1.0000-004	0.0000	0.0000	0.0000
3	0.0000	0.0000	5.0000-002	0.0000	0.0000
4	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000	0.0000	6.0000-003

1	1.0000-004	0.0000	0.0000	0.0000	0.0000
2	0.0000	1.0000+002	0.0000	0.0000	0.0000
3	0.0000	0.0000	2.0000-002	0.0000	0.0000
4	0.0000	0.0000	0.0000	2.0000-001	0.0000
5	0.0000	0.0000	0.0000	0.0000	1.0000+004

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

20/6/70 OPTIMAL CONTROL DESIGN POINT LOG2

1 OPTIMAL CLOSED LOOP EIGENSYSTEM 1

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-1.51351+0.002)*J(0.00000)	0.00000	1.00000	1 (-5.58548-0.01)*J(0.00000) 2 (-7.25977-0.01)*J(0.00000) 3 (-4.82163-0.03)*J(0.00000) 4 (-7.19496-0.02)*J(0.00000) 5 (1.00000+0.00)*J(0.00000)	-5585477 -7259772 -4046216 -8719496 1.0000000	.00000 .00000 .00000 .00000 .00000
(-9.5230+0.00)*J(0.00000)	0.00000	1.00000	1 (4.00000-0.02)*J(0.00000) 2 (-2.81594-0.01)*J(0.00000) 3 (1.88124-0.03)*J(0.00000) 4 (1.00000+0.00)*J(0.00000) 5 (1.20317-0.03)*J(0.00000)	.0408000 -2815940 -8018412 1.0000000 -8012632	.00000 .00000 .00000 .00000 .00000
(-5.74519+0.00)*J(6.24417-0.01)	5.77927+0.00	.99414	1 (1.00000+0.00)*J(0.00000) 2 (-1.51881-0.01)*J(1.30769-0.02) 3 (1.00060-0.03)*J(-1.21850-0.04) 4 (1.06219-0.01)*J(2.43617-0.02) 5 (-8.16643-0.03)*J(1.56681-0.03)	1.0000000 .1524432 .0010080 .1089770 .0083154	.00000 175.07899 -6.94311 -12.91755 169.13924
(-1.94493+0.00)*J(0.00000)	0.00000	1.00000	1 (-2.00027-0.01)*J(0.00000) 2 (1.00000+0.00)*J(0.00000) 3 (-1.94116-0.04)*J(0.00000) 4 (-7.06431-0.01)*J(0.00000) 5 (2.30265-0.02)*J(0.00000)	-2000266 1.0000000 -8001941 -7064310 .0230265	.00000 .00000 .00000 .00000 .00000

THE OPERATE MATRIX

SYSTEMS CONTROL, INC. (VT) •
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

24/0/04 OPTICAL CONTROL DESIGN POINT LPGA

	1	2	3	4	5
1	2.4058-000	1.1197-000	-1.5279-003	3.2298-006	-4.2043-004
2	1.1197-000	3.0008-005	2.7099-003	2.4459-006	3.9972-005
3	-1.5279-003	2.7099-003	1.4753-000	-2.2004-003	7.3602-003
4	3.2298-006	2.4459-006	-2.2004-003	4.9034-006	-5.1611-006
5	-4.2043-004	3.9972-005	7.3602-003	-5.1611-006	8.6130-005

CONTROLLED FEEDBACK GAINS

	1	2	3	4	5
1	-2.7568-002	-2.7334-001	-1.1290-001	-1.2320-001	4.5135-001
2	1.5472-005	-1.4358-004	4.7942-003	-2.5292-005	5.3608-004
3	4.2607-004	2.6622-003	-5.0810-001	1.3346-003	-1.6233-002
4	-0.5182-004	-3.1044-004	2.0848-001	-7.2116-004	-6.1730-003
5	3.6842-006	1.6544-005	-3.4793-004	4.4925-006	4.0909-005

F

	1	2	3	4	5
1	5.7960-001	1.7150-000	-6.2070-003	1.2200-001	6.9370-001
2	-1.9380-000	-5.0410-000	3.1540-003	-5.0140-000	1.1230-002
3	-1.7280-003	-2.1780-002	-2.2550-001	-2.5370-002	6.5630-001
4	0.0000	0.0000	0.0000	-1.0000-001	0.0000
5	1.6540-000	5.3490-000	-2.4010-003	6.4040-000	-1.5080-002

282

G

	1	2	3	4	5
1	-7.2510-000	-5.2100-003	9.2100-000	1.3620-001	-1.4420-004
2	4.3760-000	3.1720-003	-1.4110-001	-3.9600-001	5.7270-003
3	2.0370-002	2.9120-001	-1.8060-002	-2.0950-001	3.0760-001
4	1.0000-001	0.0000	0.0000	0.0000	0.0000
5	-4.0500-000	-2.3740-003	1.2340-001	5.1260-001	-1.0740-004

E.2 SUPERSONIC EVALUATION POINT DATA

This section contains closed-loop unnormalized eigensystem using off-design regulator gains from gain schedule algorithm (for open-loop data see Appendix D).

CASE	ALT (FT)	Mn	PLA (DEG)	DESCRIPTION
I	58.5K	2.15	83	Middle Pressure
II	75K	1.8	83	Low Pressure
III	40K	1.2	83	High Pressure

(16th order linear model plus one state for fuel flow lag)

AD-A052 346 SYSTEMS CONTROL INC PALO ALTO CALIF AERONAUTICAL AND--ETC F/G 21/5
F100 MULTIVARIABLE CONTROL SYNTHESIS PROGRAM. VOLUME II. APPEND--ETC(U)
JUN 77 R L DE HOFF, W E HALL, R J ADAMS F33615-75-C-2053
UNCLASSIFIED AFAPL-TR-77-35-VOL-2 NL

SYSTEMS CONTROL INC PALO ALTO CALIF AERONAUTICAL AND--ETC F/G 21/5
F100 MULTIVARIABLE CONTROL SYNTHESIS PROGRAM. VOLUME II. APPEND--ETC(U)
JUN 77 R L DE HOFF, W E HALL, R J ADAMS F33615-75-C-2053
AFAPL-TR-77-35-VOL-2 NL

UNCLASSIFIED

AFAPL-TR-77-35-VOL-2

NL

4 OF 6

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AO52346

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4 of 6
AD
AO52346

SYSTEMS CONTROL, INC. (VI) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

83/58.5K/2.15

OPTSYS CASE I

1 INPUT DATA 1

NUMBER OF STATES = 17
NUMBER OF CONTROLS = 5
NUMBER OF OUTPUTS = 7
NUMBER OF PROCESS NOISE SOURCES = 1
NUMBER OF OBSERVATIONS = 1
NUMBER OF SENSITIVITY PARAMETERS = 0

		1	2	3	4	5	6	7	8	9	10
C	1	5.3000-001	-1.4300+000	-1.0000+001	-3.4200-001	6.2600+000	0.0000	0.0000	0.0000	0.0000	0.0000
	2	-1.3200-004	-5.9200-004	0.2900-002	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	3	9.2700-003	0.0000	0.4100-001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	4	-2.4600-003	6.4100-003	-1.6400-001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	5	2.3000-005	5.2300-005	0.0000	0.0000	0.0000-003	0.0000	0.0000	0.0000	0.0000	0.0000
C	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	2	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	3	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	4	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	5	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

OPTSYS CASE I

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

CLOSED LOOP EIGENSYSTEM FOR GIVEN C

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-6.21546+002)+J(0.00000)	0.00000	1.00000	1 (6.02830-001)+J(0.00000)	.6028340	.00000
			2 (-0.09460-001)+J(0.00000)	.4094598	.00000
			3 (1.81492-003)+J(0.00000)	.0018149	.00000
			4 (-1.63878-002)+J(0.00000)	.0163878	.00000
			5 (1.07033-001)+J(0.00000)	.1070328	.00000
			6 (0.77057-001)+J(0.00000)	.770568	.00000
			7 (-9.07702-001)+J(0.00000)	.9077023	.00000
			8 (-3.76479-003)+J(0.00000)	.0037648	.00000
			9 (-7.14904-003)+J(0.00000)	.0071491	.00000
			10 (-3.95390-003)+J(0.00000)	.0039539	.00000
			11 (5.43225-003)+J(0.00000)	.0054322	.00000
			12 (7.98816-003)+J(0.00000)	.0080799	.00000
			13 (-8.44609-003)+J(0.00000)	.0084461	.00000
			14 (1.00000+000)+J(0.00000)	1.0000000	.00000
			15 (4.82332-002)+J(0.00000)	.0482332	.00000
			16 (1.02989-001)+J(0.00000)	.1029886	.00000
			17 (-3.04423-006)+J(0.00000)	.0000030	.00000

OPTSYS CASE I

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

```

(-1.93532+002)+J( 0.00000 ) 0.00000 1.00000
1 ( 2.34202-001)+J( 0.00000 ) .2342024 .00000
2 ( 7.49172-003)+J( 0.00000 ) .0074917 .00000
3 (-6.16814-004)+J( 0.00000 ) -.0006169 .00000
4 ( 1.31978-001)+J( 0.00000 ) .1319778 .00000
5 (-3.58227-001)+J( 0.00000 ) -.3582267 .00000
6 ( 1.90640-001)+J( 0.00000 ) .1906396 .00000
7 (-1.09708-001)+J( 0.00000 ) -.1097076 .00000
8 (-5.25122-003)+J( 0.00000 ) -.005212 .00000
9 (-1.31822-002)+J( 0.00000 ) -.0131822 .00000
10 ( 1.40502-001)+J( 0.00000 ) .1605019 .00000
11 (-3.46799-001)+J( 0.00000 ) -.3467990 .00000
12 (-5.02336-003)+J( 0.00000 ) -.0050234 .00000
13 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
14 (-3.26793-001)+J( 0.00000 ) -.3267931 .00000
15 (-1.42933-002)+J( 0.00000 ) -.0142933 .00000
16 (-2.67847-001)+J( 0.00000 ) -.2678473 .00000
17 ( 7.23310-004)+J( 0.00000 ) .0007233 .00000

```

```

(-5.28640+001)+J( 0.00000 ) 1.00000
1 ( 5.28923-002)+J( 0.00000 ) .0528923 .00000
2 ( 1.54064-002)+J( 0.00000 ) .0154064 .00000
3 (-1.59129-005)+J( 0.00000 ) -.0000159 .00000
4 ( 1.34173-002)+J( 0.00000 ) .0134173 .00000
5 ( 1.26714-004)+J( 0.00000 ) .0001267 .00000
6 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
7 ( 4.60736-004)+J( 0.00000 ) .0004607 .00000
8 (-1.09580-003)+J( 0.00000 ) -.0010958 .00000
9 (-1.23115-003)+J( 0.00000 ) -.0012311 .00000
10 (-2.22345-003)+J( 0.00000 ) -.0022345 .00000
11 (-1.92309-001)+J( 0.00000 ) -.1923087 .00000
12 (-2.61238-003)+J( 0.00000 ) -.0026124 .00000
13 ( 1.40417-002)+J( 0.00000 ) .0140417 .00000
14 (-9.32800-001)+J( 0.00000 ) -.9328003 .00000
15 (-3.90004-002)+J( 0.00000 ) -.0390004 .00000
16 (-1.15757-001)+J( 0.00000 ) -.1157566 .00000
17 ( 7.43234-004)+J( 0.00000 ) .0007432 .00000

```

OPTSYS CASE I

SYSTEMS CONTROL, INC. (VT)

TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

```
(-6.42800+001)+J( 0.00000 ) 0.00000 1.00000
1 (-6.32677-002)+J( 0.00000 ) -.0432677 .00000
2 (-3.20361-002)+J( 0.00000 ) -.0320361 .00000
3 (-3.50881-002)+J( 0.00000 ) .0003507 .00000
4 (-2.20336-002)+J( 0.00000 ) -.0220336 .00000
5 (-6.33321-003)+J( 0.00000 ) .0063332 .00000
6 (-3.02099-001)+J( 0.00000 ) -.3020988 .00000
7 (-4.12150-004)+J( 0.00000 ) .0004121 .00000
8 (-1.90637-003)+J( 0.00000 ) .0019064 .00000
9 (-3.47132-003)+J( 0.00000 ) .0034713 .00000
10 (-1.53447-002)+J( 0.00000 ) -.0153443 .00000
11 (-5.42254-001)+J( 0.00000 ) .5422536 .00000
12 (-7.48604-003)+J( 0.00000 ) .0074860 .00000
13 (-1.80016-001)+J( 0.00000 ) -.1800156 .00000
14 (-1.00000+000)+J( 0.00000 ) 1.0000000 .00000
15 (-4.22917-002)+J( 0.00000 ) .0422917 .00000
16 (-2.07054-001)+J( 0.00000 ) .2070542 .00000
17 (-1.35568-003)+J( 0.00000 ) -.0013557 .00000
```

```
(-4.15800+001)+J( 1.61519+000) 0.16212+001 99925
1 (-2.49084-002)+J(-1.64132-002) .0249089 -33.34270
2 (-6.55713-002)+J( 2.89039-003) .0856201 178.06503
3 (-3.89991-004)+J( 2.40400-004) .004575 31.74004
4 (-5.78599-002)+J(-9.66708-003) .0546420 -170.51279
5 (-6.43112-003)+J( 2.56346-003) .0092232 -21.73236
6 (-5.40060-002)+J(-1.49494-002) .0560477 -164.44759
7 (-4.34436-004)+J( 7.06441-004) .0008314 88.17517
8 (-5.41991-006)+J( 9.55564-004) .0009556 90.38896
9 (-5.60596-004)+J( 1.59762-003) .0016932 70.64113
10 (-2.01165-002)+J(-1.32606-002) .0240039 -146.60747
11 (-1.00000+000)+J( 0.00000 ) 1.0000000 .00000
12 (-1.32483-002)+J(-6.17189-005) .0132484 -.24492
13 (-2.17914-001)+J( 4.41937-002) .2233502 11.46430
14 (-2.33345-001)+J( 2.23576-001) .321658 146.22471
15 (-9.54841-003)+J( 9.21394-003) .0132691 146.02116
16 (-1.44155-002)+J( 1.95799-003) .0145478 7.74444
17 (-2.35716-004)+J(-1.40582-003) .0014254 -.99.51832
```


OPTSYS CASE I

SYSTEMS CONTROL, INC. (VI) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

```
(-1.3365e+001)+J( 7.52678+000) 1.53399+001 .87135
1 ( 5.44499-002)+J(-5.09099-001) .5120028 -83.89522
2 (-1.16185-001)+J(-2.39192-001) .2659167 -115.96773
3 (-6.29088-003)+J(-8.24934-003) .0103683 -127.24478
4 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
5 (-2.91980-002)+J( 2.94436-004) .0291995 179.42224
6 (-1.98325-004)+J( 2.53080-001) .2530802 90.08490
7 (-4.00494-003)+J(-8.33031-004) .0060625 -172.10213
8 (-6.34320-002)+J(-5.11644-002) .0814936 -191.11047
9 (-1.27642-001)+J(-8.93122-002) .1557854 -195.01913
10 (-2.50862-001)+J( 2.95975-001) .3879860 130.28346
11 ( 1.11483-001)+J( 6.67093-001) .6763439 80.51251
12 ( 2.71077-003)+J( 7.13957-003) .0076369 69.20912
13 (-8.44292-003)+J( 5.85739-001) .5858003 90.82591
14 ( 7.92437-002)+J( 4.96481-001) .5031599 80.93864
15 ( 5.55285-003)+J( 1.75968-002) .0184522 72.44639
16 ( 1.10290-001)+J( 3.77613-001) .3933494 73.71834
17 (-2.99835-001)+J( 7.40785-002) .3088510 166.12221
```

```
(-2.19122+000)+J( 1.87294+000) 2.89260+000 .76016
1 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
2 (-1.84070-001)+J( 5.77823-001) .6060517 107.64120
3 ( 5.82637-004)+J(-2.98684-003) .0030431 -78.96206
4 (-2.82915-001)+J(-7.25372-001) .7785916 -111.30713
5 ( 7.52728-003)+J( 1.98622-003) .0077849 14.74173
6 (-1.06677-001)+J(-1.76941-001) .2066104 -121.04572
7 ( 1.45020-003)+J(-4.25468-004) .0019531 -18.67892
8 ( 3.57205-002)+J(-2.15969-002) .0417418 -31.15785
9 ( 4.08771-002)+J(-5.13356-002) .0656222 -51.47066
10 ( 3.00662-002)+J( 2.21780-002) .0373409 35.01401
11 (-8.04691-002)+J(-2.06037-001) .2211936 -111.33342
12 (-4.08812-003)+J( 2.06918-003) .0045819 153.15399
13 (-8.33289-002)+J(-2.46264-001) .2599799 -108.69802
14 (-6.38385-002)+J(-1.85072-001) .1195770 -109.03129
15 ( 1.54320-002)+J(-2.38153-003) .0156151 -171.22730
16 (-1.07930-001)+J(-2.74311-001) .2947799 -111.47761
17 ( 3.43982-002)+J(-6.13241-002) .0723538 -57.95719
```


OPISYS CASE 1

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

(-1.00790+001)+J(0.00000	1.00000	1.00000	1	(-1.22532-001)+J(0.00000)	-1.225323	.00000
			2	(-1.54087-001)+J(0.00000)	-1.540866	.00000
			3	(1.19959+003)+J(0.00000)	.0011996	.00000
			4	(1.00000+000)+J(0.00000)	1.0000000	.00000
			5	(1.10340-002)+J(0.00000)	.0110340	.00000
			6	(5.21869-001)+J(0.00000)	.5218685	.00000
			7	(3.58946-003)+J(0.00000)	.0035895	.00000
			8	(-1.37787-003)+J(0.00000)	-.0013779	.00000
			9	(1.00663-002)+J(0.00000)	.0100663	.00000
			10	(6.59637-002)+J(0.00000)	.0659637	.00000
			11	(6.99343-001)+J(0.00000)	.6993432	.00000
			12	(5.59275-003)+J(0.00000)	.0055928	.00000
			13	(6.93806-001)+J(0.00000)	.6938063	.00000
			14	(5.36338-001)+J(0.00000)	.5363375	.00000
			15	(1.49799-002)+J(0.00000)	.0149799	.00000
			16	(9.35549-001)+J(0.00000)	.9355486	.00000
			17	(2.09926-002)+J(0.00000)	.0209926	.00000
(-2.15278+001)+J(7.76000-001)	2.15410+001	.99935	1	(9.57410-003)+J(-1.40644-002))	.0170130	-55.74552
			2	(1.63192-002)+J(-3.50775-002))	.0386870	-65.08070
			3	(-1.76346-003)+J(-5.66672-004))	.0018523	-162.14540
			4	(8.31612-002)+J(-4.69555-002))	.0955010	-29.45087
			5	(7.63382-003)+J(-4.99443-003))	.0086606	-109.49016
			6	(4.52000-001)+J(-3.14640-001))	.5507292	-14.84200
			7	(-1.92328-003)+J(-1.07556-003))	.0022036	-150.78466
			8	(1.93075-002)+J(0.62043-003))	.0198526	13.48828
			9	(5.10943-002)+J(0.15821-003))	.0517415	9.07183
			10	(-1.07933-001)+J(9.57005-002))	.1442505	138.43782
			11	(-2.07179-001)+J(1.00451-001))	.2302871	154.13351
			12	(-2.42140-003)+J(1.20267-003))	.0027036	153.54703
			13	(-1.39211-001)+J(5.03399-002))	.1480333	160.11960
			14	(-1.37640-001)+J(7.97851-002))	.1590924	149.90060
			15	(-5.15735-003)+J(3.03737-003))	.0059653	149.50447
			16	(1.00000+000)+J(0.00000)	1.0000000	.00000
			17	(8.74987-001)+J(4.55921-001))	.5951836	-143.27019

OPTSYS CASE I

SYSTEMS CONTROL INC.(VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

```
(-1.81243+001)+J( 0.00000 ) 0.00000 1.00000
```

1	(8.1477-003)+J(0.00000)	.0081468	.00000
2	(3.29687-003)+J(0.00000)	.0032969	.00000
3	(1.29033-003)+J(0.00000)	.0012903	.00000
4	(-8.57141-002)+J(0.00000)	-.0857141	.00000
5	(9.67336-003)+J(0.00000)	.0096734	.00000
6	(2.82626-001)+J(0.00000)	.2826263	.00000
7	(2.25087-003)+J(0.00000)	.0022509	.00000
8	(-2.29239-002)+J(0.00000)	-.0229239	.00000
9	(-5.05043-002)+J(0.00000)	-.0505043	.00000
10	(7.58269-002)+J(0.00000)	.0758269	.00000
11	(1.89525-001)+J(0.00000)	.1895250	.00000
12	(2.11114-003)+J(0.00000)	.0021111	.00000
13	(1.47235-001)+J(0.00000)	.1472346	.00000
14	(1.25960-001)+J(0.00000)	.1259600	.00000
15	(4.55475-003)+J(0.00000)	.0045547	.00000
16	(1.00000+000)+J(0.00000)	1.0000000	.00000
17	(-6.26690-001)+J(0.00000)	-.6266904	.00000

```
(-1.77922+000)+J( 0.00000 ) 0.00000 1.00000
```

1	(6.93112-001)+J(0.00000)	.6931122	.00000
2	(-9.48243-001)+J(0.00000)	-.9482431	.00000
3	(1.94254-003)+J(0.00000)	.0019425	.00000
4	(1.00000+000)+J(0.00000)	1.0000000	.00000
5	(7.91715-003)+J(0.00000)	.0079142	.00000
6	(1.44065-001)+J(0.00000)	.1440650	.00000
7	(3.23909-003)+J(0.00000)	.0032391	.00000
8	(3.91497-002)+J(0.00000)	.0381497	.00000
9	(6.66126-002)+J(0.00000)	.0666126	.00000
10	(6.64529-003)+J(0.00000)	.006453	.00000
11	(4.10088-001)+J(0.00000)	.4100884	.00000
12	(-1.75828-002)+J(0.00000)	-.0175828	.00000
13	(8.91953-001)+J(0.00000)	.8919530	.00000
14	(3.48761-001)+J(0.00000)	.3487609	.00000
15	(2.26454-001)+J(0.00000)	.2264536	.00000
16	(3.46413-001)+J(0.00000)	.3464128	.00000
17	(7.17262-002)+J(0.00000)	.0717262	.00000

OPTSYS CASE I

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

(-2.01525+0i1)+J(0.00000)	0.00000	1.00000	1 (2.03333-002)+J(0.00000)	.0203333	.00000
			2 (6.78019-002)+J(0.00000)	.0678019	.00000
			3 (3.44766-003)+J(0.00000)	.0034477	.00000
			4 (3.44645-002)+J(0.00000)	.0344645	.00000
			5 (2.18102-002)+J(0.00000)	.0218102	.00000
			6 (2.91764-001)+J(0.00000)	.2917636	.00000
			7 (5.35647-003)+J(0.00000)	.0053565	.00000
			8 (-5.46227-002)+J(0.00000)	-.0546227	.00000
			9 (-7.22804-003)+J(0.00000)	-.0072280	.00000
			10 (-9.40760-002)+J(0.00000)	-.0940760	.00000
			11 (4.37533-002)+J(0.00000)	.0437533	.00000
			12 (5.05518-004)+J(0.00000)	.0005055	.00000
			13 (6.20675-002)+J(0.00000)	.0620675	.00000
			14 (-4.09261-003)+J(0.00000)	-.0049261	.00000
			15 (-1.81300-004)+J(0.00000)	-.0001813	.00000
			16 (-6.39094-001)+J(0.00000)	-.6390944	.00000
			17 (1.00000+000)+J(0.00000)	1.0000000	.00000
(-6.02539-001)+J(0.00000)	0.00000	1.00000	1 (1.00000+000)+J(0.00000)	1.0000000	.00000
			2 (-1.55177-001)+J(0.00000)	-.1551773	.00000
			3 (-1.31280-003)+J(0.00000)	-.0013128	.00000
			4 (-1.36734-001)+J(0.00000)	-.1367342	.00000
			5 (1.38503-002)+J(0.00000)	.0138503	.00000
			6 (1.19702-001)+J(0.00000)	.1197019	.00000
			7 (2.67215-003)+J(0.00000)	.0026722	.00000
			8 (-2.56532-002)+J(0.00000)	-.0256532	.00000
			9 (1.99705-002)+J(0.00000)	.0199745	.00000
			10 (5.61778-002)+J(0.00000)	.0561778	.00000
			11 (8.72924-002)+J(0.00000)	.0872928	.00000
			12 (2.33468-001)+J(0.00000)	.2334685	.00000
			13 (1.11486-001)+J(0.00000)	.1114855	.00000
			14 (9.81632-003)+J(0.00000)	.0098163	.00000
			15 (1.35911-003)+J(0.00000)	.0013591	.00000
			16 (-7.14789-002)+J(0.00000)	-.0714789	.00000
			17 (1.95391-002)+J(0.00000)	.0195391	.00000

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

83/75K/1.8

OPTSYS CASE II

1 INPUT DATA 1

NUMBER OF STATES = 17
NUMBER OF CONTROLS = 5
NUMBER OF OUTPUTS = 7
NUMBER OF PROCESS NOISE SOURCES = 1
NUMBER OF OBSERVATIONS = 1
NUMBER OF SENSITIVITY PARAMETERS = 0

	1	2	3	4	5	6	7	8	9	10
1	-7.3000-001	-1.1300+000	-3.7000+000	-5.8200-001	6.2600+000	0.0000	0.0000	0.0000	0.0000	0.0000
2	-0.3200-004	-2.2000-005	6.3700-002	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
3	0.2700-003	0.0000	-7.0700-001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4	-2.0600-003	6.8100-003	-1.6000-001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5	2.3000-005	5.8300-005	0.0000	0.0000	4.0000-003	0.0000	0.0000	0.0000	0.0000	0.0000

	11	12	13	14	15	16	17
1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
2	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
3	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

SYSTEMS CONTROL, INC. (VI) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

OPTSYS CASE II

↑
↑ CLOSED LOOP EIGENSYSTEM FOR GIVEN C ↑
↑

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-5.30273+002)+J(0.00000)	0.00000	1.00000	1 (2.10450-001)+J(0.00000)	.210475	.00000
			2 (-1.09356-001)+J(0.00000)	-.100361	.00000
			3 (1.05687-003)+J(0.00000)	.0010569	.00000
			4 (5.53021-003)+J(0.00000)	.0055382	.00000
			5 (-3.86418-002)+J(0.00000)	-.0386418	.00000
			6 (6.35060-001)+J(0.00000)	.6350645	.00000
			7 (-2.61749-001)+J(0.00000)	-.2617486	.00000
			8 (3.13406-003)+J(0.00000)	.0031349	.00000
			9 (9.25586-003)+J(0.00000)	.0092559	.00000
			10 (3.28556-003)+J(0.00000)	.0032856	.00000
			11 (3.08718-003)+J(0.00000)	.0030872	.00000
			12 (4.40064-005)+J(0.00000)	.0000440	.00000
			13 (-6.44438-002)+J(0.00000)	-.0644438	.00000
			14 (1.00000+000)+J(0.00000)	1.0000000	.00000
			15 (4.41955-002)+J(0.00000)	.0441955	.00000
			16 (1.26650-001)+J(0.00000)	.1266500	.00000
			17 (-4.66893-005)+J(0.00000)	-.0000867	.00000

OPTSYS CASE II

SYSTEMS CONTROL, INC. (VI) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

```
(-2.39713+002)+J( 0.00000 ) 0.00000 1.00000
1 ( 2.60815-001)+J( 0.00000 ) .2608146 .00000
2 ( 4.88731-002)+J( 0.00000 ) .0488731 .00000
3 ( 1.47358-003)+J( 0.00000 ) .0014736 .00000
4 ( 9.76496-002)+J( 0.00000 ) .0976496 .00000
5 (-3.12263-001)+J( 0.00000 ) -.3122628 .00000
6 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
7 ( 1.49999-001)+J( 0.00000 ) .1499995 .00000
8 ( 8.50275-003)+J( 0.00000 ) .0085027 .00000
9 ( 2.79076-002)+J( 0.00000 ) .0279076 .00000
10 ( 2.18654-001)+J( 0.00000 ) .2186536 .00000
11 (-1.45273-001)+J( 0.00000 ) -.1452733 .00000
12 (-2.11549-003)+J( 0.00000 ) -.0021155 .00000
13 ( 4.26952-001)+J( 0.00000 ) .4269521 .00000
14 ( 4.62587-001)+J( 0.00000 ) .4625874 .00000
15 ( 2.03127-002)+J( 0.00000 ) .0203127 .00000
16 (-1.91580-001)+J( 0.00000 ) -.1915801 .00000
17 (-2.19637-003)+J( 0.00000 ) -.0021964 .00000
```

```
(-4.95184+001)+J( 9.96248+000 ) 5.05106+001 .98036
1 (-1.94715-002)+J(-8.17359-003) .0211174 -157.22868
2 (-1.73075-002)+J( 1.17001-002) .0208912 145.92085
3 (-2.21318-005)+J( 7.14198-006) .0000233 162.11504
4 (-4.59561-003)+J(-2.74091-003) .0053509 -149.18745
5 (-2.35101-003)+J( 1.99473-003) .0030432 139.86691
6 (-2.19699-001)+J(-3.78934-001) .4380169 -120.10437
7 (-4.05833-004)+J( 8.27839-004) .0009220 116.11557
8 (-8.07105-004)+J( 4.58477-004) .0009282 150.40118
9 (-3.09790-003)+J( 5.80560-004) .0031518 169.34562
10 ( 2.09496-002)+J(-7.37100-003) .0222085 -19.38417
11 ( 5.45024-001)+J(-4.81725-001) .7273094 -41.47221
12 ( 7.26210-003)+J(-6.66873-003) .0098595 -42.56102
13 ( 1.22419-001)+J( 1.34273-001) .1817035 87.64406
14 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
15 ( 4.17572-002)+J(-5.63905-004) .0417610 .77370
16 ( 1.28814-001)+J(-9.34903-002) .1591653 -15.97119
17 ( 1.86833-003)+J( 2.12045-004) .0018803 6.87593
```


OPTSYS CASE 11

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

```
(-5.25642+001)+J( 0.00000 ) 0.00000 1.00000
1 ( 1.44362-002)+J( 0.00000 ) .0144362 .00000
2 ( 4.06080-003)+J( 0.00000 ) .0040608 .00000
3 ( 1.45853-005)+J( 0.00000 ) .0000145 .00000
4 ( 4.49832-003)+J( 0.00000 ) .0044983 .00000
5 (-1.25760-004)+J( 0.00000 ) -.0001258 .00000
6 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
7 ( 1.18349-004)+J( 0.00000 ) .0001183 .00000
8 (-5.71188-004)+J( 0.00000 ) -.0005712 .00000
9 (-8.02505-004)+J( 0.00000 ) -.0008025 .00000
10 ( 1.59982-003)+J( 0.00000 ) .0015998 .00000
11 (-1.45415-001)+J( 0.00000 ) -.1454152 .00000
12 (-1.97420-003)+J( 0.00000 ) -.0019742 .00000
13 ( 9.12851-003)+J( 0.00000 ) .0091285 .00000
14 (-7.79371-001)+J( 0.00000 ) -.7793714 .00000
15 (-3.25843-002)+J( 0.00000 ) -.0325843 .00000
16 (-1.06660-001)+J( 0.00000 ) -.1066699 .00000
17 ( 4.74932-004)+J( 0.00000 ) .0004749 .00000
```

```
(-4.47644+001)+J( 0.00000 ) 0.00000 1.00000
1 (-2.61514-002)+J( 0.00000 ) .0261514 .00000
2 ( 2.90493-002)+J( 0.00000 ) .0290493 .00000
3 (-1.57588-006)+J( 0.00000 ) -.0000016 .00000
4 ( 8.19414-003)+J( 0.00000 ) .0081942 .00000
5 (-1.85735-003)+J( 0.00000 ) -.0018574 .00000
6 ( 2.88431-001)+J( 0.00000 ) .2884307 .00000
7 ( 1.03607-004)+J( 0.00000 ) .0001036 .00000
8 ( 1.89803-004)+J( 0.00000 ) .0001898 .00000
9 (-4.83307-004)+J( 0.00000 ) -.0004833 .00000
10 ( 1.14680-002)+J( 0.00000 ) .0114680 .00000
11 (-9.68096-001)+J( 0.00000 ) -.9680957 .00000
12 (-1.29310-002)+J( 0.00000 ) -.0129310 .00000
13 (-1.31504-001)+J( 0.00000 ) -.1315038 .00000
14 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
15 ( 4.13274-002)+J( 0.00000 ) .0413274 .00000
16 ( 4.09357-002)+J( 0.00000 ) .0409357 .00000
17 ( 3.70548-004)+J( 0.00000 ) .0003705 .00000
```

OPTSYS CASE II

SYSTEMS CONTROL, INC. (VI) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

(-1.99294+001)+J(3.15973+000)	2.00811+001	99746	1	(-1.17575-002)+J(-2.28896-002)	.0257327	-117.18780
			2	(-1.31158-003)+J(-2.62208-002)	.0262532	-92.84353
			3	(-8.39373-004)+J(-3.49983-004)	.0009094	-157.36595
			4	(4.14709-002)+J(-3.62682-002)	.0566136	-39.83857
			5	(-4.44058-003)+J(-1.92681-003)	.0048008	-156.58786
			6	(-1.00000+000)+J(0.00000)	1.0000000	.00000
			7	(-5.56045-004)+J(-1.91881-004)	.0006835	-143.69674
			8	(-5.87922-003)+J(1.56518-002)	.0167196	110.58784
			9	(4.32596-003)+J(4.47990-002)	.0450074	80.44481
			10	(-4.11470-002)+J(2.34183-001)	.2377704	99.94540
			11	(4.74920-002)+J(3.79408-001)	.3823651	82.84511
			12	(7.54210-004)+J(4.35688-003)	.0048217	80.17893
			13	(7.88039-003)+J(2.53492-001)	.2536140	88.21941
			14	(5.98603-002)+J(3.00582-001)	.3064942	78.73700
			15	(2.61413-003)+J(1.11015-002)	.0114051	76.74959
			16	(9.13702-001)+J(1.49713-001)	.9258858	9.30539
			17	(2.87839-001)+J(-1.03609-002)	.2880254	-2.06151
(-1.99575+001)+J(0.00000)	0.00000	1.00000	1	(3.46335-003)+J(0.00000)	.0034634	.00000
			2	(-1.10387-002)+J(0.00000)	-.0110387	.00000
			3	(-9.43741-004)+J(0.00000)	-.0009437	.00000
			4	(4.63354-002)+J(0.00000)	.0463354	.00000
			5	(-6.68942-003)+J(0.00000)	-.0066894	.00000
			6	(9.87720-001)+J(0.00000)	.9877204	.00000
			7	(-1.33570-003)+J(0.00000)	-.0013357	.00000
			8	(5.93565-002)+J(0.00000)	.0593565	.00000
			9	(1.68698-003)+J(0.00000)	.0016870	.00000
			10	(-1.31893-001)+J(0.00000)	-.1318932	.00000
			11	(4.73881-003)+J(0.00000)	.0047388	.00000
			12	(5.50310-005)+J(0.00000)	.0000550	.00000
			13	(1.78773-002)+J(0.00000)	.0178773	.00000
			14	(2.63423-002)+J(0.00000)	.0263423	.00000
			15	(9.76544-004)+J(0.00000)	.0009765	.00000
			16	(1.00000+000)+J(0.00000)	1.0000000	.00000
			17	(2.55633-001)+J(0.00000)	.2556334	.00000

OPTSYS CASE II

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

```
(-1.51734+001)+J( 0.00000 ) 0.00000 1.00000
1 (-5.60226-004)+J( 0.00000 ) -.0006602 .00000
2 (-9.71404-004)+J( 0.00000 ) -.0009714 .00000
3 (-3.70357-004)+J( 0.00000 ) -.0003703 .00000
4 (-4.09691-002)+J( 0.00000 ) .0409691 .00000
5 (-3.45124-003)+J( 0.00000 ) -.0034512 .00000
6 (-2.96466-001)+J( 0.00000 ) .2964662 .00000
7 (-6.11201-004)+J( 0.00000 ) -.0006112 .00000
8 (-2.84110-002)+J( 0.00000 ) .0284110 .00000
9 (-8.21888-002)+J( 0.00000 ) .0821888 .00000
10 (-1.07791-001)+J( 0.00000 ) -.1077906 .00000
11 (-9.20172-002)+J( 0.00000 ) -.0920172 .00000
12 (-1.02874-003)+J( 0.00000 ) -.0010287 .00000
13 (-5.98769-002)+J( 0.00000 ) -.0598769 .00000
14 (-5.16320-002)+J( 0.00000 ) -.0516320 .00000
15 (-1.87798-003)+J( 0.00000 ) -.0018780 .00000
16 (-6.40007-001)+J( 0.00000 ) -.6400071 .00000
17 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
```

```
(-9.19609+000)+J( 2.72153+000 ) 9.50120+000 .95890
1 (-1.59971-001)+J(-1.34556-001) .2090364 -139.93183
2 (-8.90354-002)+J(-5.4062-003) .0892027 -176.40000
3 (-1.49658-003)+J(-1.43439-002) .0020730 -136.21598
4 ( 5.07988-001)+J(-5.70319-002) .5111796 -6.40578
5 ( 4.38322-003)+J( 3.48308-004) .0043970 0.50300
6 ( 2.76208-001)+J(-3.20444-001) .4232056 -49.25784
7 ( 1.18382-003)+J(-3.82675-002) .0012441 -17.91359
8 (-3.17629-002)+J(-2.75986-002) .0420781 -119.01279
9 (-8.52843-002)+J(-5.48634-002) .1014071 -107.28845
10 ( 7.71456-002)+J( 1.52703-002) .0786423 11.10805
11 ( 9.81105-001)+J(-6.28722-002) .9831178 -3.66667
12 ( 7.68515-003)+J(-2.64386-003) .0081272 -18.94236
13 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
14 ( 7.50593-001)+J(-5.49625-002) .7527028 -4.18287
15 ( 2.08591-002)+J(-6.14727-003) .0217460 -16.42089
16 ( 7.43756-001)+J(-3.66867-001) .8293159 -26.25520
17 (-1.71641-001)+J(-5.06434-002) .1013022 -161.13654
```

OPTSYN CASE II

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

(-7.62386-001)+J(0.00000)	0.00000	1.00000	1	(-6.08453-001)+J(0.00000)	-6084535	.00000
			2	(-1.00000+000)+J(0.00000)	1.0000000	.00000
			3	(-1.13318-003)+J(0.00000)	-0011332	.00000
			4	(-5.58602-001)+J(0.00000)	-5586021	.00000
			5	(-7.63017-003)+J(0.00000)	-0076302	.00000
			6	(-2.50535-001)+J(0.00000)	-2505348	.00000
			7	(-1.98741-003)+J(0.00000)	-0019874	.00000
			8	(-4.51386-002)+J(0.00000)	-0451386	.00000
			9	(-6.60111-002)+J(0.00000)	-0660111	.00000
			10	(-4.23412-002)+J(0.00000)	-0423412	.00000
			11	(-5.83242-001)+J(0.00000)	-5832425	.00000
			12	(-3.83416-001)+J(0.00000)	-3834156	.00000
			13	(-7.26456-001)+J(0.00000)	-7264556	.00000
			14	(-5.39283-001)+J(0.00000)	-5392828	.00000
			15	(-8.20833-002)+J(0.00000)	-0820833	.00000
			16	(-5.59817-001)+J(0.00000)	-5598165	.00000
			17	(-6.74696-002)+J(0.00000)	-0674696	.00000

(-1.21352+000)+J(0.00000)	0.00000	1.00000	1	(-7.19027-001)+J(0.00000)	-7190266	.00000
			2	(-1.00000+000)+J(0.00000)	1.0000000	.00000
			3	(-1.25627-003)+J(0.00000)	-0012563	.00000
			4	(-4.96717-001)+J(0.00000)	-4967170	.00000
			5	(-4.10912-003)+J(0.00000)	-0041091	.00000
			6	(-2.13429-001)+J(0.00000)	-2134291	.00000
			7	(-1.35280-003)+J(0.00000)	-0013528	.00000
			8	(-5.02708-002)+J(0.00000)	-0502708	.00000
			9	(-8.36223-002)+J(0.00000)	-0836223	.00000
			10	(-8.27097-002)+J(0.00000)	-0827097	.00000
			11	(-4.41899-001)+J(0.00000)	-4418992	.00000
			12	(-4.50393-002)+J(0.00000)	-0450393	.00000
			13	(-5.50198-001)+J(0.00000)	-5501980	.00000
			14	(-3.75450-001)+J(0.00000)	-3754501	.00000
			15	(-8.03421-002)+J(0.00000)	-0803421	.00000
			16	(-4.30135-001)+J(0.00000)	-4301347	.00000
			17	(-8.75722-002)+J(0.00000)	-0875722	.00000

OPTSYS CASE II

SYSTEMS CONTROL, INC. (VT) -
TIME ONMATH SYNTHESIS AND ANALYSIS PROGRAM

(-2.12805+0001)+J(3.20066-001)	2.15288+000	.98846	1	(-3.55599-001)+J(1.25055-001)	.376981	140.65489
			2	(-4.15508-001)+J(-4.76800-002)	.4182345	-173.45348
			3	(2.74040-004)+J(1.00403-004)	.0002919	20.12182
			4	(6.60478-001)+J(-1.72601-002)	.6615289	-3.22885
			5	(7.24378-003)+J(2.51682-003)	.0076886	19.15958
			6	(3.19843-001)+J(-9.08314-003)	.3199718	-1.62669
			7	(1.69190-003)+J(2.81364-004)	.0017152	9.48143
			8	(-6.71942-003)+J(4.52398-003)	.0081034	146.08843
			9	(-1.15399-002)+J(3.83028-003)	.0121570	161.63823
			10	(3.40994-002)+J(2.06596-002)	.0398896	31.21017
			11	(9.36275-001)+J(-5.13567-003)	.8362912	-35186
			12	(-2.27258-002)+J(-7.69233-003)	.0239924	-161.29981
			13	(1.00000+000)+J(0.00000)	1.0000000	.00000
			14	(6.63134-001)+J(-1.79734-002)	.6633774	-1.55255
			15	(-6.89341-002)+J(-2.33477-001)	.2434412	-106.44921
			16	(6.91505-001)+J(1.17931-002)	.6916052	.97704
			17	(-1.26555-002)+J(4.51276-003)	.0134360	160.37454

(-2.28947+001)+J(0.00000)	0.00000	1.00000	1	(2.32605-002)+J(0.00000)	.0232605	.00000
			2	(1.69582-002)+J(0.00000)	.0169582	.00000
			3	(-1.12790-004)+J(0.00000)	-.0001128	.00000
			4	(4.14630-002)+J(0.00000)	.0414630	.00000
			5	(2.26214-004)+J(0.00000)	.0002262	.00000
			6	(1.34015-001)+J(0.00000)	.1340145	.00000
			7	(-3.35380-004)+J(0.00000)	-.0003354	.00000
			8	(1.76905-002)+J(0.00000)	.0176905	.00000
			9	(8.29425-002)+J(0.00000)	.0829425	.00000
			10	(-2.84451-001)+J(0.00000)	-.2844510	.00000
			11	(-3.19777-001)+J(0.00000)	-.3197772	.00000
			12	(-3.77876-003)+J(0.00000)	-.0037788	.00000
			13	(-1.79733-001)+J(0.00000)	-.1797327	.00000
			14	(-2.65867-001)+J(0.00000)	-.2658670	.00000
			15	(-1.00467-002)+J(0.00000)	-.0100467	.00000
			16	(1.00000+000)+J(0.00000)	1.0000000	.00000
			17	(-7.71361-001)+J(0.00000)	-.7713607	.00000

OPTSYS CAGE YII

83/40K/2.2

300

	1	2	3	4	5	6	7	8	9	10
1	-4.1600-002	-2.1200+000	-2.9400+001	-3.4200-001	6.2600+000	0.0000	0.0000	0.0000	0.0000	0.0000
2	-1.4800-003	-3.4000-008	3.3500-002	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
3	5.1900-003	0.0000	-2.9300-001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4	-2.9600-003	-6.1300-003	-1.2400-001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5	-2.3000-005	5.4300-005	0.0000	0.0000	2.0600-003	0.0000	0.0000	0.0000	0.0000	0.0000

[illegible]

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

OPRAYS CASE III

↑-----↑
↑ CLOSED LOOP EIGENSYSTEM FOR GIVEN C ↑
↑-----↑

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-6.00079+002)+J(0.00000)	0.00000	1.00000	1 (-7.23348-001)+J(0.00000)	-.7233480	.00000
			2 (3.00321-001)+J(0.00000)	.3903210	.00000
			3 (-1.00402-003)+J(0.00000)	-.0018640	.00000
			4 (1.23061-002)+J(0.00000)	.0123061	.00000
			5 (9.93382-004)+J(0.00000)	.0009954	.00000
			6 (-2.42665-001)+J(0.00000)	-.2426645	.00000
			7 (1.00000+000)+J(0.00000)	1.0000000	.00000
			8 (3.64109-004)+J(0.00000)	.0003641	.00000
			9 (-3.35097-004)+J(0.00000)	-.0003351	.00000
			10 (-6.29511-004)+J(0.00000)	-.0006295	.00000
			11 (2.59043-004)+J(0.00000)	.0002598	.00000
			12 (3.54229-006)+J(0.00000)	.0000035	.00000
			13 (-2.71593-004)+J(0.00000)	-.0002716	.00000
			14 (-4.27399-001)+J(0.00000)	-.4273988	.00000
			15 (-1.89062-002)+J(0.00000)	-.0189062	.00000
			16 (-3.49738-002)+J(0.00000)	-.0349738	.00000
			17 (5.34005-006)+J(0.00000)	.0000053	.00000

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(-2.7A5A0+003)+J(0.00000)	0.00000	1.00000	1	(-6.92478-001)+J(0.00000)	-6.924778	0.00000
			2	(-9.16737-002)+J(0.00000)	-9.16737	0.00000
			3	(2.14099-003)+J(0.00000)	2.1410	0.00000
			4	(-2.42214-001)+J(0.00000)	-2.422144	0.00000
			5	(1.00000+000)+J(0.00000)	1.0000000	0.00000
			6	(-2.99410-001)+J(0.00000)	-2.994101	0.00000
			7	(4.24454-001)+J(0.00000)	4.244538	0.00000
			8	(-1.61682-004)+J(0.00000)	-0.001519	0.00000
			9	(-4.04628-003)+J(0.00000)	-4.046283	0.00000
			10	(-1.06987-001)+J(0.00000)	-1.069873	0.00000
			11	(1.69200-001)+J(0.00000)	1.692003	0.00000
			12	(2.46701-003)+J(0.00000)	2.4670	0.00000
			13	(-6.69370-001)+J(0.00000)	-6.693704	0.00000
			14	(2.67216-002)+J(0.00000)	2.67216	0.00000
			15	(1.17113-003)+J(0.00000)	1.17111	0.00000
			16	(1.50763-001)+J(0.00000)	1.507626	0.00000
			17	(4.91418-004)+J(0.00000)	4.91418	0.00000
(-4.86148+001)+J(7.55549+000)	4.91994+001	.98814	1	(-1.48891-001)+J(-4.38631-002)	1.552178	-163.54511
			2	(-7.82618-002)+J(1.17379-001)	1410773	123.69309
			3	(1.81980-003)+J(-6.20461-004)	0.019227	-18.82678
			4	(-5.32282-002)+J(5.85801-002)	0.0791509	132.25950
			5	(3.09291-003)+J(-2.57895-003)	0.040270	-39.85227
			6	(-2.29305-001)+J(-8.16414-001)	8753715	-118.88034
			7	(4.22377-004)+J(2.08893-003)	0.021312	78.56907
			8	(1.53847-003)+J(1.79812-003)	0.023665	49.4477
			9	(-6.36660-004)+J(1.71442-003)	0.018288	110.37283
			10	(-3.32414-003)+J(-5.18615-003)	0.061601	-122.68875
			11	(3.05300-001)+J(-5.49572-001)	6286791	-40.94680
			12	(4.01140-003)+J(-7.48746-003)	0.084943	-61.81989
			13	(1.14872-001)+J(3.96289-002)	1215154	19.03354
			14	(1.00000+000)+J(0.00000)	1.0000000	0.00000
			15	(4.16666-002)+J(-4.50558-004)	0.0416891	-61.954
			16	(8.97266-002)+J(-8.52783-002)	1237871	-43.54398
			17	(5.54067-004)+J(-1.02733-003)	0.011672	-61.64069

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```
(-5.00975+001)+J( 0.00000 ) 0.00000 1.00000
```

1	(5.62757-002)+J(0.00000)	.0662757	.00000
2	(5.48193-003)+J(0.00000)	.0054819	.00000
3	(8.45730-004)+J(0.00000)	.0008457	.00000
4	(8.53634-003)+J(0.00000)	.0085363	.00000
5	(1.59883-003)+J(0.00000)	.0015988	.00000
6	(1.00000+000)+J(0.00000)	1.0000000	.00000
7	(5.67095-004)+J(0.00000)	.0006675	.00000
8	(-1.94541-003)+J(0.00000)	-.0019454	.00000
9	(-2.67971-003)+J(0.00000)	-.0026797	.00000
10	(3.41129-003)+J(0.00000)	.0034113	.00000
11	(-2.65259-002)+J(0.00000)	-.0265259	.00000
12	(-3.59325-004)+J(0.00000)	-.0003593	.00000
13	(8.25953-004)+J(0.00000)	.0008270	.00000
14	(-3.47616-001)+J(0.00000)	-.3476158	.00000
15	(-1.45058-002)+J(0.00000)	-.0145058	.00000
16	(-4.09197-002)+J(0.00000)	-.0409197	.00000
17	(1.70855-003)+J(0.00000)	.0017086	.00000

```
(-4.91898+001)+J( 0.00000 ) 0.00000 1.00000
```

1	(-3.64129-002)+J(0.00000)	-.0364129	.00000
2	(5.07253-003)+J(0.00000)	.0050725	.00000
3	(1.94662-003)+J(0.00000)	.0019466	.00000
4	(1.69018-002)+J(0.00000)	.0169018	.00000
5	(9.52059-004)+J(0.00000)	.0009521	.00000
6	(1.00000+000)+J(0.00000)	1.0000000	.00000
7	(4.06667-004)+J(0.00000)	.0004067	.00000
8	(-5.86190-004)+J(0.00000)	-.0005862	.00000
9	(-2.73480-003)+J(0.00000)	-.0027348	.00000
10	(1.33639-003)+J(0.00000)	.0013364	.00000
11	(-2.59336-002)+J(0.00000)	-.0259336	.00000
12	(-3.50197-004)+J(0.00000)	-.0003502	.00000
13	(-7.99990-004)+J(0.00000)	-.0008000	.00000
14	(3.41776-001)+J(0.00000)	.3417764	.00000
15	(1.42289-002)+J(0.00000)	.0142289	.00000
16	(1.75682-002)+J(0.00000)	.0175682	.00000
17	(1.78451-003)+J(0.00000)	.0017845	.00000

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(-1.29242+001)+J(5.55568+000)	1.44044+001	.89043	1	(2.07037-001)+J(-9.42804-001)	.9652706	-77.61460
			2	(1.91130-002)+J(-1.10031-001)	.1116783	-80.18568
			3	(-0.37932-003)+J(-1.33060-002)	.0140081	-108.21763
			4	(1.00000+000)+J(0.00000)	1.0000000	.00000
			5	(3.61851-003)+J(-0.30833-003)	.0057570	-48.89917
			6	(-2.77060-001)+J(1.36472-001)	.3088516	153.77675
			7	(1.71681-003)+J(-3.14705-003)	.0035849	-41.34618
			8	(-7.30762-002)+J(-6.74998-002)	.0994801	-137.27177
			9	(-1.23025-001)+J(-8.06638-002)	.1474460	-106.83353
			10	(-1.60558-001)+J(8.29528-002)	.1807205	152.67664
			11	(3.29707-002)+J(1.63083-001)	.1663630	78.56914
			12	(7.13600-004)+J(1.67642-003)	.0018220	66.94070
			13	(2.46971-002)+J(1.39471-001)	.1423930	78.37320
			14	(9.20958-003)+J(1.17387-001)	.1177478	45.51406
			15	(9.61860-004)+J(4.10734-003)	.0042185	76.81990
			16	(-1.32585-001)+J(4.73672-002)	.1407926	140.34025
			17	(-2.98259-001)+J(5.03613-002)	.3024805	170.41594
(-1.09192+001)+J(0.00000)	0.00000	1.00000	1	(-6.86400-002)+J(0.00000)	-.0686400	.00000
			2	(-1.43717-001)+J(0.00000)	-.1437170	.00000
			3	(2.15516-003)+J(0.00000)	.0021552	.00000
			4	(1.00000+000)+J(0.00000)	1.0000000	.00000
			5	(7.11447-003)+J(0.00000)	.0071145	.00000
			6	(2.26250-001)+J(0.00000)	.2262504	.00000
			7	(2.93032-003)+J(0.00000)	.0029303	.00000
			8	(-2.22507-004)+J(0.00000)	-.0002225	.00000
			9	(9.62285-003)+J(0.00000)	.0096229	.00000
			10	(7.31197-003)+J(0.00000)	.0073120	.00000
			11	(2.15372-001)+J(0.00000)	.2153723	.00000
			12	(1.84297-003)+J(0.00000)	.0018430	.00000
			13	(2.09645-001)+J(0.00000)	.2096449	.00000
			14	(1.67546-001)+J(0.00000)	.1675457	.00000
			15	(4.94592-003)+J(0.00000)	.0049469	.00000
			16	(3.06329-001)+J(0.00000)	.3063288	.00000
			17	(2.17392-002)+J(0.00000)	.0217392	.00000

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```
(-2.24629+001)+J( 0.00000 ) 0.00000 1.00000
1 ( 2.05990-002)+J( 0.00000 ) .0205990 .00000
2 ( 1.35304-001)+J( 0.00000 ) .1353079 .00000
3 (-6.35611-003)+J( 0.00000 ) -.0635611 .00000
4 ( 2.22780-001)+J( 0.00000 ) .2227798 .00000
5 (-1.61952-002)+J( 0.00000 ) -.0161952 .00000
6 ( 0.98574-001)+J( 0.00000 ) .0985736 .00000
7 (-0.43183-003)+J( 0.00000 ) -.0043183 .00000
8 ( 2.61735-002)+J( 0.00000 ) .0261735 .00000
9 ( 6.50070-002)+J( 0.00000 ) .0650070 .00000
10 (-1.97408-001)+J( 0.00000 ) -.1974085 .00000
11 (-3.64039-001)+J( 0.00000 ) -.3640391 .00000
12 (-0.34143-003)+J( 0.00000 ) -.0034143 .00000
13 (-2.22973-001)+J( 0.00000 ) -.2229730 .00000
14 (-2.86439-001)+J( 0.00000 ) -.2864387 .00000
15 (-9.38281-003)+J( 0.00000 ) -.0093828 .00000
16 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
17 (-0.42798-001)+J( 0.00000 ) -.4279798 .00000
```

```
(-2.04915+001)+J( 1.21111+000) 2.09266+001 .99932
1 ( 0.76529-002)+J(-1.23949-002) .0492385 -14.58000
2 ( 5.03757-002)+J(-5.53393-002) .0749822 -07.79109
3 (-1.63094-003)+J( 1.66648-003) .0023318 134.38255
4 ( 1.43695-001)+J(-1.25900-001) .1910474 -01.22308
5 (-3.92725-003)+J( 5.89795-003) .0070858 123.65833
6 ( 6.74091-001)+J(-1.68759-001) .6948946 -14.05518
7 (-9.60631-004)+J( 1.60235-003) .0018682 120.94322
8 ( 1.52793-003)+J(-9.61938-003) .0097400 -80.97463
9 ( 2.10991-002)+J(-5.99365-003) .0219339 -15.85833
10 (-8.15659-002)+J( 8.68238-002) .1191275 133.21152
11 (-1.21108-001)+J( 1.47548-001) .1908828 129.34002
12 (-1.39399-003)+J( 1.74247-003) .0022252 128.85915
13 (-8.17764-002)+J( 9.28210-002) .1237057 131.38084
14 (-8.69866-002)+J( 1.02097-001) .1341030 130.41784
15 (-3.20814-003)+J( 3.86076-003) .0050197 129.75522
16 ( 1.00000+000)+J( 0.00000 ) 1.0000000 .00000
17 (-2.20039-001)+J(-1.77048-001) .2824240 -101.17921
```


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SYSTEMS CONTROL, INC. (VT) -
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(-5.44468+000)+J(0.00000) 0.00000	1.00000	1 (1.00000+000)+J(0.00000) 1.0000000	.00000
			2 (9.12475-002)+J(0.00000) .0912475	.00000
			3 (6.91668-004)+J(0.00000) .0006917	.00000
			4 (-3.12229-001)+J(0.00000) -.3122289	.00000
			5 (2.31671-003)+J(0.00000) .0023167	.00000
			6 (-3.50180-002)+J(0.00000) -.0350180	.00000
			7 (1.24509-003)+J(0.00000) .0012451	.00000
			8 (5.03383-002)+J(0.00000) .0503383	.00000
			9 (5.50099-002)+J(0.00000) .0550099	.00000
			10 (3.01444-002)+J(0.00000) .0301444	.00000
			11 (-3.55168-002)+J(0.00000) -.0355168	.00000
			12 (-5.1452-005)+J(0.00000) -.000514	.00000
			13 (-3.47432-002)+J(0.00000) -.0347432	.00000
			14 (-2.39197-002)+J(0.00000) -.0239197	.00000
			15 (-1.36424-004)+J(0.00000) -.0001364	.00000
			16 (-3.00866-002)+J(0.00000) -.0300866	.00000
			17 (7.45299-002)+J(0.00000) .0745299	.00000
(-2.09234+000)+J(0.00000) 0.00000	1.00000	1 (-9.00148-001)+J(0.00000) -.9001480	.00000
			2 (-5.69883-001)+J(0.00000) -.5698833	.00000
			3 (4.80362-003)+J(0.00000) .0048436	.00000
			4 (1.00000+000)+J(0.00000) 1.0000000	.00000
			5 (9.22160-003)+J(0.00000) .0092216	.00000
			6 (1.37800-001)+J(0.00000) .1378005	.00000
			7 (3.18305-003)+J(0.00000) .0031830	.00000
			8 (-2.61868-002)+J(0.00000) -.0261868	.00000
			9 (-1.99966-002)+J(0.00000) -.0199966	.00000
			10 (-1.26448-002)+J(0.00000) -.0126448	.00000
			11 (1.07541-001)+J(0.00000) .1075407	.00000
			12 (-3.24234-003)+J(0.00000) -.0032423	.00000
			13 (1.25814-001)+J(0.00000) .1258138	.00000
			14 (6.34911-002)+J(0.00000) .0634911	.00000
			15 (-1.31620-001)+J(0.00000) -.1316204	.00000
			16 (1.68511-001)+J(0.00000) .1685107	.00000
			17 (-2.12935-002)+J(0.00000) -.0212935	.00000

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SYSTEMS CONTROL, INC. (VT) -
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```

(-1.70377+000)+J( 0.00000 ) 0.00000 1.00000 1  ( 4.00012-001)+J( 0.00000 ) 0.00000 0.0000
2  (-5.72785-001)+J( 0.00000 ) 0.00000 0.00000 2  -0.5727850 0.00000
3  ( 2.08691-003)+J( 0.00000 ) 0.00000 0.00000 3  -0.0020869 0.00000
4  ( 1.00000+000)+J( 0.00000 ) 0.00000 0.00000 4  1.0000000 0.00000
5  ( 1.33090-002)+J( 0.00000 ) 0.00000 0.00000 5  0.1330900 0.00000
6  ( 4.98108-002)+J( 0.00000 ) 0.00000 0.00000 6  0.4981080 0.00000
7  ( 4.95654-003)+J( 0.00000 ) 0.00000 0.00000 7  0.0495650 0.00000
8  ( 1.68300-002)+J( 0.00000 ) 0.00000 0.00000 8  0.1683000 0.00000
9  ( 2.09447-002)+J( 0.00000 ) 0.00000 0.00000 9  0.0209447 0.00000
10 (-7.52711-004)+J( 0.00000 ) 0.00000 0.00000 10 -0.0075271 0.00000
11 ( 9.69196-002)+J( 0.00000 ) 0.00000 0.00000 11  0.9691960 0.00000
12 (-4.56022-003)+J( 0.00000 ) 0.00000 0.00000 12 -0.0045602 0.00000
13 ( 1.17446-001)+J( 0.00000 ) 0.00000 0.00000 13  0.1174461 0.00000
14 ( 8.90253-002)+J( 0.00000 ) 0.00000 0.00000 14  0.8902530 0.00000
15 ( 4.39736-002)+J( 0.00000 ) 0.00000 0.00000 15  0.4397360 0.00000
16 ( 9.30790-002)+J( 0.00000 ) 0.00000 0.00000 16  0.9397900 0.00000
17 ( 2.27349-002)+J( 0.00000 ) 0.00000 0.00000 17  0.0227349 0.00000

(-1.90834+001)+J( 0.00000 ) 0.00000 1.00000 1  ( 2.88678-002)+J( 0.00000 ) 0.00000
2  (-3.01242-002)+J( 0.00000 ) 0.00000 0.00000 2  -0.3012420 0.00000
3  ( 8.10452-005)+J( 0.00000 ) 0.00000 0.00000 3  0.0000810 0.00000
4  (-1.26939-001)+J( 0.00000 ) 0.00000 0.00000 4  -0.1269391 0.00000
5  ( 1.13575-003)+J( 0.00000 ) 0.00000 0.00000 5  0.0011359 0.00000
6  ( 3.54271-001)+J( 0.00000 ) 0.00000 0.00000 6  0.3542713 0.00000
7  ( 3.64513-004)+J( 0.00000 ) 0.00000 0.00000 7  0.0003645 0.00000
8  ( 4.81980-004)+J( 0.00000 ) 0.00000 0.00000 8  0.0004820 0.00000
9  (-2.85701-002)+J( 0.00000 ) 0.00000 0.00000 9  -0.2857010 0.00000
10 ( 5.27434-002)+J( 0.00000 ) 0.00000 0.00000 10  0.5274340 0.00000
11 ( 7.24304-002)+J( 0.00000 ) 0.00000 0.00000 11  0.7243040 0.00000
12 ( 8.20303-004)+J( 0.00000 ) 0.00000 0.00000 12  0.0008203 0.00000
13 ( 4.87429-002)+J( 0.00000 ) 0.00000 0.00000 13  0.4874290 0.00000
14 ( 5.33226-002)+J( 0.00000 ) 0.00000 0.00000 14  0.5332260 0.00000
15 ( 1.95472-003)+J( 0.00000 ) 0.00000 0.00000 15  0.0019547 0.00000
16 ( 1.00000+000)+J( 0.00000 ) 0.00000 0.00000 16  1.0000000 0.00000
17 (-5.78841-001)+J( 0.00000 ) 0.00000 0.00000 17 -0.5788410 0.00000

```

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SYSTEMS CONTROL, INC. (VT) -
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(-7.73112-001)+J(0.00000)	0.00000	1.00000	1	(1.10935-001)+J(0.00000)	.1108358	.00000
				2	(-6.24092-001)+J(0.00000)	-.6240920	.00000
				3	(3.18722-003)+J(0.00000)	.0031872	.00000
				4	(1.00000+000)+J(0.00000)	1.0000000	.00000
				5	(1.31222-002)+J(0.00000)	.0131222	.00000
				6	(7.18621-002)+J(0.00000)	.0718621	.00000
				7	(5.01352-003)+J(0.00000)	.0050135	.00000
				8	(6.49146-003)+J(0.00000)	.0066715	.00000
				9	(1.15137-002)+J(0.00000)	.0115137	.00000
				10	(-6.60168-003)+J(0.00000)	-.0046017	.00000
				11	(9.04853-002)+J(0.00000)	.0904853	.00000
				12	(-5.31956-002)+J(0.00000)	-.0531956	.00000
				13	(1.10980-001)+J(0.00000)	.1109837	.00000
				14	(9.44497-002)+J(0.00000)	.0944497	.00000
				15	(1.44730-002)+J(0.00000)	.0144734	.00000
				16	(1.05485-001)+J(0.00000)	.1054851	.00000
				17	(1.21019-002)+J(0.00000)	.0121019	.00000

APPENDIX F

SENSITIVITY DATA FOR LINEAR QUADRATIC REGULATOR GAINS AND GAIN SCHEDULES FOR MULTIVARIABLE CONTROLLER

F.1 UTILIZATION OF SENSITIVITY DATA TO SIMPLIFY CONTROL LAW

The controller gains resulting from LQR designs at the six design points (Appendix E) are compiled in Table F.1. These gains were smoothed and simplified using the sensitivity data in Section F.2 to form the final set of implemented control gains shown in Table F.2.

F.2 SENSITIVITY DATA

Sensitivities of the closed-loop eigenvalues are given as a function of each element of the regulator gain matrix and each diagonal element of the state and control weightings. The sensitivity of the eigenvalue, λ_i , to parameter, θ_j , is defined as follows:

$$S_{\theta_j}^i = \frac{\partial \lambda_i}{\partial \theta / \theta_o}$$

where θ_o is the baseline value of the C, A, or B matrices.

The sensitivity $S_{\theta_j}^i$ is a complex vector which is associated with a particular eigenvalue λ_i . The printout is organized to show all the sensitivities of a particular matrix element of the C, A, or B matrices in a group. The Baseline Parameter Value is the value, θ_o , in the matrix. The Pole Location column contains values of the five eigenvalues, λ_i , in the fifth order linear design mode. The

Table F.1

SCI (Vt) F100 Multivariable Controller, SCI-MVC-F100/4L, Raw Feedback Gain List

REGULATOR CONTROL GAINS (RAW)									
GAIN COMPONENT	INTERMEDIATE				IDLE		$\times 10^{\text{EXP}}$ EXP:	UNITS	FEEDBACK MATRIX ELEMENT
	HPG1	HPG2	HPG3	HPG4	LPG1	LPG2			
WF/N1	-7.30	-4.15	-5.11	-11.0	-5.75	-0.28	-1	lbm/hr-rpm	(1,1)
WF/N2	-1.13	-1.81	-1.95	-2.65	-1.42	-0.67	0	lbm/hr-rpm	(1,2)
WF/PT6	-3.67	-13.4	-30.1	+16.6	14.28	-11.3	0	lbm/hr-psia	(1,3)
WF/WFC	-3.48	-5.83	-2.41	-3.55	-6.91	-1.23	-1	---	(1,4)
WF/PT4	4.43	9.67	2.86	8.08	8.86	0.45	0	lbm/hr-psia	(1,5)
AJ/N1	-4.00	-4.64	-1.91	-0.99	-2.38	0.15	-4	ft ² /rpm	(2,1)
AJ/N2	-2.19	3.75	4.56	-1.42	-6.45	-14.4	-5	ft ² /rpm	(2,2)
AJ/PT6	6.37	3.33	3.71	2.80	1.77	0.48	-2	ft ² /psia	(2,3)
CIVV/N1	8.99	9.54	6.12	2.28	1.46	0.63	-3	deg/rpm	(3,1)
CIVV/N2	-3.33	1.35	0.91	0.42	-6.02	2.67	-3	deg/rpm	(3,2)
CIVV/PT6	-7.07	-3.27	-3.58	-1.35	-5.18	-5.5	-1	deg/psia	(3,3)
RCVV/N1	-0.68	-2.98	-0.48	-5.60	-4.47	-0.49	-3	deg/rpm	(4,1)
RCVV/N2	7.98	5.20	7.25	-4.00	-4.87	-0.35	-3	deg/rpm	(4,2)
RCVV/PT6	-1.53	-1.50	-1.89	1.83	0.32	2.99	-1	deg/psia	(4,3)
BLC/N1	4.02	-2.08	0.79	2.29	0.83	0.36	-5	rpm ⁻¹	(5,1)
BLC/N2	5.86	6.06	7.53	3.86	2.99	1.56	-5	rpm ⁻¹	(5,2)
BLC/PT4	4.53	4.27	2.51	0.65	1.14	-0.39	-3	psia ⁻¹	(5,5)

Table F.2
SCI (Vt) F100 Multivariable Controller, SCI-MVC-F100/4L, Smoothed
Feedback Gain List

GAIN COMPONENT	RETULATOR CONTROL GAINS (SMOOTHED)								FEEDBACK MATRIX ELEMENT
	INTERMEDIATE				IDLE		x10 ^{EXP} EXP:	UNITS	
	HPG1	HPG2	HPG3	HPG4	LPG1	LPG2			
WF/N1	-7.30	-4.63	-4.63	-11.0	-5.75	-0.28	-1	1bm/hr-rpm	(1,1)
WF/N2	-1.13	-1.81	-1.95	-2.65	-1.42	-0.67	0	1bm/hr-rpm	(1,2)
WF/PT6	-0.37	-1.34	-3.01	0.0	0.0	-1.13	1	1bm/hr-psia	(1,3)
WF/WFC	-3.82	-3.82	-3.82	-3.82	-4.07	-4.07	-1	---	(1,4)
WF/PT4	6.26	6.26	6.26	6.26	6.26	0.0	1	1bm/hr-psia	(1,5)
AJ/N1	-4.32	-4.32	-1.91	-0.99	-2.38	0.0	-4	ft ² /rpm	(2,1)
AJ/N2	-0.22	0.0	0.0	-0.14	-0.65	-1.44	-4	ft ² /rpm	(2,2)
AJ/PT6	6.37	3.52	3.52	2.80	1.77	0.48	-2	ft ² /psia	(2,3)
CIVV/N1	9.27	9.27	6.12	2.28	1.46	0.63	-3	deg/rpm	(3,1)
CIVV/PT6	-7.07	-3.43	-3.43	-1.35	-5.37	-5.37	-1	deg/psia	(3,3)
RCVV/N1	-2.46	-2.46	-2.46	-2.46	-2.46	-2.46	-3	deg/rpm	(4,1)
RCVV/N2	6.81	6.81	6.81	-4.00	-4.87	-0.35	-3	deg/rpm	(4,2)
RCVV/PT6	-1.64	-1.64	-1.64	0.0	0.0	2.99	-1	deg/psia	(4,3)
BLC/N1	2.30	2.30	2.30	2.30	0.60	0.60	-5	rpm ⁻¹	(5,1)
BLC/N2	5.83	5.83	5.83	5.83	2.28	2.28	-5	rpm ⁻¹	(5,2)
BLC/PT4	4.40	4.40	2.51	0.65	1.14	0.0	-3	psia ⁻¹	(5,3)

Table F.3
Gain Component Symbol Index to Tables F.2 and F.3

SYMBOL	TITLE	UNITS
WF	Main Burner Fuel Flow	lbm/hr
N1	Low Rotor Speed	rpm
N2	High Rotor Speed	rpm
PT6	Augmentor Entrance Total Pressure	psia
WFC	Requested Fuel Flow	lbm/hr
PT4	Burner Pressure	psia
AJ	Jet Area	ft ²
CIVV	Compressor Inlet Variable Vane Angle	deg
RCVV	Rear Compressor Variable Stator Angle	deg
BLC	Bleed Percentage Flow	fraction

Table F.4
Index to Sensitivity Printout
(Design Point Data)

CASE	PLA (DEG)	ALTITUDE (FT)	MACH NO.	PAGE
HPG1	83	45,000	0.9	314
HPG2	83	30,000	0.9	327
HPG3	83	0	0	337
HPG4	83	0	1.2	350
LPG1	20	30,000	0.9	363
LPG2	20	0	0	376

Sensitivity data is organized into two columns containing the Real and Imaginary part of the complex vector:

$$S_{\theta_j}^i \cdot \theta_o = \frac{\partial \lambda_i}{\partial \theta_j}$$

Also, the Magnitude and Phase of $S_{\theta_j}^i$ is given. Note, if $\theta_o = 0$, then $\theta_o = 1$ is assumed.

83/45K/0.9 OPTIMAL CONTROL DESIGN POINT HPGL

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

1 SENSITIVITY OF CLOSED LOOP SYSTEM

SENSITIVITY TO 1 1 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -7.29963+001

.....POLE LOCATION.....REAL.....IMAGINARY.....SENSITIVITY.....MAGNITUDE.....PHASE.....
(-2.62414+002) + J(0.00000)	(1.82481-001) + J(0.00000)		1.33204+001	2.22045+016	
(-1.00714+001) + J(1.98371+000)	(-4.90575-001) + J(-3.69490+000)		2.72082+000	-9.75646+001	
(-1.00714+001) + J(-1.98371+000)	(-4.90575-001) + J(3.69490+000)		2.72082+000	9.75646+001	
(-3.37406+000) + J(0.00000)	(5.26473-001) + J(0.00000)		4.57303+001	1.11022+016	
(-1.49428+000) + J(0.00000)	(-6.68045+002) + J(0.00000)		4.87645+002	1.80000+002	

SENSITIVITY TO 1 2 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -1.12935+000

.....POLE LOCATION.....REAL.....IMAGINARY.....SENSITIVITY.....MAGNITUDE.....PHASE.....
(-2.62414+002) + J(0.00000)	(1.32988-001) + J(0.00000)		1.50190+001	1.11022+016	
(-1.00714+001) + J(1.98371+000)	(-2.51299-001) + J(-1.34340+001)		3.21812+001	-1.51872+002	
(-1.00714+001) + J(-1.98371+000)	(-2.51299-001) + J(1.34340+001)		3.21812+001	1.51872+002	
(-3.37406+000) + J(0.00000)	(-8.33034-002) + J(0.00000)		9.40786+002	1.80000+002	
(-1.49428+000) + J(0.00000)	(4.94043+001) + J(0.00000)		5.57947+001	1.11022+016	

SENSITIVITY TO 1 3 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -3.66976+000

.....POLE LOCATION.....REAL.....IMAGINARY.....SENSITIVITY.....MAGNITUDE.....PHASE.....
(-2.62414+002) + J(0.00000)	(7.16328-004) + J(0.00000)		2.62875+003	2.22045+016	
(-1.00714+001) + J(1.98371+000)	(-5.11862-004) + J(-2.35154+002)		8.63163+002	-9.12470+001	
(-1.00714+001) + J(-1.98371+000)	(-5.11862-004) + J(2.35154+002)		8.63163+002	9.12470+001	
(-3.37406+000) + J(0.00000)	(4.09922-004) + J(0.00000)		1.50431+003	1.11022+016	
(-1.49428+000) + J(0.00000)	(-7.57325-004) + J(0.00000)		2.77920+003	1.80000+002	

SENSITIVITY TO 1 4 ELEMENT OF C		MATRIX		BASELINE PARAMETER VALUE = -3.47691-001	
.....Pole LOCATION.....					
REAL		IMAGINARY		SENSITIVITY MAGNITUDE PHASE	
(-2.62414+002)	+ J(0.00000)	(7.10383-002)	+ J(0.00000)	2.46994-002	1.11022-016
(-1.00714+001)	+ J(1.98371+000)	(5.36682+000)	+ J(5.45886+000)	2.66090+000	4.54714+001
(-1.00714+001)	+ J(-1.98371+000)	(5.36682+000)	+ J(-5.45886+000)	2.66090+000	-4.54714+001
(-1.37016+000)	+ J(0.00000)	(-3.80485-001)	+ J(0.00000)	1.32291-001	1.80000+002
(-1.48428+000)	+ J(0.00000)	(-4.24195-001)	+ J(0.00000)	1.47489-001	1.80000+002

SENSITIVITY TO 1 5 ELEMENT OF C		MATRIX		BASELINE PARAMETER VALUE = 4.42773+000	
.....Pole LOCATION.....					
REAL		IMAGINARY		SENSITIVITY MAGNITUDE PHASE	
(-2.62414+002)	+ J(0.00000)	(-3.34796-001)	+ J(0.00000)	1.48239+000	1.80000+002
(-1.00714+001)	+ J(1.98371+000)	(2.29307-002)	+ J(-2.83201-003)	1.02302-001	-7.04057+000
(-1.00714+001)	+ J(-1.98371+000)	(2.29307-002)	+ J(2.83201-003)	1.02302-001	7.04057+000
(-3.37016+000)	+ J(0.00000)	(-4.44230-003)	+ J(0.00000)	1.96693-002	1.80000+002
(-1.45428+000)	+ J(0.00000)	(-5.23498-004)	+ J(0.00000)	2.31791-003	1.80000+002

SENSITIVITY TO 2 1 ELEMENT OF C		MATRIX		BASELINE PARAMETER VALUE = -3.99878-004	
.....Pole LOCATION.....					
REAL		IMAGINARY		SENSITIVITY MAGNITUDE PHASE	
(-2.62414+002)	+ J(0.00000)	(8.51774+001)	+ J(0.00000)	3.40606-002	1.11022-016
(-1.00714+001)	+ J(1.98371+000)	(-1.63655+003)	+ J(1.34626+003)	8.47395-001	1.40559+002
(-1.00714+001)	+ J(-1.98371+000)	(-1.63655+003)	+ J(-1.34626+003)	8.47395-001	-1.40559+002
(-3.37016+000)	+ J(0.00000)	(2.87491+003)	+ J(0.00000)	1.15121+000	0.00000
(-1.48428+000)	+ J(0.00000)	(-5.19831+001)	+ J(0.00000)	2.07459-002	1.80000+002

SENSITIVITY TO 2 2 ELEMENT OF C		MATRIX		BASELINE PARAMETER VALUE = -2.18727-005	
.....REALIMAGINARYREALIMAGINARYMAGNITUDEPHASE
(-2.52014+002) + JC 0.00000)		(6.20755+001) + JC 0.00000)		1.35776-003	1.11022-016
(-1.00714+001) + JC 1.98371+000)		(1.05922+001) + JC 1.61660+002)		3.54352-003	8.62513+001
(-1.00714+001) + JC 1.98371+000)		(1.05922+001) + JC 1.61660+002)		3.54352-003	-8.62513+001
(-3.37406+000) + JC 0.00000)		(-3.82814+002) + JC 0.00000)		8.37315-003	1.80000+002
(-1.49428+000) + JC 0.00000)		(3.84434+002) + JC 0.00000)		8.40859-003	1.11022-016
SENSITIVITY TO 2 3 ELEMENT OF C		MATRIX		BASELINE PARAMETER VALUE = 6.36764-002	
.....REALIMAGINARYREALIMAGINARYMAGNITUDEPHASE
(-2.52014+002) + JC 0.00000)		(3.34364-001) + JC 0.00000)		2.12911-002	1.11022-016
(-1.00714+001) + JC 1.98371+000)		(-1.11994+001) + JC 7.30747+000)		8.51518-001	1.46876+002
(-1.00714+001) + JC 1.98371+000)		(-1.11994+001) + JC 7.30747+000)		8.51518-001	-1.46876+002
(-3.37406+000) + JC 0.00000)		(1.89374+000) + JC 0.00000)		1.19951-001	1.11022-016
(-1.49428+000) + JC 0.00000)		(-5.89304-001) + JC 0.00000)		3.75248-002	1.80000+002
SENSITIVITY TO 2 4 ELEMENT OF C		MATRIX		BASELINE PARAMETER VALUE = 1.81536-005	
.....REALIMAGINARYREALIMAGINARYMAGNITUDEPHASE
(-2.52014+002) + JC 0.00000)		(3.31589+001) + JC 0.00000)		6.01953-004	1.11022-016
(-1.00714+001) + JC 1.98371+000)		(1.02270+003) + JC 4.22915+003)		7.89872-002	-7.64056+001
(-1.00714+001) + JC 1.98371+000)		(1.02270+003) + JC 4.22915+003)		7.89872-002	7.64056+001
(-3.37406+000) + JC 0.00000)		(-1.74849+003) + JC 0.00000)		3.17413-002	1.80000+002
(-1.49428+000) + JC 0.00000)		(-3.30082+002) + JC 0.00000)		5.99217-003	1.80000+002

93/45K/0.0 OPTIMAL CONTROL DESIGN POINT WPG1
SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

SENSITIVITY TO 2 5 ELEMENT OF C		MATRIX:		BASELINE PARAMETER VALUE = 1.31992+003	
.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL		IMAGINARY		MAGNITUDE	
(-2.62414+002) + J(0.00000)		(-1.56274+002) + J(0.00000)		2.06270+001 1.80000+002	
(-1.00714+001) + J(1.99371+000)		(-8.25206+000) + J(-1.02205+001)		1.73385+002 -1.28918+002	
(-1.00714+001) + J(-1.99371+000)		(-8.25206+000) + J(1.02205+001)		1.73385+002 1.28918+002	
(-3.37406+000) + J(0.00000)		(-2.04142+001) + J(0.00000)		2.69451+002 1.80000+002	
(-1.45428+000) + J(0.00000)		(-4.07354+001) + J(0.00000)		5.37674+004 1.80000+002	
SENSITIVITY TO 3 1 ELEMENT OF C		MATRIX:		BASELINE PARAMETER VALUE = 8.98535+003	
.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL		IMAGINARY		MAGNITUDE	
(-2.62414+002) + J(0.00000)		(-6.94004+000) + J(0.00000)		6.23587+002 1.11022-016	
(-1.00714+001) + J(1.99371+000)		(-5.38914+000) + J(6.11500+001)		7.55704+002 4.16952+000	
(-1.00714+001) + J(-1.99371+000)		(-5.38914+000) + J(-6.11500+001)		7.55704+002 -4.16952+000	
(-3.37406+000) + J(0.00000)		(-5.02835+001) + J(0.00000)		4.51815+001 1.80000+002	
(-1.45428+000) + J(0.00000)		(-6.62815+001) + J(0.00000)		5.95562+003 1.80000+002	
SENSITIVITY TO 3 2 ELEMENT OF C		MATRIX:		BASELINE PARAMETER VALUE = -3.32910+003	
.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL		IMAGINARY		MAGNITUDE	
(-2.62414+002) + J(0.00000)		(-5.05775+000) + J(0.00000)		1.68378+002 1.11022-016	
(-1.00714+001) + J(1.99371+000)		(-4.12109+001) + J(-4.93537+001)		2.14052+003 -5.01378+001	
(-1.00714+001) + J(-1.99371+000)		(-4.12109+001) + J(4.93537+001)		2.14052+003 5.01378+001	
(-3.37406+000) + J(0.00000)		(-6.68628+000) + J(0.00000)		2.22593+002 1.11022-016	
(-1.45428+000) + J(0.00000)		(-4.90175+000) + J(0.00000)		1.63184+002 1.11022-016	

SENSITIVITY TO 3 3 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -7.06987-001

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-2.52414+002)	J(0.00000)		1.92605-002	2.22045-016
(-1.00714+001)	J(1.98371+000)		3.75219-002	1.04871+001
(-1.00714+001)	J(-1.98371+000)		3.75219-002	-1.04871+001
(-3.37406+000)	J(0.00000)		2.32613-002	1.80000+002
(-1.43428+000)	J(0.00000)		5.31228-003	1.80000+002

SENSITIVITY TO 3 4 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 7.80086-004

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-2.52414+002)	J(0.00000)		2.10756-003	1.11022-016
(-1.00714+001)	J(1.98371+000)		1.34708-002	1.47206+002
(-1.00714+001)	J(-1.98371+000)		1.34708-002	1.47206+002
(-3.37406+000)	J(0.00000)		2.38233-002	1.11022-016
(-1.43428+000)	J(0.00000)		3.28317-003	1.80000+002

SENSITIVITY TO 3 5 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 5.77986-002

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-2.52414+002)	J(0.00000)		7.35939-001	1.80000+002
(-1.00714+001)	J(1.98371+000)		3.01328-003	9.44935+001
(-1.00714+001)	J(-1.98371+000)		3.01328-003	-9.44935+001
(-3.37406+000)	J(0.00000)		2.06085-002	1.11022-016
(-1.43428+000)	J(0.00000)		3.00205-004	1.80000+002

83/054/0.0 OPTIMAL CONTROL DESIGN POINT HPG1
SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

SENSITIVITY TO		4	1 ELEMENT OF C	MATRIX	BASELINE PARAMETER VALUE # -6.78373-004	
.....POLE LOCATION.....				SENSITIVITY.....	
REAL					MAGNITUDE	
IMAGINARY					PHASE	
(-2.52014+002) + J(0.00000)		(-7.74999+000) + J(0.00000)			5.25739-003 1.80000+002	
(-1.00714+001) + J(1.93371+000)		(-5.24489+000) + J(5.38597+000)			4.65207-003 1.28243+002	
(-1.00714+001) + J(-1.93371+000)		(-5.24489+000) + J(-5.38597+000)			4.65207-003 -1.28243+002	
(-3.37476+000) + J(0.00000)		(7.17524+000) + J(0.00000)			4.86817-003 1.11022-016	
(-1.48428+000) + J(0.00000)		(1.06254+000) + J(0.00000)			7.20800-004 1.11022-016	
SENSITIVITY TO		4	2 ELEMENT OF C	MATRIX	BASELINE PARAMETER VALUE # 7.97656-003	
.....POLE LOCATION.....				SENSITIVITY.....	
REAL					MAGNITUDE	
IMAGINARY					PHASE	
(-2.52014+002) + J(0.00000)		(-5.64803+000) + J(0.00000)			4.50518-002 1.80000+002	
(-1.00714+001) + J(1.93371+000)		(1.45072-001) + J(5.03795-001)			4.18184-003 7.39358+001	
(-1.00714+001) + J(-1.93371+000)		(1.45072-001) + J(-5.03795-001)			4.18184-003 -7.39358+001	
(-3.37476+000) + J(0.00000)		(-5.54236-001) + J(0.00000)			7.61152-003 1.80000+002	
(-1.48428+000) + J(0.00000)		(-7.85788+000) + J(0.00000)			6.26789-002 1.80000+002	
SENSITIVITY TO		4	3 ELEMENT OF C	MATRIX	BASELINE PARAMETER VALUE # -1.52613-001	
.....POLE LOCATION.....				SENSITIVITY.....	
REAL					MAGNITUDE	
IMAGINARY					PHASE	
(-2.52014+002) + J(0.00000)		(-3.04226-002) + J(0.00000)			4.64288-003 1.80000+002	
(-1.00714+001) + J(1.93371+000)		(-3.03642-002) + J(3.08336-002)			6.60428-003 1.30561+002	
(-1.00714+001) + J(-1.93371+000)		(-3.03642-002) + J(-3.08336-002)			6.60428-003 -1.30561+002	
(-3.37476+000) + J(0.00000)		(4.69554-003) + J(0.00000)			7.16614-004 1.11022-016	
(-1.48428+000) + J(0.00000)		(1.20455-002) + J(0.00000)			1.83829-003 1.11022-016	

SS/45K/0.0 OPTIMAL CONTROL DESIGN POINT HPG1

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

SENSITIVITY TO 4 4 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -4.89765-004

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.62414+002)	+ J(0.00000)	(-3.01701+000)	+ J(0.00000)	1.47763-003	1.80000+002
(-1.00714+001)	+ J(1.98371+000)	(3.14263-001)	+ J(-1.40768+001)	6.89606-003	-3.87212+001
(-1.00714+001)	+ J(-1.98371+000)	(3.14263-001)	+ J(1.40768+001)	6.89606-003	8.87212+001
(-3.37436+000)	+ J(0.00000)	(-4.35543+000)	+ J(0.00000)	2.13461-003	1.80000+002
(-1.49426+000)	+ J(0.00000)	(6.74692+000)	+ J(0.00000)	3.30441-003	1.11022-016

SENSITIVITY TO 4 5 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -1.58569-001

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.62414+002)	+ J(0.00000)	(1.42188+001)	+ J(0.00000)	2.25466+000	1.11022-016
(-1.00714+001)	+ J(1.98371+000)	(-3.31443-002)	+ J(-2.66173-002)	6.74060-003	-1.41233+002
(-1.00714+001)	+ J(-1.98371+000)	(-3.31443-002)	+ J(2.66173-002)	6.74060-003	1.41233+002
(-3.37436+000)	+ J(0.00000)	(-5.08563-002)	+ J(0.00000)	8.06894-003	1.80000+002
(-1.49426+000)	+ J(0.00000)	(8.32637-003)	+ J(0.00000)	1.32030-003	1.11022-016

SENSITIVITY TO 5 1 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 4.02047-005

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.62414+002)	+ J(0.00000)	(1.04520+004)	+ J(0.00000)	4.20221-001	1.11022-016
(-1.00714+001)	+ J(1.98371+000)	(-2.90037+003)	+ J(6.42601+003)	2.83452-001	1.14292+002
(-1.00714+001)	+ J(-1.98371+000)	(-2.90037+003)	+ J(-6.42601+003)	2.83452-001	-1.14292+002
(-3.37436+000)	+ J(0.00000)	(-2.01773+003)	+ J(0.00000)	8.11222-002	1.80000+002
(-1.49426+000)	+ J(0.00000)	(1.66423+002)	+ J(0.00000)	6.69099-003	1.11022-016

SENSITIVITY TO 5 2 ELEMENT OF C MATRIX BASELINE PARAMETER VALUE = 5.86199-005

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.62414+002)	+ J(0.00000)	(7.61722+003)	+ J(0.00000)	4.46521-001	1.11022-016
(-1.00714+001)	+ J(1.98371+000)	(2.59618+002)	+ J(4.66704+002)	3.15953-002	5.99848+001
(-1.00714+001)	+ J(-1.98371+000)	(2.69518+002)	+ J(-4.66704+002)	3.15953-002	-5.99848+001
(-3.37435+000)	+ J(0.00000)	(2.69301+002)	+ J(0.00000)	1.57278-002	0.00000
(-1.45425+000)	+ J(0.00000)	(-1.23076+003)	+ J(0.00000)	7.21470-002	1.80000+002

SENSITIVITY TO 5 3 ELEMENT OF C MATRIX BASELINE PARAMETER VALUE = 9.10523-003

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.62414+002)	+ J(0.00000)	(4.10295+001)	+ J(0.00000)	3.73583-001	1.11022-016
(-1.00714+001)	+ J(1.98371+000)	(-2.26535+001)	+ J(3.82904+001)	4.05089-001	1.20610+002
(-1.00714+001)	+ J(-1.98371+000)	(-2.26535+001)	+ J(-3.82904+001)	4.05089-001	-1.20610+002
(-3.37435+000)	+ J(0.00000)	(-1.32026+000)	+ J(0.00000)	1.20213-002	1.80000+002
(-1.45425+000)	+ J(0.00000)	(1.88665+000)	+ J(0.00000)	1.71784-002	1.11022-016

SENSITIVITY TO 5 4 ELEMENT OF C MATRIX BASELINE PARAMETER VALUE = 3.92125-005

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.62414+002)	+ J(0.00000)	(4.06830+003)	+ J(0.00000)	1.59552-001	1.11022-016
(-1.00714+001)	+ J(1.98371+000)	(-3.17555+003)	+ J(-1.41231+004)	5.67627-001	-1.02672+002
(-1.00714+001)	+ J(-1.98371+000)	(-3.17555+003)	+ J(1.41231+004)	5.67627-001	1.02672+002
(-3.37435+000)	+ J(0.00000)	(1.22545+003)	+ J(0.00000)	4.80531-002	1.11022-016
(-1.45425+000)	+ J(0.00000)	(1.05675+003)	+ J(0.00000)	4.14379-002	1.11022-016

83/45K/D.2 OPTIMAL CONTROL DESIGN POINT MP61

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

SENSITIVITY TO 5 S ELEMENT OF C		MATRIX		BASELINE PARAMETER VALUE # 4.53352-003	
.....POLE LOCATION.....	SENSITIVITY.....	MAGNITUDE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.52414+002)	+ J(0.00000)	(-1.71763+004)	+ J(0.00000)	8.63160+001	1.80000+002
(-1.00714+001)	+ J(1.98371+000)	(-3.96672+001)	+ J(-1.83422+001)	1.98127-001	1.55184+002
(-1.00714+001)	+ J(-1.98371+000)	(-3.96672+001)	+ J(1.83422+001)	1.98127-001	1.55184+002
(-3.17408+000)	+ J(0.00000)	(1.43076+001)	+ J(0.00000)	6.48638-002	1.11022-016
(-1.48424+000)	+ J(0.00000)	(1.30414+000)	+ J(0.00000)	5.91233-003	1.11022-016

1 SENSITIVITY OF OPTIMAL CONTROLLER DESIGN 1

SENSITIVITY TO 1 1 ELEMENT OF A MATRIX: BASELINE PARAMETER VALUE = 5.00000-004

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.62014+002)	+ J(0.00000)	(1.21148+001)	+ J(0.00000)	6.05740-003	2.22045-016
(-1.00714+001)	+ J(1.9371+000)	(-9.51982+001)	+ J(1.27137+003)	6.37463-001	9.42823+001
(-1.00714+001)	+ J(-1.9371+000)	(-9.51982+001)	+ J(-1.27137+003)	6.37463-001	-9.42823+001
(-3.37006+000)	+ J(0.00000)	(-2.43854+003)	+ J(0.00000)	1.21927+000	1.80000+002
(-1.48428+000)	+ J(0.00000)	(1.21081+002)	+ J(0.00000)	6.05403-002	1.11022-016

SENSITIVITY TO 2 2 ELEMENT OF A MATRIX: BASELINE PARAMETER VALUE = 5.00000-004

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.62014+002)	+ J(0.00000)	(-1.15460+001)	+ J(0.00000)	5.77299-003	1.80000+002
(-1.00714+001)	+ J(1.9371+000)	(2.64502+001)	+ J(3.04339+001)	2.01721-002	4.90340+001
(-1.00714+001)	+ J(-1.9371+000)	(2.64502+001)	+ J(-3.04339+001)	2.01721-002	-4.90340+001
(-3.37006+000)	+ J(0.00000)	(3.43784+001)	+ J(0.00000)	1.71842-002	1.11022-016
(-1.48428+000)	+ J(0.00000)	(-7.76224+002)	+ J(0.00000)	3.88112-001	1.80000+002

SENSITIVITY TO 3 3 ELEMENT OF A MATRIX: BASELINE PARAMETER VALUE = 5.00000-001

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.62014+002)	+ J(0.00000)	(3.44237-004)	+ J(0.00000)	1.97118-004	2.22045-016
(-1.00714+001)	+ J(1.9371+000)	(-4.57295-002)	+ J(5.83756-002)	3.70773-002	1.28074+002
(-1.00714+001)	+ J(-1.9371+000)	(-4.57295-002)	+ J(-5.83756-002)	3.70773-002	-1.28074+002
(-3.37006+000)	+ J(0.00000)	(5.90178-003)	+ J(0.00000)	2.95089-003	1.11022-016
(-1.48428+000)	+ J(0.00000)	(1.29533-003)	+ J(0.00000)	6.47664-004	1.11022-016

SENSITIVITY TO 4 4 ELEMENT OF A MATRIX: BASELINE PARAMETER VALUE = 0.00000

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-2.52414+002) + J(0.00000)	(-2.30791+001) + J(0.00000)		2.30791+001	1.80000+002	
(-1.00714+001) + J(1.98371+000)	(-2.01935+004) + J(-2.39987+004)		3.13645+004	-1.30079+002	
(-1.00714+001) + J(-1.98371+000)	(-2.01935+004) + J(2.39987+004)		3.13645+004	1.30079+002	
(-3.37405+000) + J(0.00000)	(1.50940+003) + J(0.00000)		1.50940+003	1.11022-016	
(-1.49425+000) + J(0.00000)	(1.98038+003) + J(0.00000)		1.98038+003	1.11022-016	

SENSITIVITY TO 5 5 ELEMENT OF A MATRIX: BASELINE PARAMETER VALUE = 1.00000+000

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-2.52414+002) + J(0.00000)	(-7.47977+001) + J(0.00000)		7.47977+001	1.80000+002	
(-1.00714+001) + J(1.98371+000)	(-4.67495+001) + J(-2.22679+001)		5.35946+001	-1.55450+002	
(-1.00714+001) + J(-1.98371+000)	(-4.67495+001) + J(2.22679+001)		5.35946+001	1.55450+002	
(-3.37405+000) + J(0.00000)	(-6.07360+002) + J(0.00000)		6.07360+002	1.80000+002	
(-1.49425+000) + J(0.00000)	(1.04557+002) + J(0.00000)		1.04557+002	1.11022-016	

SENSITIVITY TO 1 1 ELEMENT OF B MATRIX: BASELINE PARAMETER VALUE = 1.00000+004

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-2.52414+002) + J(0.00000)	(1.58711+004) + J(0.00000)		1.58711+000	1.11022-016	
(-1.00714+001) + J(1.98371+000)	(9.08498+003) + J(-8.67024+003)		1.25583+000	-4.36619+001	
(-1.00714+001) + J(-1.98371+000)	(9.08498+003) + J(8.67024+003)		1.25583+000	4.36619+001	
(-3.37405+000) + J(0.00000)	(1.33770+003) + J(0.00000)		1.33770+001	1.11022-016	
(-1.49425+000) + J(0.00000)	(1.93695+003) + J(0.00000)		1.93695+001	1.11022-016	

83/454/0.0 OPTIMAL CONTROL DESIGN POINT MPGI
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TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

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SENSITIVITY TO 2 2 ELEMENT OF B      MATRIX:
.....POLE LOCATION.....
REAL      IMAGINARY
( -2.52014+002 ) + J( 0.00000 )
( -1.00714+001 ) + J( 1.98371+000 )
( -1.00714+001 ) + J( -1.98371+000 )
( -3.37425+000 ) + J( 0.00000 )
( -1.48428+000 ) + J( 0.00000 )

.....REAL      IMAGINARY
( 4.08554-004 ) + J( 0.00000 )
( 1.02328-004 ) + J( 3.72230-004 )
( 1.02328-004 ) + J( 3.72230-004 )
( 2.13252-003 ) + J( 0.00000 )
( 5.72507-005 ) + J( 0.00000 )

.....SENSITIVITY.....MAGNITUDE.....PHASE
.....REAL      IMAGINARY
1.63421+001      1.11022-016
1.54415+001      7.46280+001
1.54415+001      -7.46280+001
8.53047+001      1.11022-016
2.29003+002      1.11022-016

BASELINE PARAMETER VALUE = 4.00000+002

SENSITIVITY TO 3 3 ELEMENT OF B      MATRIX:
.....POLE LOCATION.....
REAL      IMAGINARY
( -2.52014+002 ) + J( 0.00000 )
( -1.00714+001 ) + J( 1.98371+000 )
( -1.00714+001 ) + J( -1.98371+000 )
( -3.37425+000 ) + J( 0.00000 )
( -1.48428+000 ) + J( 0.00000 )

.....REAL      IMAGINARY
( 1.17030+000 ) + J( 0.00000 )
( -6.29881-002 ) + J( 4.10432-002 )
( -6.29881-002 ) + J( 4.10432-002 )
( 5.79492-001 ) + J( 0.00000 )
( 7.14172-002 ) + J( 0.00000 )

.....SENSITIVITY.....MAGNITUDE.....PHASE
.....REAL      IMAGINARY
5.85248+001      1.11022-016
3.75892+002      1.46911+002
3.75892+002      -1.46911+002
2.89746+001      1.11022-016
3.57085+002      1.11022-016

BASELINE PARAMETER VALUE = 5.00000+001

SENSITIVITY TO 4 4 ELEMENT OF B      MATRIX:
.....POLE LOCATION.....
REAL      IMAGINARY
( -2.52014+002 ) + J( 0.00000 )
( -1.00714+001 ) + J( 1.98371+000 )
( -1.00714+001 ) + J( -1.98371+000 )
( -3.37425+000 ) + J( 0.00000 )
( -1.48428+000 ) + J( 0.00000 )

.....REAL      IMAGINARY
( 9.49813+000 ) + J( 0.00000 )
( -1.11330+001 ) + J( 3.67397-002 )
( -1.11330+001 ) + J( 3.67397-002 )
( 1.57683-002 ) + J( 0.00000 )
( 3.24799-001 ) + J( 0.00000 )

.....SENSITIVITY.....MAGNITUDE.....PHASE
.....REAL      IMAGINARY
1.49963+000      1.11022-016
2.34470+002      -1.61737+002
2.34470+002      1.61737+002
3.15365+003      1.11022-016
6.49598+002      1.11022-016

BASELINE PARAMETER VALUE = 2.00000+001

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83/45x/0.9 OPTIMAL CONTROL DESIGN POINT MP61 SYSTEMS CONTROL, INC. (VT) - TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

SENSITIVITY TO S S ELEMENT OF B MATRIX: BASELINE PARAMETER VALUE = 1.00000+004

.....POLE LOCATION.....	SENSITIVITY.....		PHASE
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE
(-2.52414+002)	+ J(0.00000)	(7.05693-003)	+ J(0.00000)	7.05693+001
(-1.00714+001)	+ J(1.98371+000)	(-3.50881-005)	+ J(2.07488-005)	4.29381+001
(-1.00714+001)	+ J(-1.98371+000)	(-3.50881-005)	+ J(-2.07488-005)	4.29381+001
(-3.37406+000)	+ J(0.00000)	(-1.97220-006)	+ J(0.00000)	1.97220+002
(-1.43428+000)	+ J(0.00000)	(-7.43365-008)	+ J(0.00000)	7.63365+004
				1.11022-016
				1.44800+002
				1.44800+002
				1.80000+002
				1.80000+002

SYSTEMS CONTROL INC.(VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

4/3/68 3.3 DETAILED CONTROL DESIGN POINT H002

1 SENSITIVITY OF CLOSED LOOP SYSTEM

SENSITIVITY TO 1 1 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -5.15255+002

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-5.23249+002)	+ J(0.00000)	(-1.05138-001)	+ J(0.00000)	5.41728-003	1.80000+002
(-1.37052+001)	+ J(3.84489+000)	(-3.63755-002)	+ J(-6.02711-001)	3.11115-002	-8.55443+001
(-1.37052+001)	+ J(-3.84489+000)	(-3.63755-002)	+ J(6.02711-001)	3.11115-002	8.55443+001
(-3.47335+000)	+ J(7.81584+001)	(-8.79339-003)	+ J(-5.94506+001)	3.06356-002	-9.91527+001
(-3.47335+000)	+ J(-7.81584+001)	(-8.79339-003)	+ J(5.94506+001)	3.06356-002	9.91527+001

SENSITIVITY TO 1 2 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -1.71175+000

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-5.23249+002)	+ J(0.00000)	(-1.54415-002)	+ J(0.00000)	2.64320-002	1.80000+002
(-1.37052+001)	+ J(3.84489+000)	(-5.50890-001)	+ J(-8.32520-001)	1.70805+000	-1.23454+002
(-1.37052+001)	+ J(-3.84489+000)	(-5.50890-001)	+ J(8.32520-001)	1.70805+000	1.23454+002
(-3.47335+000)	+ J(7.81584+001)	(-3.21450-001)	+ J(3.49527-002)	5.53486-001	9.20565+000
(-3.47335+000)	+ J(-7.81584+001)	(-3.21450-001)	+ J(-3.49527-002)	5.53486-001	-9.20565+000

SENSITIVITY TO 1 3 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -4.35730+001

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-5.23249+002)	+ J(0.00000)	(-6.14276-003)	+ J(0.00000)	2.67681-003	1.11022-016
(-1.37052+001)	+ J(3.84489+000)	(-1.58325-003)	+ J(-2.13610-002)	9.33332-001	-9.42443+001
(-1.37052+001)	+ J(-3.84489+000)	(-1.58325-003)	+ J(2.13610-002)	9.33332-001	9.42443+001
(-3.47335+000)	+ J(7.81584+001)	(-6.99358-004)	+ J(-1.55158+003)	7.41511-002	-1.14251+002
(-3.47335+000)	+ J(-7.81584+001)	(-6.99358-004)	+ J(1.55158+003)	7.41511-002	1.14251+002

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

8/10/77 0.2 OPTIMAL CONTROL DESIGN PRINT MAGP

SENSITIVITY TO 1 4 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -6.42553+001

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-5.22209+002) + J(0.00000)	(2.93301-002)	J(0.00000)	1.86462-002	1.11022-016	
(-1.37052+001) + J(3.84059+000)	(5.38061+000)	J(1.41840+000)	3.57544+000	1.47679+001	
(-1.37052+001) + J(-3.84059+000)	(5.38061+000)	J(-1.41840+000)	3.57544+000	-1.47679+001	
(-3.47335+000) + J(7.81584+001)	(-3.47335+000)	J(7.81584+001)	2.55654+001	1.73451+002	
(-3.47335+000) + J(-7.81584+001)	(-3.47335+000)	J(-7.81584+001)	2.55654+001	-1.73451+002	

SENSITIVITY TO 1 5 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -1.09034+001

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-5.22209+002) + J(0.00000)	(1.40524-001)	J(0.00000)	1.53329+000	1.11022-016	
(-1.37052+001) + J(3.84059+000)	(8.34271-003)	J(-6.20099-003)	1.13340+001	-3.66228+001	
(-1.37052+001) + J(-3.84059+000)	(8.34271-003)	J(6.20099+003)	1.13340+001	3.66228+001	
(-3.47335+000) + J(7.81584+001)	(-4.54883-004)	J(9.70083-004)	1.16824+002	1.15123+002	
(-3.47335+000) + J(-7.81584+001)	(-4.54883-004)	J(-9.70083+004)	1.16824+002	-1.15123+002	

SENSITIVITY TO 2 1 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -3.34759+004

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-5.22209+002) + J(0.00000)	(9.28025+002)	J(0.00000)	3.14512+001	1.11022-016	
(-1.37052+001) + J(3.84059+000)	(-7.17903+002)	J(-3.05402+001)	2.43416+001	-1.77564+002	
(-1.37052+001) + J(-3.84059+000)	(-7.17903+002)	J(3.05402+001)	2.43416+001	1.77564+002	
(-3.47335+000) + J(7.81584+001)	(5.06141+002)	J(-2.09796+003)	7.19771+001	-7.34851+001	
(-3.47335+000) + J(-7.81584+001)	(5.06141+002)	J(2.09796+003)	7.19771+001	7.34851+001	

SYSTEMS CONTROL, INC. (VTS) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

83/304/0.2 OPTIMAL CONTROL DESIGN POINT HPG2

SENSITIVITY TO 2 2 ELEMENT OF C		MATRIX:		BASELINE PARAMETER VALUE = -2.31993-004	
.....POLE LOCATION.....					
REAL	IMAGINARY	REAL	IMAGINARY	SENSITIVITY	PHASE
(-5.22212+002) + J(0.00000)	(-2.75941+002) + J(0.00000)	3.15339+002	1.11022-016		
(-1.37032+001) + J(3.84239+000)	(-2.75941+002) + J(6.72110+002)	2.75482-001	1.45528+002		
(-1.37032+001) + J(3.84239+000)	(-2.75941+002) + J(6.72110+002)	2.75482-001	-1.45528+002		
(-3.47335+000) + J(7.51554+001)	(-1.10516+003) + J(4.34740+002)	2.75514+001	2.14733+001		
(-3.47335+000) + J(7.51554+001)	(-1.10516+003) + J(4.34740+002)	2.75514+001	-2.14733+001		
.....POLE LOCATION.....					
REAL	IMAGINARY	REAL	IMAGINARY	SENSITIVITY	PHASE
(-5.22212+002) + J(0.00000)	(-2.75941+002) + J(0.00000)	3.15339+002	1.11022-016		
(-1.37032+001) + J(3.84239+000)	(-2.75941+002) + J(6.72110+002)	2.75482-001	1.45528+002		
(-1.37032+001) + J(3.84239+000)	(-2.75941+002) + J(6.72110+002)	2.75482-001	-1.45528+002		
(-3.47335+000) + J(7.51554+001)	(-1.10516+003) + J(4.34740+002)	2.75514+001	2.14733+001		
(-3.47335+000) + J(7.51554+001)	(-1.10516+003) + J(4.34740+002)	2.75514+001	-2.14733+001		
.....POLE LOCATION.....					
REAL	IMAGINARY	REAL	IMAGINARY	SENSITIVITY	PHASE
(-5.22212+002) + J(0.00000)	(-2.75941+002) + J(0.00000)	3.15339+002	1.11022-016		
(-1.37032+001) + J(3.84239+000)	(-2.75941+002) + J(6.72110+002)	2.75482-001	1.45528+002		
(-1.37032+001) + J(3.84239+000)	(-2.75941+002) + J(6.72110+002)	2.75482-001	-1.45528+002		
(-3.47335+000) + J(7.51554+001)	(-1.10516+003) + J(4.34740+002)	2.75514+001	2.14733+001		
(-3.47335+000) + J(7.51554+001)	(-1.10516+003) + J(4.34740+002)	2.75514+001	-2.14733+001		
.....POLE LOCATION.....					
REAL	IMAGINARY	REAL	IMAGINARY	SENSITIVITY	PHASE
(-5.22212+002) + J(0.00000)	(-2.75941+002) + J(0.00000)	3.15339+002	1.11022-016		
(-1.37032+001) + J(3.84239+000)	(-2.75941+002) + J(6.72110+002)	2.75482-001	1.45528+002		
(-1.37032+001) + J(3.84239+000)	(-2.75941+002) + J(6.72110+002)	2.75482-001	-1.45528+002		
(-3.47335+000) + J(7.51554+001)	(-1.10516+003) + J(4.34740+002)	2.75514+001	2.14733+001		
(-3.47335+000) + J(7.51554+001)	(-1.10516+003) + J(4.34740+002)	2.75514+001	-2.14733+001		

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

AS/3/4/0.0 OPTIMAL CONTROL DESIGN PRINT HPG2

SENSITIVITY TO 2 5 ELEMENT OF C		MATRIX		BASELINE PARAMETER VALUE = 6.78179-003	
.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.22222+002) + J(0.00000)		(-1.24172+003) + J(0.00000)		8.42156+000	1.80000+002
(-1.37052+001) + J(3.54429+000)		(-7.55452+000) + J(9.79554+000)		8.38224+002	-1.27641+002
(-1.37052+001) + J(-3.54429+000)		(-7.55452+000) + J(9.79554+000)		8.38224+002	1.27641+002
(-3.47235+000) + J(7.81580+001)		(-2.54398+000) + J(2.99727+000)		2.68679+002	1.30390+002
(-3.47235+000) + J(-7.81580+001)		(-2.54398+000) + J(-2.99727+000)		2.68679+002	-1.30390+002
.....					
SENSITIVITY TO 3 1 ELEMENT OF C		MATRIX		BASELINE PARAMETER VALUE = 1.02145-002	
.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-5.22222+002) + J(0.00000)		(3.78845+001) + J(0.00000)		3.86971+001	1.11022-016
(-1.37052+001) + J(3.54429+000)		(4.40637+000) + J(-3.33809+001)		4.51379+002	-4.33223+000
(-1.37052+001) + J(-3.54429+000)		(4.40637+000) + J(3.33809+001)		4.51379+002	4.33223+000
(-3.47235+000) + J(7.81580+001)		(-2.97786+001) + J(1.15580+001)		3.26282+001	1.58787+002
(-3.47235+000) + J(-7.81580+001)		(-2.97786+001) + J(-1.15580+001)		3.26282+001	-1.58787+002
.....					
SENSITIVITY TO 3 2 ELEMENT OF C		MATRIX		BASELINE PARAMETER VALUE = 4.39125-003	
.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-5.22222+002) + J(0.00000)		(5.56407+000) + J(0.00000)		2.44332+002	1.11022-016
(-1.37052+001) + J(3.54429+000)		(5.49128+000) + J(-4.81409+000)		3.20480+002	-4.12404+001
(-1.37052+001) + J(-3.54429+000)		(5.49128+000) + J(4.81409+000)		3.20480+002	4.12404+001
(-3.47235+000) + J(7.81580+001)		(-4.74551+000) + J(-1.67107+001)		7.62826+002	-1.04855+002
(-3.47235+000) + J(-7.81580+001)		(-4.74551+000) + J(1.67107+001)		7.62826+002	1.04855+002

SENSITIVITY TO 3 3 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -1.46491+001

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-5.22249+002)	J(0.00000)	(-2.21343-002)	J(0.00000)	3.24247-003	1.80000+002
(-1.37052+001)	J(3.84489+000)	(1.53319-001)	J(3.26735-002)	2.29641-002	-1.20303+001
(-1.37052+001)	J(-3.84489+000)	(1.53319-001)	J(3.26735-002)	2.29641-002	1.20303+001
(-3.47235+000)	J(7.81554+001)	(-5.31515-002)	J(6.61099-002)	1.33930-002	1.33689+002
(-3.47235+000)	J(-7.81554+001)	(-5.31515-002)	J(-6.61099-002)	1.33930-002	-1.33689+002

SENSITIVITY TO 3 4 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 1.12603-003

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-5.22249+002)	J(0.00000)	(-1.05636+001)	J(0.00000)	1.19005-002	1.80000+002
(-1.37052+001)	J(3.84489+000)	(-4.95016+000)	J(4.00216+001)	4.58559-002	9.69820+001
(-1.37052+001)	J(-3.84489+000)	(-4.95016+000)	J(-4.00216+001)	4.58559-002	-9.69820+001
(-3.47235+000)	J(7.81554+001)	(1.02345+001)	J(1.87661+001)	2.40694-002	5.13933+001
(-3.47235+000)	J(-7.81554+001)	(1.02345+001)	J(-1.87661+001)	2.40694-002	-5.13933+001

SENSITIVITY TO 3 5 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 2.78028+001

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-5.22249+002)	J(0.00000)	(-5.06714+001)	J(0.00000)	1.40881+001	1.80000+002
(-1.37052+001)	J(3.84489+000)	(5.32350-002)	J(5.43456-002)	2.11510-002	4.55913+001
(-1.37052+001)	J(-3.84489+000)	(5.32350-002)	J(-5.43456-002)	2.11510-002	-4.55913+001
(-3.47235+000)	J(7.81554+001)	(5.74802-002)	J(3.07506-003)	1.60039-002	3.04228+000
(-3.47235+000)	J(-7.81554+001)	(5.74802-002)	J(-3.07506-003)	1.60039-002	-3.04228+000

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SYSTEMS CONTROL, INC. (VI) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

8/30/70 9.0 ORIGINAL CONTROL DESIGN PRINT 4832

SENSITIVITY TO S ELEMENT OF C		BASELINE PARAMETER VALUE = 4.42427E-003	
POLE LOCATION.....		SENSITIVITY.....	
REAL	IMAGINARY	MAGNITUDE	PHASE
(-5.3924E+002)	+ J(0.0000)	2.80454E+002	1.80000E+002
(-1.3702E+001)	+ J(3.4443E+000)	1.03270E+001	-1.19087E+002
(-1.3702E+001)	+ J(3.4443E+000)	1.03270E+001	1.19087E+002
(-3.4735E+000)	+ J(7.8153E+000)	2.43423E+000	-7.94482E+001
(-3.4735E+000)	+ J(7.8153E+000)	2.43423E+000	7.94482E+001

SENSITIVITY TO 4. 4 ELEMENT OF A MATRIX: BASELINE PARAMETER VALUE = 0.00000

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-5.29249+002) + J(0.00000)	(-5.29249+002)	J(0.00000)	3.02044+000	1.80000+002	
(-1.37052+001) + J(3.84489+000)	(-1.37052+001)	J(3.84489+000)	1.79578+004	-1.59287+002	
(-1.37052+001) + J(-3.84489+000)	(-1.37052+001)	J(-3.84489+000)	1.79578+004	1.59287+002	
(-3.47935+000) + J(7.81584+001)	(-3.47935+000)	J(7.81584+001)	1.61420+003	-6.32432+000	
(-3.47935+000) + J(-7.81584+001)	(-3.47935+000)	J(-7.81584+001)	1.61420+003	6.32432+000	

SENSITIVITY TO 5. 5 ELEMENT OF A MATRIX: BASELINE PARAMETER VALUE = 4.00000+000

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-5.29249+002) + J(0.00000)	(-5.29249+002)	J(0.00000)	2.21487+002	1.40000+002	
(-1.37052+001) + J(3.84489+000)	(-1.37052+001)	J(3.84489+000)	4.29957+001	-1.74348+002	
(-1.37052+001) + J(-3.84489+000)	(-1.37052+001)	J(-3.84489+000)	4.29957+001	1.74348+002	
(-3.47935+000) + J(7.81584+001)	(-3.47935+000)	J(7.81584+001)	3.20676+002	-7.54981+001	
(-3.47935+000) + J(-7.81584+001)	(-3.47935+000)	J(-7.81584+001)	3.20676+002	7.54981+001	

SENSITIVITY TO 1. 1 ELEMENT OF B MATRIX: BASELINE PARAMETER VALUE = 1.00000+000

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-5.29249+002) + J(0.00000)	(-5.29249+002)	J(0.00000)	8.45819+001	1.11022+016	
(-1.37052+001) + J(3.84489+000)	(-1.37052+001)	J(3.84489+000)	2.30336+000	-3.45526+001	
(-1.37052+001) + J(-3.84489+000)	(-1.37052+001)	J(-3.84489+000)	2.30336+000	3.45526+001	
(-3.47935+000) + J(7.81584+001)	(-3.47935+000)	J(7.81584+001)	1.43148+001	-2.90780+000	
(-3.47935+000) + J(-7.81584+001)	(-3.47935+000)	J(-7.81584+001)	1.43148+001	2.90780+000	

SENSITIVITY TO 2 2 ELEMENT OF B MATRIX: BASELINE PARAMETER VALUE = 1.00000+003

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-5.29249+002)	+ J(0.00000)	(6.00167-003)	+ J(0.00000)	6.00167+000	1.11022-016
(-1.37052+001)	+ J(3.84489+000)	(2.36910-004)	+ J(4.43534+004)	5.02841-001	6.18015+001
(-1.37052+001)	+ J(-3.84489+000)	(2.36910-004)	+ J(-4.43534+004)	5.02841+001	-6.18015+001
(-3.47935+000)	+ J(7.81584+001)	(4.42286-004)	+ J(3.78307+004)	5.82007-001	-4.05419+001
(-3.47935+000)	+ J(-7.81584+001)	(4.42286-004)	+ J(-3.78307+004)	5.82007+001	4.05419+001

SENSITIVITY TO 3 3 ELEMENT OF B MATRIX: BASELINE PARAMETER VALUE = 1.00000+000

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-5.29249+002)	+ J(0.00000)	(9.62242+000)	+ J(0.00000)	9.62242+000	1.11022-016
(-1.37052+001)	+ J(3.84489+000)	(-1.15249-001)	+ J(-1.20869+003)	1.15255-001	-1.79399+002
(-1.37052+001)	+ J(-3.84489+000)	(-1.15249-001)	+ J(1.20869+003)	1.15255+001	1.79399+002
(-3.47935+000)	+ J(7.81584+001)	(2.12671-001)	+ J(5.43611+002)	2.19509-001	1.43344+001
(-3.47935+000)	+ J(-7.81584+001)	(2.12671-001)	+ J(-5.43611+002)	2.19509+001	-1.43344+001

SENSITIVITY TO 4 4 ELEMENT OF B MATRIX: BASELINE PARAMETER VALUE = 8.00000+001

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-5.29249+002)	+ J(0.00000)	(1.54773+000)	+ J(0.00000)	1.23818+000	1.11022-016
(-1.37052+001)	+ J(3.84489+000)	(-7.19700-004)	+ J(-1.31961-002)	1.05725-002	-9.31218+001
(-1.37052+001)	+ J(-3.84489+000)	(-7.19700-004)	+ J(1.31961+002)	1.05725+002	9.31218+001
(-3.47935+000)	+ J(7.81584+001)	(1.35798-001)	+ J(6.11160+002)	1.19134-001	2.42301+001
(-3.47935+000)	+ J(-7.81584+001)	(1.35798-001)	+ J(-6.11160+002)	1.19134+001	-2.42301+001

R3/30x10.7 OPTIMAL CONTROL DESIGN POINT HPG2
 SYSTEMS CONTROL, INC. (VT) -
 TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

SENSITIVITY TO S S ELEMENT OF B		MATRIX		BASELINE PARAMETER VALUE = 8.00000+004	
.....POLE LOCATION.....					
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-5.32249+002)	+ J(0.00000)	(2.54783+003)	+ J(0.00000)	2.03826+002	1.11022+016
(-1.37062+001)	+ J(3.84449+000)	(-1.88957+005)	+ J(9.55428+006)	1.69391+000	1.53177+002
(-1.37052+001)	+ J(-3.84449+000)	(-1.88957+005)	+ J(-9.55428+006)	1.69391+000	-1.53177+002
(-3.47935+000)	+ J(7.81540+001)	(-9.85492+008)	+ J(-9.47008+007)	7.61698+002	-9.59411+001
(-3.47935+000)	+ J(-7.81540+001)	(-9.85492+008)	+ J(9.47008+007)	7.61698+002	9.59411+001

83/04/0 OPTIMAL CONTROL DESIGN POINT WPGT

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

1 SENSITIVITY OF CLOSED LOOP SYSTEM 1

SENSITIVITY TO 1 1 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -5.10654+001

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-3.49854+002)	+ J(0.00000)	(7.98152-002)	+ J(0.00000)	4.07579-002	1.11022-016
(-1.00200+001)	+ J(2.96341+000)	(1.93198-001)	+ J(-1.82093+000)	9.35083-001	-8.39437+001
(-1.00200+001)	+ J(-2.96341+000)	(1.93198-001)	+ J(1.82093+000)	9.35083-001	8.39437+001
(-1.05634+001)	+ J(0.00000)	(-6.99481-001)	+ J(0.00000)	3.57193-001	1.80000+002
(-5.13391+000)	+ J(0.00000)	(2.47589-001)	+ J(0.00000)	1.26432-001	1.11022-016

SENSITIVITY TO 1 2 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -1.94638+000

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-3.49854+002)	+ J(0.00000)	(3.95938-002)	+ J(0.00000)	7.70647-002	1.11022-016
(-1.00200+001)	+ J(2.96341+000)	(-2.17297-001)	+ J(-2.86713-001)	7.00217-001	-1.27158+002
(-1.00200+001)	+ J(-2.96341+000)	(-2.17297-001)	+ J(2.86713-001)	7.00217-001	1.27158+002
(-1.05634+001)	+ J(0.00000)	(-1.49016-001)	+ J(0.00000)	2.90042-001	1.80000+002
(-5.13391+000)	+ J(0.00000)	(8.31117-001)	+ J(0.00000)	1.61767+000	1.11022-016

SENSITIVITY TO 1 3 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -3.00513+001

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-3.49854+002)	+ J(0.00000)	(2.19037-004)	+ J(0.00000)	6.58233-003	2.22045-016
(-1.00200+001)	+ J(2.96341+000)	(1.95160-004)	+ J(-1.33938-002)	4.02545-001	-9.91653+001
(-1.00200+001)	+ J(-2.96341+000)	(1.95160-004)	+ J(1.33938-002)	4.02545-001	9.91653+001
(-1.05634+001)	+ J(0.00000)	(5.49572-005)	+ J(0.00000)	1.65153-003	1.11022-016
(-5.13391+000)	+ J(0.00000)	(-3.13331-003)	+ J(0.00000)	9.41601-002	1.80000+002

SENSITIVITY TO 1 4 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -2.40679+001

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-3.49854+002)	+ J(0.00000)	(1.59587+002)	+ J(0.00000)	3.84093+003	1.11022+016
(-1.00200+001)	+ J(2.96341+000)	(4.39244+000)	+ J(2.42695+000)	1.20781+000	2.89220+001
(-1.00200+001)	+ J(-2.96341+000)	(4.39244+000)	+ J(-2.42695+000)	1.20781+000	-2.89220+001
(-1.05634+001)	+ J(0.00000)	(3.83773+000)	+ J(0.00000)	9.23662+001	1.11022+016
(-6.13391+000)	+ J(0.00000)	(-2.63857+000)	+ J(0.00000)	6.35050+001	1.80000+002

SENSITIVITY TO 1 5 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 2.85502+000

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-3.49854+002)	+ J(0.00000)	(-1.45049+001)	+ J(0.00000)	4.14117+001	1.80000+002
(-1.00200+001)	+ J(2.96341+000)	(3.77374+003)	+ J(-3.32320+003)	1.43562+002	-4.13675+001
(-1.00200+001)	+ J(-2.96341+000)	(3.77374+003)	+ J(3.32320+003)	1.43562+002	4.13675+001
(-1.05634+001)	+ J(0.00000)	(8.22401+003)	+ J(0.00000)	2.34797+002	1.11022+016
(-6.13391+000)	+ J(0.00000)	(-1.82299+003)	+ J(0.00000)	5.20467+003	1.80000+002

SENSITIVITY TO 2 1 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -1.90720+004

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-3.49854+002)	+ J(0.00000)	(-2.37805+002)	+ J(0.00000)	4.53541+002	1.80000+002
(-1.00200+001)	+ J(2.96341+000)	(-5.27256+003)	+ J(-1.00375+004)	2.16240+000	-1.17712+002
(-1.00200+001)	+ J(-2.96341+000)	(-5.27256+003)	+ J(1.00375+004)	2.16240+000	1.17712+002
(-1.05634+001)	+ J(0.00000)	(8.52568+003)	+ J(0.00000)	1.81674+000	1.11022+016
(-6.13391+000)	+ J(0.00000)	(9.01947+002)	+ J(0.00000)	1.72019+001	1.11022+016

SENSITIVITY TO 2 2 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -4.56350+005

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-3.49854+002)	+ J(0.00000)	(-1.17967+002)	+ J(0.00000)	5.38344+003	1.80000+002
(-1.00200+001)	+ J(2.96341+000)	(-2.10323+003)	+ J(-7.27898+002)	1.01553+001	1.60927+002
(-1.00200+001)	+ J(-2.96341+000)	(-2.10323+003)	+ J(7.27898+002)	1.01553+001	1.60927+002
(-1.06634+001)	+ J(0.00000)	(2.02933+003)	+ J(0.00000)	9.26086+002	1.11022-016
(-6.13391+000)	+ J(0.00000)	(3.02769+003)	+ J(0.00000)	1.38168+001	1.11022-016

SENSITIVITY TO 2 3 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 3.71416+002

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-3.49854+002)	+ J(0.00000)	(-6.52607+001)	+ J(0.00000)	2.42388+002	1.80000+002
(-1.00200+001)	+ J(2.96341+000)	(-4.50923+001)	+ J(-6.96119+001)	3.08054+000	1.22934+002
(-1.00200+001)	+ J(-2.96341+000)	(-4.50923+001)	+ J(6.96119+001)	3.08054+000	1.22934+002
(-1.06634+001)	+ J(0.00000)	(-7.48418+001)	+ J(0.00000)	2.77974+002	1.80000+002
(-6.13391+000)	+ J(0.00000)	(-1.14144+001)	+ J(0.00000)	4.23949+001	1.80000+002

SENSITIVITY TO 2 4 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 2.05994+005

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-3.49854+002)	+ J(0.00000)	(-4.75481+001)	+ J(0.00000)	9.79461+004	1.80000+002
(-1.00200+001)	+ J(2.96341+000)	(3.09613+004)	+ J(-2.62530+003)	6.40073+001	4.84668+000
(-1.00200+001)	+ J(-2.96341+000)	(3.09613+004)	+ J(2.62530+003)	6.40073+001	4.84668+000
(-1.06634+001)	+ J(0.00000)	(-5.22630+004)	+ J(0.00000)	1.07659+000	1.80000+002
(-6.13391+000)	+ J(0.00000)	(-9.61211+003)	+ J(0.00000)	1.98003+001	1.80000+002

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SENSITIVITY TO 2 5 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -3.1660E+004

.....REALPOLE LOCATION..... IMAGINARYREALIMAGINARYSENSITIVITY..... MAGNITUDEPHASE
(-3.49854+002) + J(0.00000)	(4.32164+002) + J(0.00000)	1.36827-001	1.11022-016		
(-1.00200+001) + J(2.96341+000)	(7.98680+000) + J(-3.00929+001)	9.85754-003	-7.51362+001		
(-1.00200+001) + J(-2.96341+000)	(7.98680+000) + J(3.00929+001)	9.85754-003	7.51362+001		
(-1.05634+001) + J(0.00000)	(-1.11998+002) + J(0.00000)	3.54590-002	1.80000+002		
(-6.13391+000) + J(0.00000)	(-6.64099+000) + J(0.00000)	2.10239-003	1.80000+002		

SENSITIVITY TO 3 1 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 6.11540E+003

.....REALPOLE LOCATION..... IMAGINARYREALIMAGINARYSENSITIVITY..... MAGNITUDEPHASE
(-3.49854+002) + J(0.00000)	(1.45257+001) + J(0.00000)	8.88303-002	1.11022-016		
(-1.00200+001) + J(2.96341+000)	(2.47530+001) + J(1.67108+002)	1.03308+000	9.15744+001		
(-1.00200+001) + J(-2.96341+000)	(2.47530+001) + J(-1.67108+002)	1.03308+000	-9.15744+001		
(-1.05634+001) + J(0.00000)	(-1.63292+002) + J(0.00000)	9.98597-001	1.80000+002		
(-6.13391+000) + J(0.00000)	(2.00517-001) + J(0.00000)	1.22624-003	1.11022-016		

SENSITIVITY TO 3 2 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -9.05701E+004

.....REALPOLE LOCATION..... IMAGINARYREALIMAGINARYSENSITIVITY..... MAGNITUDEPHASE
(-3.49854+002) + J(0.00000)	(7.20573+000) + J(0.00000)	6.52624-003	1.11022-016		
(-1.00200+001) + J(2.96341+000)	(2.60243+001) + J(2.05969+001)	3.00591-002	3.83598+001		
(-1.00200+001) + J(-2.96341+000)	(2.60243+001) + J(-2.05969+001)	3.00591-002	-3.83598+001		
(-1.05634+001) + J(0.00000)	(-1.47875+001) + J(0.00000)	3.15070-002	1.80000+002		
(-6.13391+000) + J(0.00000)	(6.73101-001) + J(0.00000)	6.09629-004	0.00000		

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SENSITIVITY TO 3 3 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 3.57681+001

.....POLE LOCATION.....	SENSITIVITY.....		PHASE
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE
(-3.49554+002)	+ J(0.00000)	(3.96628+002)	+ J(0.00000)	1.42582+002
(-1.00200+001)	+ J(2.95341+000)	(2.91573+001)	+ J(1.20088+000)	4.42012+001
(-1.00200+001)	+ J(-2.95341+000)	(2.91573+001)	+ J(-1.20088+000)	4.42012+001
(-1.05634+001)	+ J(0.00000)	(1.28296+002)	+ J(0.00000)	4.58891+003
(-6.13391+000)	+ J(0.00000)	(-2.53759+003)	+ J(0.00000)	9.07649+004
				1.80000+002

SENSITIVITY TO 3 4 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 8.89014+005

.....POLE LOCATION.....	SENSITIVITY.....		PHASE
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE
(-3.49554+002)	+ J(0.00000)	(2.90435+000)	+ J(0.00000)	2.58201+004
(-1.00200+001)	+ J(2.95341+000)	(-4.48338+002)	+ J(-1.15446+002)	4.11581+002
(-1.00200+001)	+ J(-2.95341+000)	(-4.48338+002)	+ J(1.15446+002)	4.11581+002
(-1.05634+001)	+ J(0.00000)	(8.95908+002)	+ J(0.00000)	7.96475+002
(-6.13391+000)	+ J(0.00000)	(-2.13692+000)	+ J(0.00000)	1.89375+004
				1.90000+002

SENSITIVITY TO 3 5 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 4.60516+002

.....POLE LOCATION.....	SENSITIVITY.....		PHASE
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE
(-3.49554+002)	+ J(0.00000)	(-2.3976+001)	+ J(0.00000)	1.21565+000
(-1.00200+001)	+ J(2.95341+000)	(-2.60414+001)	+ J(3.83901+001)	2.13629+002
(-1.00200+001)	+ J(-2.95341+000)	(-2.60414+001)	+ J(-3.83901+001)	2.13629+002
(-1.05634+001)	+ J(0.00000)	(1.91987+000)	+ J(0.00000)	8.84132+002
(-6.13391+000)	+ J(0.00000)	(-1.47639+003)	+ J(0.00000)	6.79302+005
				1.80000+002

SENSITIVITY TO 4 1 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -0.83116-000

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-3.43854+002) + J(0.00000)	(-3.48281+001) + J(0.00000)		1.68260-002	1.80000+002	
(-1.00200+001) + J(2.95341+000)	(-2.23067+001) + J(4.77772+001)		2.54738-002	-1.15027+002	
(-1.00200+001) + J(2.95341+000)	(-2.23067+001) + J(4.77772+001)		2.54738-002	1.15027+002	
(-1.05634+001) + J(0.00000)	(7.73030+001) + J(0.00000)		3.73683-002	1.11022-016	
(-6.13391+000) + J(0.00000)	(-1.33516+001) + J(0.00000)		6.45037-003	1.80000+002	

SENSITIVITY TO 4 2 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 7.24900-003

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-3.43854+002) + J(0.00000)	(-1.72771+001) + J(0.00000)		1.25242-001	1.80000+002	
(-1.00200+001) + J(2.95341+000)	(-9.62110+000) + J(3.84000+000)		7.50932-002	-1.58242+002	
(-1.00200+001) + J(2.95341+000)	(-9.62110+000) + J(3.84000+000)		7.50932-002	1.58242+002	
(-1.05634+001) + J(0.00000)	(1.56855+001) + J(0.00000)		1.19380-001	1.11022-016	
(-6.13391+000) + J(0.00000)	(-4.45192+001) + J(0.00000)		3.24894-001	1.80000+002	

SENSITIVITY TO 4 3 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -1.89024-001

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-3.43854+002) + J(0.00000)	(-9.55787-002) + J(0.00000)		1.80666-002	1.80000+002	
(-1.00200+001) + J(2.95341+000)	(-1.94308-001) + J(3.33200-001)		7.29096-002	-1.20249+002	
(-1.00200+001) + J(2.95341+000)	(-1.94308-001) + J(3.33200-001)		7.29096-002	1.20249+002	
(-1.05634+001) + J(0.00000)	(-6.07358-003) + J(0.00000)		1.14805-003	1.80000+002	
(-6.13391+000) + J(0.00000)	(1.68768-001) + J(0.00000)		3.19390-002	1.11022-016	

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SENSITIVITY TO 4 4 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -7.64106+005

.....POLE LOCATION..... REALSENSITIVITY..... IMAGINARY	MAGNITUDE	PHASE
(-3.49650+002) + J(0.00000)	(-6.93373+000) + J(0.00000)	5.32103+004	1.80000+002
(-1.00200+001) + J(2.96341+000)	(1.40400+002) + J(-5.45089+000)	1.10416+002	-2.16180+000
(-1.00200+001) + J(-2.96341+000)	(1.40400+002) + J(5.45089+000)	1.10416+002	2.16180+000
(-1.06634+001) + J(0.00000)	(-4.24126+002) + J(0.00000)	3.24077+002	1.80000+002
(-6.13391+000) + J(0.00000)	(1.42289+002) + J(0.00000)	1.09724+002	1.11022+016

SENSITIVITY TO 4 5 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -2.32416+001

.....POLE LOCATION..... REALSENSITIVITY..... IMAGINARY	MAGNITUDE	PHASE
(-3.49650+002) + J(0.00000)	(6.32933+001) + J(0.00000)	1.47104+001	1.11022+016
(-1.00200+001) + J(2.96341+000)	(4.35576+002) + J(-1.38054+001)	3.36522+002	-7.24513+001
(-1.00200+001) + J(-2.96341+000)	(4.35576+002) + J(1.38054+001)	3.36522+002	7.24513+001
(-1.06634+001) + J(0.00000)	(-9.08874+001) + J(0.00000)	2.11237+001	1.80000+002
(-6.13391+000) + J(0.00000)	(9.83071+002) + J(0.00000)	2.28482+002	1.11022+016

SENSITIVITY TO 5 1 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -7.93757+006

.....POLE LOCATION..... REALSENSITIVITY..... IMAGINARY	MAGNITUDE	PHASE
(-3.49650+002) + J(0.00000)	(3.53549+004) + J(0.00000)	2.80632+001	1.11022+016
(-1.00200+001) + J(2.96341+000)	(-1.31658+004) + J(-5.05253+003)	1.11935+001	-1.59005+002
(-1.00200+001) + J(-2.96341+000)	(-1.31658+004) + J(5.05253+003)	1.11935+001	1.59005+002
(-1.06634+001) + J(0.00000)	(1.54331+004) + J(0.00000)	1.22501+001	1.11022+016
(-6.13391+000) + J(0.00000)	(-2.23652+003) + J(0.00000)	1.79113+002	1.80000+002

SENSITIVITY TO S 2 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 7.52679-005

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.49834+002) + J(0.00000)	(1.75385+004) + J(0.00000)	(1.32008+000)		1.11022-016	
(-1.00200+001) + J(2.98341+000)	(-2.56478+003) + J(1.04769+003)	2.08531-001		1.57781+002	
(-1.00200+001) + J(-2.98341+000)	(-2.56478+003) + J(-1.04769+003)	2.08531-001		-1.57781+002	
(-1.05634+001) + J(0.00000)	(3.28784+003) + J(0.00000)	2.47469-001		1.11022-016	
(-6.13391+000) + J(0.00000)	(-7.57478+003) + J(0.00000)	5.70136-001		1.80000+002	

SENSITIVITY TO S 3 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 6.05981-003

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.49834+002) + J(0.00000)	(9.70245+001) + J(0.00000)	5.87950-001		1.11022-016	
(-1.00200+001) + J(2.98341+000)	(-9.92744+001) + J(2.80420+001)	6.25124-001		-1.64227+002	
(-1.00200+001) + J(-2.98341+000)	(-9.92744+001) + J(2.80420+001)	6.25124-001		1.64227+002	
(-1.05634+001) + J(0.00000)	(-1.21255+000) + J(0.00000)	7.14785-003		1.80000+002	
(-6.13391+000) + J(0.00000)	(2.85558+001) + J(0.00000)	1.73049-001		1.11022-016	

SENSITIVITY TO S 4 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 1.13751-005

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.49834+002) + J(0.00000)	(7.06907+003) + J(0.00000)	8.04114-002		1.11022-016	
(-1.00200+001) + J(2.98341+000)	(2.67787+004) + J(-2.78556+004)	4.39614-001		-4.61395+001	
(-1.00200+001) + J(-2.98341+000)	(2.67787+004) + J(2.78556+004)	4.39614-001		4.61395+001	
(-1.05634+001) + J(0.00000)	(-8.46742+004) + J(0.00000)	9.63180-001		1.80000+002	
(-6.13391+000) + J(0.00000)	(2.40478+004) + J(0.00000)	2.73547-001		1.11022-016	

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SENSITIVITY TO 5 5 ELEMENT OF C MATRIX BASELINE PARAMETER VALUE = 2.51112-003

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-3.42434+002)	+ J(0.00000)	(-6.42507+004)	+ J(0.00000)	1.61341+002	1.80000+002
(-1.00200+001)	+ J(2.95341+000)	(-1.72358+001)	+ J(-3.46772+001)	9.72416-002	-1.16429+002
(-1.00200+001)	+ J(-2.95341+000)	(-1.72358+001)	+ J(3.46772+001)	9.72416-002	1.16429+002
(-1.05434+001)	+ J(0.00000)	(-1.81451+002)	+ J(0.00000)	4.55646-001	1.80000+002
(-6.13331+000)	+ J(0.00000)	(1.66146+001)	+ J(0.00000)	4.17212-002	1.11022-016

***** SENSITIVITY OF OPTIMAL CONTROLLED DESIGN *****

SENSITIVITY TO 1 1 ELEMENT OF A MATRIX: BASELINE PARAMETER VALUE = 1.00000+003

.....POLE LOCATION.....SENSITIVITY.....PHASE.....
REAL	IMAGINARY	MAGNITUDE
(-3.49854+002) + J(0.00000)	(-2.64226+000) + J(0.00000)	1.80000+002
(-1.00200+001) + J(2.95341+000)	(-1.24177+002) + J(1.92087+003)	9.34989+001
(-1.00200+001) + J(-2.95341+000)	(-1.24177+002) + J(-1.92087+003)	9.34989+001
(-1.05634+001) + J(0.00000)	(-1.11012+003) + J(0.00000)	1.80000+002
(-6.13391+000) + J(0.00000)	(-1.96304+002) + J(0.00000)	1.80000+002

SENSITIVITY TO 2 2 ELEMENT OF A MATRIX: BASELINE PARAMETER VALUE = 2.00000+003

.....POLE LOCATION.....SENSITIVITY.....PHASE.....
REAL	IMAGINARY	MAGNITUDE
(-3.49854+002) + J(0.00000)	(-2.67735+000) + J(0.00000)	1.80000+002
(-1.00200+001) + J(2.95341+000)	(7.31817+001) + J(1.21768+002)	5.89945+001
(-1.00200+001) + J(-2.95341+000)	(7.31817+001) + J(-1.21768+002)	5.89945+001
(-1.05634+001) + J(0.00000)	(2.53078+001) + J(0.00000)	1.11022+016
(-6.13391+000) + J(0.00000)	(-7.48078+002) + J(0.00000)	1.80000+002

SENSITIVITY TO 3 3 ELEMENT OF A MATRIX: BASELINE PARAMETER VALUE = 5.00000+000

.....POLE LOCATION.....SENSITIVITY.....PHASE.....
REAL	IMAGINARY	MAGNITUDE
(-3.49854+002) + J(0.00000)	(1.43333+004) + J(0.00000)	1.11022+016
(-1.00200+001) + J(2.95341+000)	(-8.94498+002) + J(-1.62439+001)	9.27195+001
(-1.00200+001) + J(-2.95341+000)	(-8.94498+002) + J(1.62439+001)	9.27195+001
(-1.05634+001) + J(0.00000)	(-1.71170+003) + J(0.00000)	8.55850+003
(-6.13391+000) + J(0.00000)	(-2.26132+002) + J(0.00000)	1.13066+001

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SENSITIVITY TO 4 4 ELEMENT OF A MATRIX BASELINE PARAMETER VALUE = 0.00000
.....POLE LOCATION.....
REAL IMAGINARY SENSITIVITY MAGNITUDE PHASE

(-3.49954+002) + J(0.00000) (-3.77440+000) + J(0.00000) 3.77440+000 1.80000+002
(-1.00200+001) + J(2.96341+000) (-1.64239+004) + J(-1.15251+004) 2.00643+004 1.40942+002
(-1.00200+001) + J(-2.96341+000) (-1.64239+004) + J(1.15251+004) 2.00643+004 1.40942+002
(-1.05534+001) + J(0.00000) (-1.61073+004) + J(0.00000) 1.61073+004 1.80000+002
(-2.13391+000) + J(0.00000) (-1.14969+004) + J(0.00000) 1.14969+004 1.11022+016

SENSITIVITY TO 5 5 ELEMENT OF A MATRIX BASELINE PARAMETER VALUE = 2.00000+000
.....POLE LOCATION.....
REAL IMAGINARY SENSITIVITY MAGNITUDE PHASE

(-3.49954+002) + J(0.00000) (-5.57147+001) + J(0.00000) 1.31429+002 1.80000+002
(-1.00200+001) + J(2.96341+000) (-2.92959+002) + J(-8.38775+002) 1.77693+001 1.09253+002
(-1.00200+001) + J(-2.96341+000) (-2.92959+002) + J(8.38775+002) 1.77693+001 1.09253+002
(-1.05534+001) + J(0.00000) (-4.01518+001) + J(0.00000) 8.03036+001 1.80000+002
(-2.13391+000) + J(0.00000) (-1.16402+002) + J(0.00000) 2.36804+002 1.11022+016

SENSITIVITY TO 1 1 ELEMENT OF B MATRIX BASELINE PARAMETER VALUE = 1.00000+004
.....POLE LOCATION.....
REAL IMAGINARY SENSITIVITY MAGNITUDE PHASE

(-3.49954+002) + J(0.00000) (4.61646+003) + J(0.00000) 4.61646+001 1.11022+016
(-1.00200+001) + J(2.96341+000) (5.46826+003) + J(-1.07207+004) 1.20348+000 6.29755+001
(-1.00200+001) + J(-2.96341+000) (5.46826+003) + J(1.07207+004) 1.20348+000 6.29755+001
(-1.05534+001) + J(0.00000) (2.20826+003) + J(0.00000) 2.20826+001 1.11022+016
(-2.13391+000) + J(0.00000) (7.17193+003) + J(0.00000) 7.17193+001 1.11022+016

SYSTEMS CONTROL INC.(VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

R3/0K/0 OPTIMAL CONTROL DESIGN POINT HPG3

SENSITIVITY TO 2 2 ELEMENT OF B MATRIX: BASELINE PARAMETER VALUE = 2.00000+003

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-3.43454+002)	J(0.00000)	(5.13459-005)	J(0.00000)	1.02772-001
(-1.02200+001)	J(2.95341+000)	(-1.33789-005)	J(2.72559-004)	5.46374-001
(-1.02200+001)	J(-2.95341+000)	(-1.33789-005)	J(-2.72559-004)	5.46374-001
(-1.02200+001)	J(0.00000)	(1.15623-003)	J(0.00000)	2.31247-000
(-6.13391+000)	J(0.00000)	(3.69920-004)	J(0.00000)	7.33984-001

SENSITIVITY TO 3 3 ELEMENT OF B MATRIX: BASELINE PARAMETER VALUE = 2.00000+000

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-3.43454+002)	J(0.00000)	(4.44653-001)	J(0.00000)	8.89306-001
(-1.02200+001)	J(2.95341+000)	(6.47936-003)	J(-2.24193-001)	4.48573-001
(-1.02200+001)	J(-2.95341+000)	(6.47936-003)	J(2.24193-001)	4.48573-001
(-1.02200+001)	J(0.00000)	(3.39577-001)	J(0.00000)	6.77154-001
(-6.13391+000)	J(0.00000)	(-1.20504-002)	J(0.00000)	2.41008-002

SENSITIVITY TO 4 4 ELEMENT OF B MATRIX: BASELINE PARAMETER VALUE = 1.00000+000

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-3.43454+002)	J(0.00000)	(1.12090+001)	J(0.00000)	1.12090+001
(-1.02200+001)	J(2.95341+000)	(5.12822-002)	J(-1.16005-001)	1.26834-001
(-1.02200+001)	J(-2.95341+000)	(5.12822-002)	J(1.16005-001)	1.26834-001
(-1.02200+001)	J(0.00000)	(-3.72866-001)	J(0.00000)	3.72866-001
(-6.13391+000)	J(0.00000)	(3.43799-001)	J(0.00000)	3.43799-001

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

83/04/0 OPTIMAL CONTROL DESIGN POINT HPGX

SENSITIVITY TO 5 5 ELEMENT OF R MATRIX BASELINE PARAMETER VALUE = 1.00000+005

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.49854+002)	+ J(0.00000)	(1.18788-003)	+ J(0.00000)	1.18788+002	1.11022-016
(-1.00200+001)	+ J(2.95341+000)	(-1.00607-006)	+ J(-9.38336-007)	1.37574-001	-1.36995+002
(-1.00200+001)	+ J(-2.95341+000)	(-1.00607-006)	+ J(9.38336-007)	1.37574-001	1.36995+002
(-1.05634+001)	+ J(0.00000)	(-9.65378-006)	+ J(0.00000)	9.65378-001	1.80000+002
(-4.13331+000)	+ J(0.00000)	(5.29129-005)	+ J(0.00000)	5.29129-003	1.11022-016

1 SENSITIVITY OF CLOSED LOOP SYSTEM 1

SENSITIVITY TO 1 1 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -1.10079+000

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.85272+002)	+ J(0.00000)	(3.56017-001)	+ J(0.00000)	3.91900-001	1.11022-016
(-1.22957+001)	+ J(4.12893+000)	(1.87598-001)	+ J(-2.14176+000)	2.36665+000	-8.49943+001
(-1.22957+001)	+ J(-4.12893+000)	(1.87598-001)	+ J(2.14176+000)	2.36665+000	8.49943+001
(-8.32037+000)	+ J(3.35619+000)	(-3.81481-001)	+ J(-1.52805+001)	4.52284-001	-1.58197+002
(-8.32037+000)	+ J(-3.35619+000)	(-3.81481-001)	+ J(1.52805+001)	4.52284-001	1.58197+002

SENSITIVITY TO 1 2 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -2.65115+000.

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.85272+002)	+ J(0.00000)	(1.50717-001)	+ J(0.00000)	3.99573-001	1.11022-016
(-1.22957+001)	+ J(4.12893+000)	(1.32008-001)	+ J(8.17788-002)	4.11687-001	3.17783+001
(-1.22957+001)	+ J(-4.12893+000)	(1.32008-001)	+ J(-8.17788-002)	4.11687-001	-3.17783+001
(-8.32037+000)	+ J(3.35619+000)	(1.22784-001)	+ J(-3.24665-001)	9.20233-001	-5.92841+001
(-8.32037+000)	+ J(-3.35619+000)	(1.22784-001)	+ J(3.24665-001)	9.20233-001	5.92841+001

SENSITIVITY TO 1 3 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 1.65710+001

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.85272+002)	+ J(0.00000)	(8.71190-004)	+ J(0.00000)	1.44365-002	1.11022-016
(-1.22957+001)	+ J(4.12893+000)	(-3.45170-003)	+ J(-1.44296-002)	2.45859-001	-1.03453+002
(-1.22957+001)	+ J(-4.12893+000)	(-3.45170-003)	+ J(1.44296-002)	2.45859-001	1.03453+002
(-8.32037+000)	+ J(3.35619+000)	(1.85811-003)	+ J(1.56888-003)	4.02983-002	4.01758+001
(-8.32037+000)	+ J(-3.35619+000)	(1.85811-003)	+ J(-1.56888-003)	4.02983-002	-4.01758+001

R370X/1.2 OPTIMAL CONTROL DESIGN POINT HPG4

SENSITIVITY TO 1 4 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -3.54623-001

.....POLE LOCATION.....REALIMAGINARYSENSITIVITY.....MAGNITUDE.....PHASE.....
(-2.85272+002) + J(0.00000)	(1.94907-001)	J(0.00000)	6.98277-002	1.11022-016	
(-1.22257+001) + J(4.12893+000)	(3.82169+000)	J(2.20907+000)	1.56538+000	3.00294+001	
(-1.22257+001) + J(4.12893+000)	(3.82169+000)	J(2.20907+000)	1.56538+000	-3.00294+001	
(-8.32037+000) + J(3.35619+000)	(1.07986+000)	J(1.23358+000)	5.81387-001	4.88015+001	
(-8.32037+000) + J(3.35619+000)	(1.07986+000)	J(1.23358+000)	5.81387-001	-4.88015+001	

SENSITIVITY TO 1 5 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 8.07091+000

.....POLE LOCATION.....REALIMAGINARYSENSITIVITY.....MAGNITUDE.....PHASE.....
(-2.85272+002) + J(0.00000)	(-5.62097-001)	J(0.00000)	4.59313+000	1.80000+002	
(-1.22257+001) + J(4.12893+000)	(2.22380-002)	J(-5.88629-003)	1.85662-001	-1.48259+001	
(-1.22257+001) + J(4.12893+000)	(2.22380-002)	J(5.88629-003)	1.85662-001	1.48259+001	
(-8.32037+000) + J(3.35619+000)	(3.11058-003)	J(-5.90386-003)	5.38586-002	-6.22166+001	
(-8.32037+000) + J(3.35619+000)	(3.11058-003)	J(5.90386-003)	5.38586-002	6.22166+001	

SENSITIVITY TO 2 1 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -9.85169-005

.....POLE LOCATION.....REALIMAGINARYSENSITIVITY.....MAGNITUDE.....PHASE.....
(-2.85272+002) + J(0.00000)	(1.03304+003)	J(0.00000)	1.01516-001	1.11022-016	
(-1.22257+001) + J(4.12893+000)	(-4.70855+003)	J(-6.11991+003)	7.60712-001	-1.27574+002	
(-1.22257+001) + J(4.12893+000)	(-4.70855+003)	J(6.11991+003)	7.60712-001	1.27574+002	
(-8.32037+000) + J(3.35619+000)	(4.16080+003)	J(-5.33786+002)	4.13269-001	-7.31050+000	
(-8.32037+000) + J(3.35619+000)	(4.16080+003)	J(5.33786+002)	4.13269-001	7.31050+000	

83/04/1.2 OPTIMAL CONTROL DESIGN POINT MPSU

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

SENSITIVITY TO 2 2 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -1.41500+004

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-2.85272+002)	+ J(0.00000)		6.17265+002	1.11022-016
(-1.22937+001)	+ J(4.12893+000)		7.89166+002	-1.08016+001
(-1.22937+001)	+ J(4.12893+000)		7.89166+002	1.08016+001
(-8.32037+000)	+ J(3.35619+000)		5.01459+001	8.14025+001
(-8.32037+000)	+ J(3.35619+000)		5.01459+001	-8.14025+001

SENSITIVITY TO 2 3 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 2.79849+002

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-2.85272+002)	+ J(0.00000)		7.05651+002	1.11022-016
(-1.22937+001)	+ J(4.12893+000)		1.49122+000	-1.46033+002
(-1.22937+001)	+ J(4.12893+000)		1.49122+000	1.46033+002
(-8.32037+000)	+ J(3.35619+000)		6.94828+001	1.68318+002
(-8.32037+000)	+ J(3.35619+000)		6.94828+001	1.68318+002

SENSITIVITY TO 2 4 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 8.76632+008

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-2.85272+002)	+ J(0.00000)		4.9610+005	1.11022-016
(-1.22937+001)	+ J(4.12893+000)		1.38979+003	-1.25505+001
(-1.22937+001)	+ J(4.12893+000)		1.38979+003	1.25505+001
(-8.32037+000)	+ J(3.35619+000)		1.46734+003	-1.60312+002
(-8.32037+000)	+ J(3.35619+000)		1.46734+003	1.60312+002

83/06/1.2 OPTIMAL CONTROL DESIGN POINT WPG4

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

SENSITIVITY TO 2 5 ELEMENT OF C MATRIX BASELINE PARAMETER VALUE = 7.40016+004

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.85272+002)	+ J(0.00000)	1.21894+000		1.80000+002	
(-1.22957+001)	+ J(4.12893+000)	6.11392+002		-5.74058+001	
(-1.22957+001)	+ J(-4.12893+000)	6.11392+002		5.74058+001	
(-8.32037+000)	+ J(3.35561+000)	5.04184+002		8.86700+001	
(-8.32037+000)	+ J(-3.35561+000)	5.04184+002		-8.86700+001	

SENSITIVITY TO 3 1 ELEMENT OF C MATRIX BASELINE PARAMETER VALUE = 2.28333+003

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.85272+002)	+ J(0.00000)	3.33889+001		1.80000+002	
(-1.22957+001)	+ J(4.12893+000)	2.82824+001		1.02300+002	
(-1.22957+001)	+ J(-4.12893+000)	2.82824+001		-1.02300+002	
(-8.32037+000)	+ J(3.35561+000)	1.43631+001		1.67812+002	
(-8.32037+000)	+ J(-3.35561+000)	1.43631+001		-1.67812+002	

SENSITIVITY TO 3 2 ELEMENT OF C MATRIX BASELINE PARAMETER VALUE = 4.11474+004

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.85272+002)	+ J(0.00000)	2.58436+002		1.80000+002	
(-1.22957+001)	+ J(4.12893+000)	3.73489+003		-1.40922+002	
(-1.22957+001)	+ J(-4.12893+000)	3.73489+003		1.40922+002	
(-8.32037+000)	+ J(3.35561+000)	2.21833+002		-1.03275+002	
(-8.32037+000)	+ J(-3.35561+000)	2.21833+002		1.03275+002	

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

R3/OK/1.2 OPTIMAL CONTROL DESIGN POINT HPG

SENSITIVITY TO 3 3 ELEMENT OF C		MATRIX		BASELINE PARAMETER VALUE = -1.35335-001	
.....POLE LOCATION..... REAL IMAGINARY	REAL IMAGINARY	SENSITIVITY..... MAGNITUDE PHASE	
(-2.45272+002) + J(0.00000)		(-3.57829-001) + J(0.00000)		4.84269-002 1.90000+002	
(-1.22957+001) + J(4.12893+000)		(9.16169-002) + J(8.49855-001)		1.15682-001 8.38472+001	
(-1.22957+001) + J(-4.12893+000)		(9.16169-002) + J(-8.49855-001)		1.15682-001 -8.38472+001	
(-8.32037+000) + J(3.35619+000)		(3.70148-001) + J(4.01119-002)		5.03873-002 5.03873-002	
(-8.32037+000) + J(-3.35619+000)		(3.70148-001) + J(-4.01119-002)		5.03873-002 -5.03873-002	
SENSITIVITY TO 3 4 ELEMENT OF C		MATRIX		BASELINE PARAMETER VALUE = -2.23093-005	
.....POLE LOCATION..... REAL IMAGINARY	REAL IMAGINARY	SENSITIVITY..... MAGNITUDE PHASE	
(-2.45272+002) + J(0.00000)		(-8.08768+001) + J(0.00000)		1.80430-003 1.80000+002	
(-1.22957+001) + J(4.12893+000)		(-2.02221+002) + J(-1.54215+002)		5.67356-003 -1.42671+002	
(-1.22957+001) + J(-4.12893+000)		(-2.02221+002) + J(1.54215+002)		5.67356-003 1.42671+002	
(-8.32037+000) + J(3.35619+000)		(2.42659+002) + J(6.41612+001)		5.59959-003 1.48106+001	
(-8.32037+000) + J(-3.35619+000)		(2.42659+002) + J(-6.41612+001)		5.59959-003 -1.48106+001	
SENSITIVITY TO 3 5 ELEMENT OF C		MATRIX		BASELINE PARAMETER VALUE = -4.75250-002	
.....POLE LOCATION..... REAL IMAGINARY	REAL IMAGINARY	SENSITIVITY..... MAGNITUDE PHASE	
(-2.45272+002) + J(0.00000)		(2.33749+002) + J(0.00000)		1.11089+001 1.11022-016	
(-1.22957+001) + J(4.12893+000)		(-1.31389+000) + J(1.73582-001)		6.29852-002 1.72474+002	
(-1.22957+001) + J(-4.12893+000)		(-1.31389+000) + J(-1.73582-001)		6.29852-002 -1.72474+002	
(-8.32037+000) + J(3.35619+000)		(-1.10471-001) + J(-1.01567+000)		4.85542-002 -9.62076+001	
(-8.32037+000) + J(-3.35619+000)		(-1.10471-001) + J(1.01567+000)		4.85542-002 9.62076+001	

SYSTEMS CONTROL, INC. (VI) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

83/04/1.2 OPTIMAL CONTROL DESIGN POINT HPGU

SENSITIVITY TO 4 1 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -5.60451+003

.....POLE LOCATION.....SENSITIVITY.....MAGNITUDE.....PHASE.....
REAL	IMAGINARY		
(-2.85272+002) + J(0.00000)		6.40483-001	1.80000+002
(-1.22537+001) + J(4.12893+000)		4.38009-001	-7.8799+001
(-1.22537+001) + J(-4.12893+000)		4.38009-001	7.8799+001
(-8.32037+000) + J(3.35619+000)		3.12290-001	3.68556+001
(-8.32037+000) + J(-3.35619+000)		3.12290-001	-3.68556+001

SENSITIVITY TO 4 2 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -3.99927+003

.....POLE LOCATION.....SENSITIVITY.....MAGNITUDE.....PHASE.....
REAL	IMAGINARY		
(-2.85272+002) + J(0.00000)		1.93482-001	1.80000+002
(-1.22537+001) + J(4.12893+000)		2.25750-002	3.78927+001
(-1.22537+001) + J(-4.12893+000)		2.25750-002	-3.78927+001
(-8.32037+000) + J(3.35619+000)		1.88259-001	1.25769+002
(-8.32037+000) + J(-3.35619+000)		1.88259-001	-1.25769+002

SENSITIVITY TO 4 3 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 1.83162+001

.....POLE LOCATION.....SENSITIVITY.....MAGNITUDE.....PHASE.....
REAL	IMAGINARY		
(-2.85272+002) + J(0.00000)		5.12209-002	1.80000+002
(-1.22537+001) + J(4.12893+000)		9.87842-002	-9.73386+001
(-1.22537+001) + J(-4.12893+000)		9.87842-002	9.73386+001
(-8.32037+000) + J(3.35619+000)		6.04069-002	-1.24772+002
(-8.32037+000) + J(-3.35619+000)		6.04069-002	1.24772+002

83/0K/1.2 OPTIMAL CONTROL DESIGN POINT WPS4
SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

SENSITIVITY TO 4 4 ELEMENT OF C		MATRIX:		BASELINE PARAMETER VALUE = -7.95231-004	
.....POLE LOCATION.....			SENSITIVITY.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.85272+002) + J(0.00000)		(-6.32062+001) + J(0.00000)		5.02635-002	1.80000+002
(-1.22357+001) + J(4.12893+000)		(1.23578+002) + J(9.46417+001)		1.27603-001	3.61438+001
(-1.22357+001) + J(-4.12893+000)		(1.23578+002) + J(-9.46417+001)		1.27603-001	-3.61438+001
(-8.32037+000) + J(3.35619+000)		(-9.73749+001) + J(-1.99586+002)		1.76809-001	-1.16146+002
(-8.32037+000) + J(-3.35619+000)		(-9.73749+001) + J(1.99586+002)		1.76809-001	1.16146+002

SENSITIVITY TO 4 5 ELEMENT OF C		MATRIX:		BASELINE PARAMETER VALUE = -1.03356-001	
.....POLE LOCATION.....			SENSITIVITY.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.85272+002) + J(0.00000)		(1.82677+002) + J(0.00000)		1.88808+001	1.11022-016
(-1.22357+001) + J(4.12893+000)		(8.26560-001) + J(-1.26651-001)		8.64271-002	-9.71152+000
(-1.22357+001) + J(-4.12893+000)		(8.26560-001) + J(1.26651-001)		8.64271-002	9.71152+000
(-8.32037+000) + J(3.35619+000)		(-6.15307-001) + J(6.83534-001)		9.35366-002	1.32836+002
(-8.32037+000) + J(-3.35619+000)		(-6.15307-001) + J(-6.83534-001)		9.35366-002	-1.32836+002

SENSITIVITY TO 5 1 ELEMENT OF C		MATRIX:		BASELINE PARAMETER VALUE = 2.28857-005	
.....POLE LOCATION.....			SENSITIVITY.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.85272+002) + J(0.00000)		(7.13749+004) + J(0.00000)		1.63346+000	1.11022-016
(-1.22357+001) + J(4.12893+000)		(-2.42429+004) + J(1.43645+004)		6.44896-001	1.40352+002
(-1.22357+001) + J(-4.12893+000)		(-2.42429+004) + J(-1.43645+004)		6.44896-001	-1.40352+002
(-8.32037+000) + J(3.35619+000)		(8.85539+003) + J(9.63415+003)		2.99630-001	4.71796+001
(-8.32037+000) + J(-3.35619+000)		(8.85539+003) + J(-9.63415+003)		2.99630-001	-4.71796+001

83/04/1,2 OPTIMAL CONTROL DESIGN POINT WPGU

SENSITIVITY TO	5	2	ELEMENT OF C	MATRIX	BASELINE PARAMETER VALUE =	3.86320+005
.....POLE LOCATION.....
.....REAL
.....IMAGINARY
.....SENSITIVITY.....
.....MAGNITUDE
.....PHASE
(-2.85272+002) + J(0.00000)	(3.02159+004) + J(0.00000)	1.16733+000	1.16733+000	1.16733+000	1.16733+000	1.16733+000
(-1.22957+001) + J(4.12893+000)	(-1.37559+002) + J(-2.03064+003)	7.86275+002	7.86275+002	7.86275+002	7.86275+002	7.86275+002
(-1.22957+001) + J(4.12893+000)	(-1.37559+002) + J(2.03064+003)	7.86275+002	7.86275+002	7.86275+002	7.86275+002	7.86275+002
(-6.32037+000) + J(3.35619+000)	(-7.99541+003) + J(7.64259+003)	4.27291+001	4.27291+001	4.27291+001	4.27291+001	4.27291+001
(-8.32037+000) + J(-3.35619+000)	(-7.99541+003) + J(-7.64259+003)	4.27291+001	4.27291+001	4.27291+001	4.27291+001	4.27291+001
SENSITIVITY TO 5 3 ELEMENT OF C	SENSITIVITY TO 5 3 ELEMENT OF C	SENSITIVITY TO 5 3 ELEMENT OF C	SENSITIVITY TO 5 3 ELEMENT OF C	SENSITIVITY TO 5 3 ELEMENT OF C	SENSITIVITY TO 5 3 ELEMENT OF C	SENSITIVITY TO 5 3 ELEMENT OF C
.....POLE LOCATION.....
.....REAL
.....IMAGINARY
.....SENSITIVITY.....
.....MAGNITUDE
.....PHASE
(-2.85272+002) + J(0.00000)	(1.74638+002) + J(0.00000)	4.40283+002	4.40283+002	4.40283+002	4.40283+002	4.40283+002
(-1.22957+001) + J(4.12893+000)	(-1.27305+002) + J(1.46999+002)	4.90201+002	4.90201+002	4.90201+002	4.90201+002	4.90201+002
(-1.22957+001) + J(4.12893+000)	(-1.27305+002) + J(-1.46999+002)	4.90201+002	4.90201+002	4.90201+002	4.90201+002	4.90201+002
(-6.32037+000) + J(3.35619+000)	(-3.18242+001) + J(7.08547+001)	1.95345+002	1.95345+002	1.95345+002	1.95345+002	1.95345+002
(-8.32037+000) + J(-3.35619+000)	(-3.18242+001) + J(7.08547+001)	1.95345+002	1.95345+002	1.95345+002	1.95345+002	1.95345+002
SENSITIVITY TO 5 4 ELEMENT OF C	SENSITIVITY TO 5 4 ELEMENT OF C	SENSITIVITY TO 5 4 ELEMENT OF C	SENSITIVITY TO 5 4 ELEMENT OF C	SENSITIVITY TO 5 4 ELEMENT OF C	SENSITIVITY TO 5 4 ELEMENT OF C	SENSITIVITY TO 5 4 ELEMENT OF C
.....POLE LOCATION.....
.....REAL
.....IMAGINARY
.....SENSITIVITY.....
.....MAGNITUDE
.....PHASE
(-2.85272+002) + J(0.00000)	(3.24733+004) + J(0.00000)	2.40723+001	2.40723+001	2.40723+001	2.40723+001	2.40723+001
(-1.22957+001) + J(4.12893+000)	(-5.67015+003) + J(-5.75775+004)	3.52803+001	3.52803+001	3.52803+001	3.52803+001	3.52803+001
(-1.22957+001) + J(4.12893+000)	(-5.67015+003) + J(5.75775+004)	3.52803+001	3.52803+001	3.52803+001	3.52803+001	3.52803+001
(-6.32037+000) + J(3.35619+000)	(-1.40680+004) + J(-5.03113+004)	3.18563+001	3.18563+001	3.18563+001	3.18563+001	3.18563+001
(-8.32037+000) + J(-3.35619+000)	(-1.40680+004) + J(5.03113+004)	3.18563+001	3.18563+001	3.18563+001	3.18563+001	3.18563+001

R3/04/1.2 OPTIMAL CONTROL DESIGN POINT HPG4
 SYSTEMS CONTROL, INC. (VT) -
 TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

SENSITIVITY TO	S	ELEMENT OF C	MATRIX	BASELINE PARAMETER VALUE = 6.52071-004
.....POLE LOCATION.....				
REAL				
(-2.85272+002) + J(0.00000)				
(-1.22957+001) + J(4.12893+000)				
(-1.22957+001) + J(-4.12893+000)				
(-8.32037+000) + J(3.35619+000)				
(-8.32037+000) + J(-3.35619+000)				
.....SENSITIVITY.....				
REAL				
(-1.14094+005) + J(0.00000)				
(-2.32580+002) + J(-1.91864+002)				
(-2.32580+002) + J(1.91864+002)				
(-1.70623+002) + J(1.26901+002)				
(-1.70623+002) + J(-1.26901+002)				
MAGNITUDE				
7.43971+001				
1.96603+001				
1.96603+001				
1.38657+001				
1.38657+001				
PHASE				
1.80000+002				
-1.40440+002				
1.40440+002				
1.43360+002				
-1.43360+002				

1 SENSITIVITY OF OPTIMAL CONTROLLER DESIGN 1

SENSITIVITY TO 1 1 ELEMENT OF A MATRIX1 BASELINE PARAMETER VALUE = 4.00000+003

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.85272+002)	J(0.00000)	(-4.13703+000)	J(0.00000)	1.65481+002	1.80000+002
(-1.22557+001)	J(4.12893+000)	(-1.22863+002)	J(3.15541+002)	1.35484+000	1.11269+002
(-1.22557+001)	J(-4.12893+000)	(-1.22863+002)	J(-3.15541+002)	1.35484+000	-1.11269+002
(-8.32037+000)	J(3.35619+000)	(-1.18924+002)	J(-7.38250+000)	4.76613+001	-1.76448+002
(-8.32037+000)	J(-3.35619+000)	(-1.18924+002)	J(7.38250+000)	4.76613+001	1.76448+002

SENSITIVITY TO 2 2 ELEMENT OF A MATRIX1 BASELINE PARAMETER VALUE = 2.00000+003

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.85272+002)	J(0.00000)	(-4.01913+000)	J(0.00000)	8.03826+003	1.80000+002
(-1.22557+001)	J(4.12893+000)	(-1.63073+001)	J(-1.35546+001)	4.24101+002	-1.40267+002
(-1.22557+001)	J(-4.12893+000)	(-1.63073+001)	J(1.35546+001)	4.24101+002	1.40267+002
(-8.32037+000)	J(3.35619+000)	(-6.63878+001)	J(5.00058+001)	1.66228+001	1.43012+002
(-8.32037+000)	J(-3.35619+000)	(-6.63878+001)	J(-5.00058+001)	1.66228+001	-1.43012+002

SENSITIVITY TO 3 3 ELEMENT OF A MATRIX1 BASELINE PARAMETER VALUE = 3.00000+001

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.85272+002)	J(0.00000)	(3.13292+004)	J(0.00000)	9.39876+003	1.11022+016
(-1.22557+001)	J(4.12893+000)	(-3.00927+002)	J(-1.88104+002)	1.06464+000	-1.47991+002
(-1.22557+001)	J(-4.12893+000)	(-3.00927+002)	J(1.88104+002)	1.06464+000	1.47991+002
(-8.32037+000)	J(3.35619+000)	(-2.00528+002)	J(-9.92546+003)	6.71242+001	-1.53666+002
(-8.32037+000)	J(-3.35619+000)	(-2.00528+002)	J(9.92546+003)	6.71242+001	1.53666+002

SENSITIVITY TO 4 4 ELEMENT OF A MATRIX: BASELINE PARAMETER VALUE = 0.00000

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.85272+002)	+ J(0.00000)	(-2.81944+001)	+ J(0.00000)	2.81844+001	1.80000+002
(-1.22957+001)	+ J(4.12893+000)	(-5.89110+003)	+ J(-4.77116+003)	7.57306+003	-1.40949+002
(-1.22957+001)	+ J(-4.12893+000)	(-5.89110+003)	+ J(4.77116+003)	7.57306+003	1.40949+002
(-8.32037+000)	+ J(3.35619+000)	(-2.28416+003)	+ J(-2.96428+003)	3.74224+003	-1.27617+002
(-8.32037+000)	+ J(-3.35619+000)	(-2.28416+003)	+ J(2.96428+003)	3.74224+003	1.27617+002

SENSITIVITY TO 5 5 ELEMENT OF A MATRIX: BASELINE PARAMETER VALUE = 2.00000+000

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.85272+002)	+ J(0.00000)	(-4.36528+001)	+ J(0.00000)	8.73056+001	1.80000+002
(-1.22957+001)	+ J(4.12893+000)	(-1.66902+001)	+ J(-1.51876+001)	4.51321+001	-1.37699+002
(-1.22957+001)	+ J(-4.12893+000)	(-1.66902+001)	+ J(1.51876+001)	4.51321+001	1.37699+002
(-8.32037+000)	+ J(3.35619+000)	(-6.09446+002)	+ J(7.51752+002)	1.93602+001	1.20050+002
(-8.32037+000)	+ J(-3.35619+000)	(-6.09446+002)	+ J(-7.51752+002)	1.93602+001	-1.20050+002

SENSITIVITY TO 1 1 ELEMENT OF B MATRIX: BASELINE PARAMETER VALUE = 2.00000+000

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.85272+002)	+ J(0.00000)	(2.30717+004)	+ J(0.00000)	4.61435+000	1.11022+016
(-1.22957+001)	+ J(4.12893+000)	(5.85272+003)	+ J(-4.34319+003)	1.62263+000	-3.23661+001
(-1.22957+001)	+ J(-4.12893+000)	(5.85272+003)	+ J(4.34319+003)	1.62263+000	3.23661+001
(-8.32037+000)	+ J(3.35619+000)	(6.95447+002)	+ J(-2.52199+003)	5.23224+001	-7.45837+001
(-8.32037+000)	+ J(-3.35619+000)	(6.95447+002)	+ J(2.52199+003)	5.23224+001	7.45837+001

SENSITIVITY TO 2 2 ELEMENT OF A		MATRIX:		BASELINE PARAMETER VALUE = 8.00000+003	
.....REAL.....POLE LOCATION.....IMAGINARY.....			SENSITIVITY.....MAGNITUDE.....PHASE.....	
(-2.42272+002) + J(0.00000)		(1.31453+004) + J(0.00000)		1.00000+000 1.11022-016	
(-1.22957+001) + J(4.12893+000)		(8.33348+005) + J(2.26027+005)		6.90773+001 1.51751+001	
(-1.22957+001) + J(-4.12893+000)		(8.33348+005) + J(-2.26027+005)		6.90773+001 -1.51751+001	
(-8.32037+000) + J(3.35619+000)		(1.17624+004) + J(4.62415+005)		1.01110+000 2.14612+001	
(-8.32037+000) + J(-3.35619+000)		(1.17624+004) + J(-4.62415+005)		1.01110+000 -2.14612+001	
SENSITIVITY TO 3 3 ELEMENT OF B		MATRIX:		BASELINE PARAMETER VALUE = 2.00000+001	
.....REAL.....POLE LOCATION.....IMAGINARY.....			SENSITIVITY.....MAGNITUDE.....PHASE.....	
(-2.42272+002) + J(0.00000)		(4.67314+001) + J(0.00000)		9.34627+000 1.11022-016	
(-1.22957+001) + J(4.12893+000)		(1.87591+003) + J(6.89359+003)		1.42885+001 -7.47772+001	
(-1.22957+001) + J(-4.12893+000)		(1.87591+003) + J(-6.89359+003)		1.42885+001 7.47772+001	
(-8.32037+000) + J(3.35619+000)		(6.51793+003) + J(3.08357+003)		1.44211+001 -2.53184+001	
(-8.32037+000) + J(-3.35619+000)		(6.51793+003) + J(-3.08357+003)		1.44211+001 2.53184+001	
SENSITIVITY TO 4 4 ELEMENT OF B		MATRIX:		BASELINE PARAMETER VALUE = 8.00000+000	
.....REAL.....POLE LOCATION.....IMAGINARY.....			SENSITIVITY.....MAGNITUDE.....PHASE.....	
(-2.42272+002) + J(0.00000)		(1.83018+000) + J(0.00000)		1.46414+001 1.11022-016	
(-1.22957+001) + J(4.12893+000)		(2.23370+003) + J(1.17589+002)		9.57533+002 -7.92044+001	
(-1.22957+001) + J(-4.12893+000)		(2.23370+003) + J(-1.17589+002)		9.57533+002 7.92044+001	
(-8.32037+000) + J(3.35619+000)		(1.04456+003) + J(4.08132+002)		3.26612+001 9.85340+001	
(-8.32037+000) + J(-3.35619+000)		(1.04456+003) + J(-4.08132+002)		3.26612+001 -9.85340+001	

SYSTEMS CONTROL INC.(VT)
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

23/04/1.2 OPTIMAL CONTROL DESIGN POINT HPGW

SENSITIVITY TO 5 5 ELEMENT OF R MATRIX: BASELINE PARAMETER VALUE = 8.00000+005

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-2.95372+002)	+ J(0.00000)	(7.20948-005)	+ J(0.00000)	5.76758+001	1.11022-016
(-1.22357+001)	+ J(4.12893+000)	(-4.14730-007)	+ J(6.90411-007)	6.44319-001	1.20993+002
(-1.22357+001)	+ J(-4.12893+000)	(-4.14730-007)	+ J(-6.90411-007)	6.44319-001	1.20993+002
(-5.32037+000)	+ J(3.35519+000)	(1.41700-007)	+ J(-6.67846-008)	1.25320-001	2.52349+001
(-5.32037+000)	+ J(-3.35519+000)	(1.41700-007)	+ J(6.67846-008)	1.25320-001	2.52349+001

1 SENSITIVITY OF CLOSED LOOP SYSTEM 1

SENSITIVITY TO 1 1 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -1.03002+000

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.43512+002) + J(0.00000)	(6.41513-001) + J(0.00000)		6.41590-001	1.11022-016
(-1.03770+001) + J(2.15777-000)	(-3.85769-001) + J(-8.38139+000)		9.24355+001	-9.24355+001
(-1.03770+001) + J(-2.15777-000)	(-3.85769-001) + J(8.38139+000)		8.41482+000	9.24355+001
(-2.42732+000) + J(0.00000)	(7.50133-001) + J(0.00000)		7.73200-001	1.11022-016
(-2.22719-001) + J(0.00000)	(-9.46750-003) + J(0.00000)		9.75909-003	1.80000+002

SENSITIVITY TO 1 2 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -1.23813+000

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.43512+002) + J(0.00000)	(3.54893-001) + J(0.00000)		4.39035-001	1.11022-016
(-1.03770+001) + J(2.15777-000)	(1.90351+000) + J(-6.17767+000)		8.00401+000	-7.28705+001
(-1.03770+001) + J(-2.15777-000)	(1.90351+000) + J(6.17767+000)		8.00401+000	7.28705+001
(-2.42732+000) + J(0.00000)	(-7.48305-001) + J(0.00000)		9.26508-001	1.80000+002
(-2.22719-001) + J(0.00000)	(-2.60345-003) + J(0.00000)		3.22875-003	1.80000+002

SENSITIVITY TO 1 3 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 1.12875+002

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.43512+002) + J(0.00000)	(-2.43865-004) + J(0.00000)		2.97901-002	1.80000+002
(-1.03770+001) + J(2.15777-000)	(-2.03892-002) + J(-1.00424-001)		1.15646+001	-1.01422+002
(-1.03770+001) + J(-2.15777-000)	(-2.03892-002) + J(1.00424-001)		1.15646+001	1.01422+002
(-2.42732+000) + J(0.00000)	(2.89560-004) + J(0.00000)		3.26954-002	1.11022-016
(-2.22719-001) + J(0.00000)	(5.26757-005) + J(0.00000)		5.94550-005	1.11022-016

SYSTEMS CONTROL INC.(VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

20/04/77 NATURAL CONTROL DESIGN POINT LOGS

SENSITIVITY TO 1 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -2.60470+001

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.93512+002) + J(0.00000)	(5.41008-001)	J(0.00000)	1.51335+001	1.11022-016	
(-1.04774+001) + J(2.15757+000)	(4.65334+000)	J(2.06689+001)	5.51834+000	7.73149+001	
(-1.04774+001) + J(2.15757+000)	(4.65334+000)	J(2.06689+001)	5.51834+000	-7.73149+001	
(-2.22719+001) + J(0.00000)	(9.80305-002)	J(0.00000)	2.55340+002	1.11022-016	
(-2.22719+001) + J(0.00000)	(1.62229-002)	J(0.00000)	4.24122+003	1.11022-016	

SENSITIVITY TO 1 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 9.82335+000

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.93512+002) + J(0.00000)	(-6.59147-001)	J(0.00000)	6.47504+000	1.80000+002	
(-1.04774+001) + J(2.15757+000)	(7.93000-002)	J(4.55659-002)	8.98430+001	2.98623+001	
(-1.04774+001) + J(2.15757+000)	(7.93000-002)	J(4.55659-002)	8.98430+001	-2.98623+001	
(-2.22719+001) + J(0.00000)	(-9.77355-003)	J(0.00000)	8.62251+002	1.80000+002	
(-2.22719+001) + J(0.00000)	(1.21995-004)	J(0.00000)	1.22680+003	0.00000	

SENSITIVITY TO 2 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 5.91753+006

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.93512+002) + J(0.00000)	(-4.47371+000)	J(0.00000)	2.65423+005	1.80000+002	
(-1.04774+001) + J(2.15757+000)	(-2.87284+002)	J(1.54573+003)	9.33555+003	1.00547+002	
(-1.04774+001) + J(2.15757+000)	(-2.87284+002)	J(1.54573+003)	9.33555+003	1.00547+002	
(-2.22719+001) + J(0.00000)	(2.08150+002)	J(0.00000)	1.23589+003	1.11022-016	
(-2.22719+001) + J(0.00000)	(5.35000+001)	J(0.00000)	3.17653+004	1.11022-016	

SYSTEMS CONTROL INC.(VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

20/05/00 OPTIMAL CONTROL DESIGN POINT LOGS

SENSITIVITY TO 2 ELEMENT OF C	MATRIX:	BASLINE PARAMETER VALUE = 1.60979+004
.....POLE LOCATION.....		
REAL	IMAGINARY	SENSITIVITY
.....	MAGNITUDE
.....	PHASE
(-1.0512+002) + J(0.0000)	(-2.47374+000) + J(0.00000)	3.92223-004
(-1.0512+002) + J(2.1527+000)	(-5.11312+002) + J(1.04581+003)	1.80000+002
(-1.0512+002) + J(2.1527+000)	(-5.11312+002) + J(1.04581+003)	1.20308+002
(-1.0512+002) + J(0.0000)	(-2.07643+002) + J(0.00000)	1.95005-001
(-1.0512+002) + J(0.0000)	(-2.07643+002) + J(0.00000)	3.34262-002
(-1.0512+002) + J(0.0000)	(-1.07400+001) + J(0.00000)	1.80000+002
(-1.0512+002) + J(0.0000)	(-1.07400+001) + J(0.00000)	1.11022-016
SENSITIVITY TO 3 ELEMENT OF C	MATRIX:	BASLINE PARAMETER VALUE = 2.62495-002
.....POLE LOCATION.....		
REAL	IMAGINARY	SENSITIVITY
.....	MAGNITUDE
.....	PHASE
(-1.0512+002) + J(0.0000)	(-1.83939+003) + J(0.00000)	4.82830-005
(-1.0512+002) + J(2.1527+000)	(-5.09771+001) + J(1.91905+001)	5.03978-001
(-1.0512+002) + J(2.1527+000)	(-5.09771+001) + J(1.91905+001)	5.03978-001
(-1.0512+002) + J(0.0000)	(-5.03754+002) + J(0.00000)	2.10822-003
(-1.0512+002) + J(0.0000)	(-2.07672+001) + J(0.00000)	7.81374+003
(-1.0512+002) + J(0.0000)	(-2.07672+001) + J(0.00000)	1.11022-016
(-1.0512+002) + J(0.0000)	(-2.07672+001) + J(0.00000)	1.80000+002
SENSITIVITY TO 4 ELEMENT OF C	MATRIX:	BASLINE PARAMETER VALUE = 1.83800-004
.....POLE LOCATION.....		
REAL	IMAGINARY	SENSITIVITY
.....	MAGNITUDE
.....	PHASE
(-1.0512+002) + J(0.0000)	(-4.04097+000) + J(0.00000)	7.44366-004
(-1.0512+002) + J(2.1527+000)	(-3.04314+001) + J(3.97002+003)	7.29716-001
(-1.0512+002) + J(2.1527+000)	(-3.04314+001) + J(3.97002+003)	7.29716-001
(-1.0512+002) + J(0.0000)	(-2.12018+001) + J(0.00000)	4.99759-003
(-1.0512+002) + J(0.0000)	(-2.12018+001) + J(0.00000)	1.69124+002
(-1.0512+002) + J(0.0000)	(-2.12018+001) + J(0.00000)	1.80000+002

27/3/70, 2 OPTICAL CONTROL DESIGN POINT LOG1 SYSTEMS CONTROL INC.(VT) - TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

SENSITIVITY TO 2 5 ELEMENT OF C		MATRIX		BASELINE PARAMETER VALUE = 9.43117-004	
.....REAL	POLE LOCATION.....	SENSITIVITY.....	
	REAL	IMAGINARY	
			MAGNITUDE	
			PHASE	
(-1.45312+002)	+ J(0.00000)	(-1.45312+002)	+ J(0.00000)	4.33319-003	1.11022-016
(-1.04773+001)	+ J(2.15357+000)	(-1.04773+001)	+ J(2.15357+000)	1.61641-002	-1.34936+002
(-1.04773+001)	+ J(2.15357+000)	(-1.04773+001)	+ J(2.15357+000)	1.61641-002	1.34936+002
(-2.42271+000)	+ J(0.00000)	(-2.42271+000)	+ J(0.00000)	2.29708-003	1.80000+002
(-2.42271+000)	+ J(0.00000)	(-2.42271+000)	+ J(0.00000)	6.63637-004	1.80000+002
SENSITIVITY TO 3 1 ELEMENT OF C		MATRIX		BASELINE PARAMETER VALUE = -2.97371-003	
.....REAL	POLE LOCATION.....	SENSITIVITY.....	
	REAL	IMAGINARY	
			MAGNITUDE	
			PHASE	
(-1.03512+002)	+ J(0.00000)	(-1.03512+002)	+ J(0.00000)	1.62191-002	1.80000+002
(-1.03512+002)	+ J(2.15357+000)	(-1.03512+002)	+ J(2.15357+000)	2.36397-002	-5.63988+001
(-1.03512+002)	+ J(2.15357+000)	(-1.03512+002)	+ J(2.15357+000)	2.36397-002	5.63988+001
(-2.42271+000)	+ J(0.00000)	(-2.42271+000)	+ J(0.00000)	2.90002-003	1.11022-016
(-2.42271+000)	+ J(0.00000)	(-2.42271+000)	+ J(0.00000)	6.21591-004	1.80000+002
SENSITIVITY TO 3 2 ELEMENT OF C		MATRIX		BASELINE PARAMETER VALUE = -9.46540-003	
.....REAL	POLE LOCATION.....	SENSITIVITY.....	
	REAL	IMAGINARY	
			MAGNITUDE	
			PHASE	
(-1.03512+002)	+ J(0.00000)	(-1.03512+002)	+ J(0.00000)	2.85468-002	1.80000+002
(-1.03512+002)	+ J(2.15357+000)	(-1.03512+002)	+ J(2.15357+000)	5.81203-002	-5.63378+001
(-1.03512+002)	+ J(2.15357+000)	(-1.03512+002)	+ J(2.15357+000)	5.81203-002	5.63378+001
(-2.42271+000)	+ J(0.00000)	(-2.42271+000)	+ J(0.00000)	9.20840-003	1.80000+002
(-2.42271+000)	+ J(0.00000)	(-2.42271+000)	+ J(0.00000)	5.45104-004	1.80000+002

SYSTEMS CONTROL INC.(VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

20/3/64 4.4 OPTIMAL CONTROL DESIGN POINT LOG1

SENSITIVITY TO 3 3 ELEMENT OF C				BASELINE PARAMETER VALUE = -5.34169-001				
POLE LOCATION				SENSITIVITY				
REAL				MAGNITUDE				
IMAGINARY				PHASE				
(-1.43512+002)	+	J(0.00000)		(2.24951-003)	+	J(0.00000)	1.1978-003	1.11022-016
(-1.07774+001)	+	J(2.15787+000)		(-4.52403-003)	+	J(-9.46936-002)	5.19852-002	-9.50852+001
(-1.07774+001)	+	J(-2.15787+000)		(-8.42403-003)	+	J(9.46936-002)	5.19852-002	9.50852+001
(-2.42752+000)	+	J(0.00000)		(3.76576-004)	+	J(0.00000)	2.01155-004	1.11022-016
(-2.22712-001)	+	J(0.00000)		(1.15297-003)	+	J(0.00000)	5.21224-004	1.11022-016
SENSITIVITY TO 3 4 ELEMENT OF C				BASELINE PARAMETER VALUE = -7.51705-003				
POLE LOCATION				SENSITIVITY				
REAL				MAGNITUDE				
IMAGINARY				PHASE				
(-1.43512+002)	+	J(0.00000)		(-4.93744+000)	+	J(0.00000)	3.71150-002	1.80000+002
(-1.07774+001)	+	J(2.15787+000)		(2.23225+000)	+	J(2.00000+001)	1.51275-001	8.34516+001
(-1.07774+001)	+	J(-2.15787+000)		(2.23225+000)	+	J(-2.00000+001)	1.51275-001	-8.34516+001
(-2.42752+000)	+	J(0.00000)		(1.27446-001)	+	J(0.00000)	9.58016-004	0.00000
(-2.22712-001)	+	J(0.00000)		(3.59493-001)	+	J(0.00000)	2.70233-003	1.11022-016
SENSITIVITY TO 3 5 ELEMENT OF C				BASELINE PARAMETER VALUE = -4.54540-001				
POLE LOCATION				SENSITIVITY				
REAL				MAGNITUDE				
IMAGINARY				PHASE				
(-1.43512+002)	+	J(0.00000)		(5.60148+000)	+	J(0.00000)	2.54609+000	1.11022-016
(-1.07774+001)	+	J(2.15787+000)		(7.00981-002)	+	J(5.13324-002)	3.94883-002	3.62190+001
(-1.07774+001)	+	J(-2.15787+000)		(7.00981-002)	+	J(-5.13324-002)	3.94883-002	-3.62190+001
(-2.42752+000)	+	J(0.00000)		(-1.14114-002)	+	J(0.00000)	5.18482-003	1.80000+002
(-2.22712-001)	+	J(0.00000)		(2.75742-003)	+	J(0.00000)	1.25336-003	1.11022-016

SYSTEMS CONTROL, INC. (CVT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

20/8/70 OPTIMAL CONTROL DESIGN POINT LPS1

SENSITIVITY TO 4 1 ELEMENT OF C MATRIX BASELINE PARAMETER VALUE = -4.09419-001

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.05512+002)	+ JC (0.00000)		1.16401-001	1.80000+002
(-1.04772+001)	+ JC (2.1577+000)		1.25662-001	-9.83175+001
(-1.04772+001)	+ JC (2.1577+000)		1.25662-001	8.83175+001
(-2.02772+000)	+ JC (0.00000)		9.33412-002	1.11022-016
(-2.02771+001)	+ JC (0.00000)		5.46991-005	1.80000+002

SENSITIVITY TO 4 2 ELEMENT OF C MATRIX BASELINE PARAMETER VALUE = -3.42149-001

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.05512+002)	+ JC (0.00000)		5.37893-002	1.80000+002
(-1.04772+001)	+ JC (2.1577+000)		8.15326-002	-9.85585+001
(-1.04772+001)	+ JC (2.1577+000)		8.15326-002	9.85585+001
(-2.02772+000)	+ JC (0.00000)		7.79151-002	1.80000+002
(-2.02771+001)	+ JC (0.00000)		1.25646-005	1.80000+002

SENSITIVITY TO 4 3 ELEMENT OF C MATRIX BASELINE PARAMETER VALUE = 2.57161-001

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.05512+002)	+ JC (0.00000)		3.00608-003	1.11022-016
(-1.04772+001)	+ JC (2.1577+000)		9.71091-002	-9.71039+001
(-1.04772+001)	+ JC (2.1577+000)		9.71091-002	9.71039+001
(-2.02772+000)	+ JC (0.00000)		2.26391-003	1.11022-016
(-2.02771+001)	+ JC (0.00000)		1.91152-005	0.00000

LOG1

SENSITIVITY TO 4 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -1.51545-003

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.03512+002)	+ JC (0.00000)		3.90038-002	1.80000+002
(-1.03770+001)	+ JC (2.15757+000)		1.18364-001	8.13322+001
(-1.03770+001)	+ JC (-2.15757+000)		1.18364-001	8.13322+001
(-2.03732+000)	+ JC (0.00000)		4.31114-003	1.11022-016
(-2.03714+001)	+ JC (0.00000)		3.42226-005	0.00000

SENSITIVITY TO 5 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -2.30965-001

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.03512+002)	+ JC (0.00000)		6.74390+000	1.11022-016
(-1.03770+001)	+ JC (2.15757+000)		7.78991-002	3.42003+001
(-1.03770+001)	+ JC (-2.15757+000)		7.78991-002	3.42003+001
(-2.03732+000)	+ JC (0.00000)		6.16151-002	1.80000+002
(-2.03714+001)	+ JC (0.00000)		4.07077-005	0.00000

SENSITIVITY TO 5 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 1.03685-005

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.03512+002)	+ JC (0.00000)		6.91786-002	2.20005-016
(-1.03770+001)	+ JC (2.15757+000)		1.36230-001	5.46499+001
(-1.03770+001)	+ JC (-2.15757+000)		1.36230-001	-9.00000+001
(-2.03732+000)	+ JC (0.00000)		2.30132-003	1.80000+002
(-2.03714+001)	+ JC (0.00000)		4.08891-004	1.80000+002

207300000 DETAIL CONTROL DESIGN POINT LOG1
SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

SENSITIVITY TO S 2 ELEMENT OF C

WATRIX: BASELINE PARAMETER VALUE = 2.74863-005

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.4512+002) + JC 0.0000	1.4512	0.0000	1.01405-001	1.11022-016	
(-1.0477+001) + JC 2.1527+000	1.0477	2.1527	2.83331-001	1.14631-002	
(-1.0477+001) + JC 2.1527+000	1.0477	2.1527	2.83331-001	-1.14631-002	
(-2.2271+001) + JC 0.0000	2.2271	0.0000	6.05881-003	1.11022-016	
(-2.2271+001) + JC 0.0000	2.2271	0.0000	2.98614-004	1.60000-002	

SENSITIVITY TO S 3 ELEMENT OF C

WATRIX: BASELINE PARAMETER VALUE = -6.16318-005

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.4512+002) + JC 0.0000	1.4512	0.0000	2.23934-004	1.80000-002	
(-1.0477+001) + JC 2.1527+000	1.0477	2.1527	1.38896-002	8.60835-001	
(-1.0477+001) + JC 2.1527+000	1.0477	2.1527	1.38896-002	-8.60835-001	
(-2.2271+001) + JC 0.0000	2.2271	0.0000	6.99430-006	1.50000-002	
(-2.2271+001) + JC 0.0000	2.2271	0.0000	1.79094-005	0.00000	

SENSITIVITY TO S 4 ELEMENT OF C

WATRIX: BASELINE PARAMETER VALUE = 1.44088-005

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.4512+002) + JC 0.0000	1.4512	0.0000	8.70274-002	1.11022-016	
(-1.0477+001) + JC 2.1527+000	1.0477	2.1527	4.85064-001	-9.51800-001	
(-1.0477+001) + JC 2.1527+000	1.0477	2.1527	4.85064-001	9.51800-001	
(-2.2271+001) + JC 0.0000	2.2271	0.0000	4.17936-004	1.80000-002	
(-2.2271+001) + JC 0.0000	2.2271	0.0000	9.77171-004	1.11022-016	

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

20/3/67 OPTIMAL CONTROL DESIGN POINT LPS1

SENSITIVITY TO S ELEMENT OF C MATRIX BASELINE PARAMETER VALUE = 1.13249-003

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-1.03512+002)	+ JC 0.00000)	(-0.45212+003)	+ JC 0.00000)	7.76002+000	1.80000+002
(-1.04770+001)	+ JC 2.15257+000)	(-1.15470+002)	+ JC (-8.82437+001)	1.64583-001	-1.42613+002
(-1.04770+001)	+ JC -2.15257+000)	(-1.15470+002)	+ JC 8.82437+001)	1.64583-001	1.42613+002
(-2.82752+000)	+ JC 0.00000)	(2.82714+000)	+ JC 0.00000)	2.94123-003	0.00000
(-2.82717+001)	+ JC 0.00000)	(5.20152-001)	+ JC 0.00000)	5.89101-004	1.11022-016

 1 SENSITIVITY OF OPTIMAL CONTROLLER DESIGN

SENSITIVITY TO 1 1 ELEMENT OF A MATRIX BASELINE PARAMETER VALUE = 2.00000-004

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.43512+002) + J(0.00000)	(-2.15258+001) + J(0.00000)	4.30516-003	1.80000+002		
(-1.04774+001) + J(2.15787+000)	(-1.56929+003) + J(9.17236+003)	1.86113+000	9.97087+001		
(-1.04774+001) + J(2.15787+000)	(-1.56929+003) + J(9.17236+003)	1.86113+000	-9.97087+001		
(-2.42732+000) + J(0.00000)	(-2.61703+003) + J(0.00000)	5.23405-001	1.80000+002		
(-2.22719+001) + J(0.00000)	(2.30490+001) + J(0.00000)	4.60979-003	2.22045-016		

SENSITIVITY TO 2 2 ELEMENT OF A MATRIX BASELINE PARAMETER VALUE = 1.00000-005

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.43512+002) + J(0.00000)	(-7.25508+001) + J(0.00000)	7.25506-004	1.80000+002		
(-1.04774+001) + J(2.15787+000)	(-5.13993+003) + J(1.14225+004)	1.25256-001	1.14227+002		
(-1.04774+001) + J(2.15787+000)	(-5.13993+003) + J(1.14225+004)	1.25256-001	-1.14227+002		
(-2.42732+000) + J(0.00000)	(1.85808+003) + J(0.00000)	1.85808-002	1.11022-016		
(-2.22719+001) + J(0.00000)	(2.10896+001) + J(0.00000)	2.10896-004	1.11022-016		

SENSITIVITY TO 3 3 ELEMENT OF A MATRIX BASELINE PARAMETER VALUE = 2.00000-002

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.43512+002) + J(0.00000)	(-6.11528+004) + J(0.00000)	1.22306-005	1.80000+002		
(-1.04774+001) + J(2.15787+000)	(-2.03429+001) + J(-8.98355-001)	1.84220-002	-1.02759+002		
(-1.04774+001) + J(2.15787+000)	(-2.03429+001) + J(8.98355-001)	1.84220-002	1.02759+002		
(-2.42732+000) + J(0.00000)	(1.44922+003) + J(0.00000)	2.89844-005	1.11022-016		
(-2.22719+001) + J(0.00000)	(-2.35850+003) + J(0.00000)	4.71701-005	1.80000+002		

20/10/0.9 OPTIMAL CONTROL DESIGN POINT LPS1
SYSTEMS CONTROL INC.(VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

SENSITIVITY TO 4 4 ELEMENT OF A MATRIX: BASELINE PARAMETER VALUE = 0.0000

.....POLE LOCATION.....SENSITIVITY.....MAGNITUDE.....PHASE.....
REAL	IMAGINARY		
(-1.03512+002) + J(0.00000)	(-3.36258+002) + J(0.00000)	3.36258+002	1.80000+002
(-1.04774+001) + J(2.15787+000)	(-1.08712+004) + J(5.17638+004)	5.28930+004	1.01861+002
(-1.04774+001) + J(-2.15787+000)	(-1.08712+004) + J(5.17638+004)	5.28930+004	1.01861+002
(-2.42732+000) + J(0.00000)	(-2.17663+002) + J(0.00000)	2.17663+002	1.80000+002
(-2.22719+001) + J(0.00000)	(-5.54770+001) + J(0.00000)	5.54770+001	1.80000+002

SENSITIVITY TO 5 5 ELEMENT OF A MATRIX: BASELINE PARAMETER VALUE = 8.00000+001

.....POLE LOCATION.....SENSITIVITY.....MAGNITUDE.....PHASE.....
REAL	IMAGINARY		
(-1.03512+002) + J(0.00000)	(-2.78765+001) + J(0.00000)	2.23012+001	1.80000+002
(-1.04774+001) + J(2.15787+000)	(-1.99060+000) + J(-1.80519+000)	2.14978+000	-1.37797+002
(-1.04774+001) + J(-2.15787+000)	(-1.99060+000) + J(1.80519+000)	2.14978+000	1.37797+002
(-2.42732+000) + J(0.00000)	(5.12096+001) + J(0.00000)	4.09677+001	1.11022+016
(-2.22719+001) + J(0.00000)	(-2.33560+002) + J(0.00000)	1.86844+002	1.80000+002

SENSITIVITY TO 1 1 ELEMENT OF B MATRIX: BASELINE PARAMETER VALUE = 1.00000+004

.....POLE LOCATION.....SENSITIVITY.....MAGNITUDE.....PHASE.....
REAL	IMAGINARY		
(-1.03512+002) + J(0.00000)	(6.49258+004) + J(0.00000)	6.49258+000	1.11022+016
(-1.04774+001) + J(2.15787+000)	(2.39454+004) + J(-2.26577+003)	2.40722+000	-5.40089+000
(-1.04774+001) + J(-2.15787+000)	(2.39454+004) + J(2.26577+003)	2.40722+000	5.40089+000
(-2.42732+000) + J(0.00000)	(-2.04859+002) + J(0.00000)	2.04859+002	1.80000+002
(-2.22719+001) + J(0.00000)	(-5.54550+001) + J(0.00000)	5.54550+003	1.80000+002

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

20/30<0.9 OPTIMAL CONTROL DESIGN POINT LPG1

SENSITIVITY TO 2 2 ELEMENT OF B MATRIX: BASELINE PARAMETER VALUE = 2.00000+002

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-1.43512+002)	+ J(0.00000)	(1.80356-006)	+ J(0.00000)	3.60711-004	0.00000
(-1.04774+001)	+ J(2.15787+000)	(2.17815-004)	+ J(1.65172-004)	5.46718-002	3.71735+001
(-1.04774+001)	+ J(-2.15787+000)	(2.17815-004)	+ J(-1.65172-004)	5.46718-002	-3.71735+001
(-2.42732+000)	+ J(0.00000)	(2.11128-004)	+ J(0.00000)	4.22257-002	2.2045-016
(-2.22719-001)	+ J(0.00000)	(1.00284-004)	+ J(0.00000)	2.00568-002	2.22045-016

SENSITIVITY TO 3 3 ELEMENT OF B MATRIX: BASELINE PARAMETER VALUE = 4.00000+002

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-1.43512+002)	+ J(0.00000)	(5.75574+001)	+ J(0.00000)	2.30230+000	1.11022-016
(-1.04774+001)	+ J(2.15787+000)	(-1.77354+000)	+ J(-1.24564+000)	8.66908-002	-1.44918+002
(-1.04774+001)	+ J(-2.15787+000)	(-1.77354+000)	+ J(1.24564+000)	8.66908-002	1.44918+002
(-2.42732+000)	+ J(0.00000)	(3.33257-001)	+ J(0.00000)	1.33303-002	1.11022-016
(-2.22719-001)	+ J(0.00000)	(5.15421-002)	+ J(0.00000)	2.06169-003	1.11022-016

SENSITIVITY TO 4 4 ELEMENT OF B MATRIX: BASELINE PARAMETER VALUE = 4.00000+001

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-1.43512+002)	+ J(0.00000)	(1.52311+001)	+ J(0.00000)	6.09242+000	1.11022-016
(-1.04774+001)	+ J(2.15787+000)	(-4.85613-001)	+ J(-2.68192-001)	2.21900-001	-1.51089+002
(-1.04774+001)	+ J(-2.15787+000)	(-4.85613-001)	+ J(2.68192-001)	2.21900-001	1.51089+002
(-2.42732+000)	+ J(0.00000)	(-5.05978-002)	+ J(0.00000)	2.02391-002	1.80000+002
(-2.22719-001)	+ J(0.00000)	(5.46994-004)	+ J(0.00000)	2.18798-004	1.11022-016

20/30/0.9 OPTIMAL CONTROL DESIGN POINT LPG1

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

SENSITIVITY TO S S ELEMENT OF R MATRIX BASELINE PARAMETER VALUE = 2.00000+000

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-1.43512+002)	+ J(0.00000)	(3.51041-004)	+ J(0.00000)	7.02081+000	1.11022-016
(-1.04774+001)	+ J(2.15787+000)	(-1.06458-005)	+ J(-6.79910-006)	2.52635-001	-1.47435+002
(-1.04774+001)	+ J(-2.15787+000)	(-1.06458-005)	+ J(6.79910-006)	2.52635-001	1.47435+002
(-2.42732+000)	+ J(0.00000)	(4.01487-006)	+ J(0.00000)	8.02974-002	1.11022-016
(-2.22713+001)	+ J(0.00000)	(-1.43957-007)	+ J(0.00000)	2.87914-003	1.80000+002

1 SENSITIVITY OF CLOSED LOOP SYSTEM 1

SENSITIVITY TO 1 1 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -2.75676+002

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.51351+002) + J(0.00000)	(2.49130+000) + J(0.00000)		6.86793+002	1.11022-016	
(-9.55230+000) + J(0.00000)	(6.62185+001) + J(0.00000)		1.82509+002	1.11022-016	
(-5.74539+000) + J(6.24817+001)	(-5.00204+000) + J(-8.36185+001)		2.30928+000	-9.34234+001	
(-5.74539+000) + J(-6.24817+001)	(-5.00204+000) + J(8.36185+001)		2.30928+000	9.34234+001	
(-1.94493+000) + J(0.00000)	(-4.00414+001) + J(0.00000)		1.10385+002	1.80000+002	

SENSITIVITY TO 1 2 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -6.73882+001

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.51351+002) + J(0.00000)	(3.23809+000) + J(0.00000)		2.18209+000	1.11022-016	
(-9.55230+000) + J(0.00000)	(-4.57027+000) + J(0.00000)		3.07983+000	1.80000+002	
(-5.74539+000) + J(6.24817+001)	(1.85319+000) + J(1.26347+001)		8.60538+000	9.14557+001	
(-5.74539+000) + J(-6.24817+001)	(1.85319+000) + J(-1.26347+001)		8.60538+000	-9.14557+001	
(-1.94493+000) + J(0.00000)	(2.00180+000) + J(0.00000)		1.34898+000	1.11022-016	

SENSITIVITY TO 1 3 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -1.12896+001

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.51351+002) + J(0.00000)	(2.06140+002) + J(0.00000)		2.32723+001	1.11022-016	
(-9.55230+000) + J(0.00000)	(3.05326+002) + J(0.00000)		3.44700+001	1.11022-016	
(-5.74539+000) + J(6.24817+001)	(-1.51940+002) + J(-8.30594+002)		9.53266+001	-1.00367+002	
(-5.74539+000) + J(-6.24817+001)	(-1.51940+002) + J(8.30594+002)		9.53266+001	1.00367+002	
(-1.94493+000) + J(0.00000)	(-3.89563+004) + J(0.00000)		4.38694+003	1.80000+002	

SENSITIVITY TO 1 4 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -1.23198-001

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.51351+002) + J(0.00000)	(3.20918+001) + J(0.00000)	3.95364+002	1.11022-016	
(-9.53230+000) + J(0.00000)	(1.62300+001) + J(0.00000)	1.99950+000	1.11022-016	
(-5.74539+000) + J(6.24817-001)	(-2.56840+000) + J(-8.76002+000)	1.12464+000	-1.06341+002	
(-5.74539+000) + J(-6.24817-001)	(-2.56840+000) + J(8.76002+000)	1.12464+000	1.06341+002	
(-1.24493+000) + J(0.00000)	(-1.41414+000) + J(0.00000)	1.74218+001	1.80000+002	

SENSITIVITY TO 1 5 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 4.51350-001

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.51351+002) + J(0.00000)	(-4.46032+000) + J(0.00000)	2.01317+000	1.80000+002	
(-9.53230+000) + J(0.00000)	(2.05013+002) + J(0.00000)	9.25326+003	1.11022-016	
(-5.74539+000) + J(6.24817-001)	(1.71863+001) + J(6.75027+001)	3.14393+001	7.57160+001	
(-5.74539+000) + J(-6.24817-001)	(1.71863+001) + J(-6.75027+001)	3.14393+001	-7.57160+001	
(-1.24493+000) + J(0.00000)	(4.60945+002) + J(0.00000)	2.06048+002	1.11022-016	

SENSITIVITY TO 2 1 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 1.54718-005

REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.51351+002) + J(0.00000)	(1.42391+003) + J(0.00000)	2.20304+002	1.11022-016	
(-9.53230+000) + J(0.00000)	(9.57771+001) + J(0.00000)	1.48184+003	1.11022-016	
(-5.74539+000) + J(6.24817-001)	(-3.37037+003) + J(-3.76159+004)	5.84317+001	-9.51201+001	
(-5.74539+000) + J(-6.24817-001)	(-3.37037+003) + J(3.76159+004)	5.84317+001	9.51201+001	
(-1.24493+000) + J(0.00000)	(5.05989+000) + J(0.00000)	7.82855+005	0.00000	

SYSTEMS CONTROL, INC. (V.T.)
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

20/04/0 OPTIMAL CONTROL DESIGN POINT LPG2

SENSITIVITY TO 2 2 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -1.43977-004

.....REALPOLE LOCATION.....IMAGINARYREALSENSITIVITY.....IMAGINARYMAGNITUDE.....PHASE.....
(-1.51351+002) + J(0.00000)	(1.85074+003) + J(0.00000)	2.64463-001	1.11022-016		
(-0.55230+000) + J(0.00000)	(-6.61035+002) + J(0.00000)	9.51737-002	1.80000+002		
(-5.74539+000) + J(6.24817-001)	(1.00380+003) + J(5.66308+003)	8.28012-001	7.99591+001		
(-5.74539+000) + J(-6.24817-001)	(1.00380+003) + J(-5.66308+003)	8.28912-001	-7.99591+001		
(-1.24843+000) + J(0.00000)	(-2.52961+001) + J(0.00000)	3.64205-003	1.80000+002		

SENSITIVITY TO 2 3 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 4.79622-003

.....REALPOLE LOCATION.....IMAGINARYREALSENSITIVITY.....IMAGINARYMAGNITUDE.....PHASE.....
(-1.51351+002) + J(0.00000)	(1.17819+001) + J(0.00000)	5.65088-002	2.22045-016		
(-0.55230+000) + J(0.00000)	(4.41817+000) + J(0.00000)	2.11809-002	0.00000		
(-5.74539+000) + J(6.24817-001)	(-7.95591+000) + J(-3.72279+001)	1.82585-001	-1.02063+002		
(-5.74539+000) + J(-6.24817-001)	(-7.95591+000) + J(3.72279+001)	1.82585-001	1.02063+002		
(-1.24843+000) + J(0.00000)	(4.91038-003) + J(0.00000)	2.35513-005	0.00000		

SENSITIVITY TO 2 4 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -2.52918-005

.....REALPOLE LOCATION.....IMAGINARYREALSENSITIVITY.....IMAGINARYMAGNITUDE.....PHASE.....
(-1.51351+002) + J(0.00000)	(1.83421+002) + J(0.00000)	4.63306-003	1.11022-016		
(-0.55230+000) + J(0.00000)	(2.34748+003) + J(0.00000)	5.93719-002	1.11022-016		
(-5.74539+000) + J(6.24817-001)	(-1.27438+003) + J(-3.91342+003)	1.04093-001	-1.04038+002		
(-5.74539+000) + J(-6.24817-001)	(-1.27438+003) + J(3.91342+003)	1.04093-001	1.04038+002		
(-1.24843+000) + J(0.00000)	(1.79689+001) + J(0.00000)	4.51963-004	0.00000		

SENSITIVITY TO 2 5 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 5.36076-004

REAL	POLE LOCATION	IMAGINARY	REAL	SENSITIVITY	IMAGINARY	MAGNITUDE	PHASE
(-1.51351+002)	+ J(0.00000)		(-2.54930+003)	+ J(0.00000)		1.36662+000	1.80000+002
(-9.55230+000)	+ J(0.00000)		(-2.96527+000)	+ J(0.00000)		1.58961+003	1.11022-016
(-5.74539+000)	+ J(6.24817-001)		(-8.64608+001)	+ J(3.01907+002)		1.68351+001	7.40193+001
(-5.74539+000)	+ J(-6.24817-001)		(-8.64608+001)	+ J(-3.01907+002)		1.68351+001	-7.40193+001
(-1.24873+000)	+ J(0.00000)		(-5.82480-001)	+ J(0.00000)		3.12253+004	1.80000+002

SENSITIVITY TO 3 1 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 6.28071-004

REAL	POLE LOCATION	IMAGINARY	REAL	SENSITIVITY	IMAGINARY	MAGNITUDE	PHASE
(-1.51351+002)	+ J(0.00000)		(-7.28595+000)	+ J(0.00000)		4.57610+003	1.80000+002
(-9.55230+000)	+ J(0.00000)		(-3.87483+001)	+ J(0.00000)		2.43367+004	1.80000+002
(-5.74539+000)	+ J(6.24817-001)		(-8.73273+000)	+ J(1.74803+002)		1.09926+001	8.71401+001
(-5.74539+000)	+ J(-6.24817-001)		(-8.73273+000)	+ J(-1.74803+002)		1.09926+001	-8.71401+001
(-1.24873+000)	+ J(0.00000)		(-1.79811+002)	+ J(0.00000)		1.12934+005	0.00000

SENSITIVITY TO 3 2 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 2.66619-003

REAL	POLE LOCATION	IMAGINARY	REAL	SENSITIVITY	IMAGINARY	MAGNITUDE	PHASE
(-1.51351+002)	+ J(0.00000)		(-2.46998+000)	+ J(0.00000)		2.52488+002	1.80000+002
(-9.55230+000)	+ J(0.00000)		(-2.67433+000)	+ J(0.00000)		7.13027+003	1.11022-016
(-5.74539+000)	+ J(6.24817-001)		(-3.61223+000)	+ J(-2.64352+001)		7.11361+002	-9.77811+001
(-5.74539+000)	+ J(-6.24817-001)		(-3.61223+000)	+ J(2.64352+001)		7.11361+002	9.77811+001
(-1.24873+000)	+ J(0.00000)		(-8.98936+002)	+ J(0.00000)		2.39673+004	1.80000+002

AD-A052 346 SYSTEMS CONTROL INC PALO ALTO CALIF AERONAUTICAL AND--ETC F/G 21/5
F100 MULTIVARIABLE CONTROL SYNTHESIS PROGRAM. VOLUME II. APPEND--ETC(U)
JUN 77 R L DE HOFF, W E HALL, R J ADAMS F33615-75-C-2053
UNCLASSIFIED AFAPL-TR-77-35-VOL-2 NL

SYSTEMS CONTROL INC PALO ALTO CALIF AERONAUTICAL AND--ETC F/G 21/5
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SENSITIVITY TO 3 3 ELEMENT OF C		MATRIX:		BASELINE PARAMETER VALUE = -5.4816+001	
.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	
(-1.51351+002) + J(0.00000)		(-6.02957+002) + J(0.00000)		3.30467+002	1.80000+002
(-9.55230+000) + J(0.00000)		(-1.78554+002) + J(0.00000)		9.79363+003	1.80000+002
(-5.74539+000) + J(6.24817+001)		(3.00378+002) + J(1.73845+001)		9.67666+002	8.01970+001
(-5.74539+000) + J(6.24817+001)		(3.00378+002) + J(1.73845+001)		9.67666+002	-8.01970+001
(-1.94493+000) + J(0.00000)		(1.74498+005) + J(0.00000)		9.56528+006	0.00000

SENSITIVITY TO 3 4 ELEMENT OF C		MATRIX:		BASELINE PARAMETER VALUE = 1.33662+003	
.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	
(-1.51351+002) + J(0.00000)		(-9.38544+001) + J(0.00000)		1.25448+003	1.80000+002
(-9.55230+000) + J(0.00000)		(-9.49712+000) + J(0.00000)		1.26941+002	1.80000+002
(-5.74539+000) + J(6.24817+001)		(5.18608+000) + J(1.83547+001)		2.54938+002	7.42225+001
(-5.74539+000) + J(6.24817+001)		(5.18608+000) + J(1.83547+001)		2.54938+002	-7.42225+001
(-1.94493+000) + J(0.00000)		(6.35036+002) + J(0.00000)		8.48804+005	0.00000

SENSITIVITY TO 3 5 ELEMENT OF C		MATRIX:		BASELINE PARAMETER VALUE = -1.62332+002	
.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	
(-1.51351+002) + J(0.00000)		(1.30445+001) + J(0.00000)		2.11754+001	1.1022+016
(-9.55230+000) + J(0.00000)		(-1.1995+002) + J(0.00000)		1.94742+004	1.80000+002
(-5.74539+000) + J(6.24817+001)		(-3.45198+001) + J(-1.41364+000)		2.36253+002	1.03721+002
(-5.74539+000) + J(6.24817+001)		(-3.45198+001) + J(1.41364+000)		2.36253+002	1.03721+002
(-1.94493+000) + J(0.00000)		(-2.06993+003) + J(0.00000)		3.36017+005	1.80000+002

SENSITIVITY TO # 1 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -4.91892-004

.....POLE LOCATION.....
REAL IMAGINARY SENSITIVITY MAGNITUDE PHASE

(-1.51351+002) + J(0.00000) (-2.85947+001) + J(0.00000) 1.00652-002 1.80000+002
(-9.55230+000) + J(0.00000) (2.77215-001) + J(0.00000) 1.36357-004 0.00000
(-5.74539+000) + J(6.24817-001) (2.12658+001) + J(-1.13499+002) 5.67998-002 -7.93879+001
(-5.74539+000) + J(-6.24817-001) (2.12658+001) + J(1.13499+002) 5.67998-002 7.93879+001
(-1.94893+000) + J(0.00000) (-5.94235-001) + J(0.00000) 2.92293-004 1.80000+002

SENSITIVITY TO # 2 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -3.49538-004

.....POLE LOCATION.....
REAL IMAGINARY SENSITIVITY MAGNITUDE PHASE

(-1.51351+002) + J(0.00000) (-3.71662+001) + J(0.00000) 1.29910-002 1.80000+002
(-9.55230+000) + J(0.00000) (-1.91328+000) + J(0.00000) 6.68766-004 1.80000+002
(-5.74539+000) + J(6.24817-001) (-1.74566+000) + J(1.75165+001) 6.15303-003 9.56913+001
(-5.74539+000) + J(-6.24817-001) (-1.74566+000) + J(-1.75165+001) 6.15303-003 -9.56913+001
(-1.94893+000) + J(0.00000) (2.97078+000) + J(0.00000) 1.03840-003 0.00000

SENSITIVITY TO # 3 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 2.98680-001

.....POLE LOCATION.....
REAL IMAGINARY SENSITIVITY MAGNITUDE PHASE

(-1.51351+002) + J(0.00000) (-2.36603-001) + J(0.00000) 7.06486-002 1.80000+002
(-9.55230+000) + J(0.00000) (1.27821-002) + J(0.00000) 3.81775-003 1.11022-016
(-5.74539+000) + J(6.24817-001) (7.44873-003) + J(-1.16159-001) 3.47657-002 -9.63310+001
(-5.74539+000) + J(-6.24817-001) (7.44873-003) + J(1.16159-001) 3.47657-002 9.63310+001
(-1.94893+000) + J(0.00000) (-5.74576-004) + J(0.00000) 1.72242-004 1.80000+002

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

20/5 00 OPTIMAL CONTROL DESIGN POINT LPG2

SENSITIVITY TO 4 4 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -7.21163-004

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-1.5131+002)	+ J(0.00000)	(-3.69344+000)	+ J(0.00000)	2.6115-003	1.80000+002
(-9.55230+000)	+ J(0.00000)	(-6.79448+000)	+ J(0.00000)	4.8015-003	1.11022-016
(-5.74539+000)	+ J(6.24817-001)	(-5.06196+001)	+ J(-1.25739+001)	9.07516-003	-9.23054+001
(-5.74539+000)	+ J(-6.24817-001)	(-5.06196+001)	+ J(1.25739+001)	9.07516-003	9.23054+001
(-1.94493+000)	+ J(0.00000)	(-2.09665+000)	+ J(0.00000)	1.51347-003	1.80000+002

SENSITIVITY TO 4 5 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -6.17304-003

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-1.5131+002)	+ J(0.00000)	(-5.11947+001)	+ J(0.00000)	3.16027-001	1.11022-016
(-9.55230+000)	+ J(0.00000)	(-8.58259-003)	+ J(0.00000)	5.28806-005	0.00000
(-5.74539+000)	+ J(6.24817-001)	(-4.16555-003)	+ J(9.60204-001)	5.92743-003	9.97515+001
(-5.74539+000)	+ J(-6.24817-001)	(-4.16555-003)	+ J(-9.60204-001)	5.92743-003	-8.97515+001
(-1.94493+000)	+ J(0.00000)	(-6.84065-002)	+ J(0.00000)	4.22276-004	1.11022-016

SENSITIVITY TO 5 1 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 3.58915-004

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-1.5131+002)	+ J(0.00000)	(-5.95314+003)	+ J(0.00000)	2.13668-002	1.11022-016
(-9.55230+000)	+ J(0.00000)	(-1.74040+002)	+ J(0.00000)	6.28094-004	1.80000+002
(-5.74539+000)	+ J(6.24817-001)	(-1.06390+004)	+ J(4.01647+004)	1.49129-001	1.04836+002
(-5.74539+000)	+ J(-6.24817-001)	(-1.06390+004)	+ J(-4.01647+004)	1.49129-001	-1.04836+002
(-1.94493+000)	+ J(0.00000)	(-1.07332+003)	+ J(0.00000)	3.87385-003	1.11022-016

SENSITIVITY TO 5 2 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 1.55660-005

.....POLE LOCATION.....SENSITIVITY.....MAGNITUDE.....PHASE.....
REAL	IMAGINARY		
(-1.51351+002) + J(0.00000)	(7.73765+003) + J(0.00000)	1.20444-001	1.11022-016
(-9.55230+000) + J(0.00000)	(1.20395+003) + J(0.00000)	1.87408-002	1.11022-016
(-5.74539+000) + J(6.24817-001)	(1.09064+003) + J(6.23939+003)	9.85951-002	-3.00850+001
(-5.74539+000) + J(-6.24817-001)	(1.09064+003) + J(6.23939+003)	9.85951-002	9.00850+001
(-1.94893+000) + J(0.00000)	(-5.39588+003) + J(0.00000)	8.39923-002	1.80000+002

SENSITIVITY TO 5 3 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = -3.87933-004

.....POLE LOCATION.....SENSITIVITY.....MAGNITUDE.....PHASE.....
REAL	IMAGINARY		
(-1.51351+002) + J(0.00000)	(4.92585+001) + J(0.00000)	1.91090-002	1.11022-016
(-9.55230+000) + J(0.00000)	(-8.04325+000) + J(0.00000)	3.12024-003	1.80000+002
(-5.74539+000) + J(6.24817-001)	(-5.75134+000) + J(4.14853+001)	1.62474-002	9.78930+001
(-5.74539+000) + J(-6.24817-001)	(-5.75134+000) + J(-4.14853+001)	1.62474-002	-9.78930+001
(-1.94893+000) + J(0.00000)	(1.04743+000) + J(0.00000)	4.06331-004	1.11022-016

SENSITIVITY TO 5 4 ELEMENT OF C MATRIX: BASELINE PARAMETER VALUE = 4.49248-006

.....POLE LOCATION.....SENSITIVITY.....MAGNITUDE.....PHASE.....
REAL	IMAGINARY		
(-1.51351+002) + J(0.00000)	(7.66857+002) + J(0.00000)	3.44509-003	1.11022-016
(-9.55230+000) + J(0.00000)	(-4.27550+003) + J(0.00000)	1.92076-002	1.80000+002
(-5.74539+000) + J(6.24817-001)	(-1.51587+002) + J(4.52544+003)	2.03418-002	9.19186+001
(-5.74539+000) + J(-6.24817-001)	(-1.51587+002) + J(-4.52544+003)	2.03418-002	-9.19186+001
(-1.94893+000) + J(0.00000)	(3.81182+003) + J(0.00000)	1.71245-002	1.11022-016

20/04/0 OPTIMAL CONTROL DESIGN POINT LRG2

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

SENSITIVITY TO S S ELEMENT OF C		MATRIX		BASELINE PARAMETER VALUE = 4.09087+005	
.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	
(-1.51351+002) + J(0.00000)		(-1.06583+004) + J(0.00000)		4.36015+001	1.80000+002
(-9.55230+000) + J(0.00000)		(-5.40069+000) + J(0.00000)		2.20935+004	1.80000+002
(-5.74539+000) + J(6.24817+001)		(2.39524+001) + J(-3.44671+002)		1.41341+002	-8.50248+001
(-5.74539+000) + J(-6.24817+001)		(2.39524+001) + J(3.44671+002)		1.41341+002	8.60248+001
(-1.94433+000) + J(0.00000)		(-1.24248+002) + J(0.00000)		5.08282+003	1.80000+002

•FIN

SENSITIVITY OF OPTIMAL CONTROLLER DESIGN

SENSITIVITY TO 1 1 ELEMENT OF A MATRIX: BASELINE PARAMETER VALUE = 1.00000-005

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.51351+002) + J(0.00000)	(1.85639+003)	J(0.00000)	1.86639+002	1.11022-016	
(-2.55230+000) + J(0.00000)	(1.45802+003)	J(0.00000)	1.45802+002	2.22045-016	
(-5.74539+000) + J(6.24817-001)	(-4.78652+004)	J(-1.30202+005)	1.38721+000	-1.10185+002	
(-1.24823+000) + J(0.00000)	(-4.78652+004)	J(1.30202+005)	1.38721+000	1.10185+002	
			2.11519+002	1.11022-016	

SENSITIVITY TO 2 2 ELEMENT OF A MATRIX: BASELINE PARAMETER VALUE = 1.00000-004

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.51351+002) + J(0.00000)	(-9.21384+002)	J(0.00000)	9.21384+002	1.80000+002	
(-2.55230+000) + J(0.00000)	(6.46910+003)	J(0.00000)	6.46910+001	1.11022-016	
(-5.74539+000) + J(6.24817-001)	(-2.47343+003)	J(-2.88237+004)	2.89296+000	-9.40048+001	
(-1.24823+000) + J(0.00000)	(-2.47343+003)	J(2.88237+004)	2.89296+000	9.40048+001	
			7.43718+001	1.80000+002	

SENSITIVITY TO 3 3 ELEMENT OF A MATRIX: BASELINE PARAMETER VALUE = 5.00000-002

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.51351+002) + J(0.00000)	(-1.04746+002)	J(0.00000)	5.23979+004	1.80000+002	
(-2.55230+000) + J(0.00000)	(-2.21691+002)	J(0.00000)	1.10445+003	1.80000+002	
(-5.74539+000) + J(6.24817-001)	(-3.09383+002)	J(-7.31255+002)	3.97005+003	-1.12933+002	
(-1.24823+000) + J(0.00000)	(-3.09383+002)	J(7.31255+002)	3.97005+003	1.12933+002	
			1.13988+004	1.11022-016	

20/004/0 OPTIMAL CONTROL DESIGN POINT LPGA

SYSTEMS CONTROL, INC. (VT) -
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SENSITIVITY TO 4 4 ELEMENT OF A MATRIX: BASELINE PARAMETER VALUE = 0.00000

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.51331+002) + J(0.00000)	(-1.92229+002)	J(0.00000)	1.92229+002	1.90000+002	
(-9.55230+000) + J(0.00000)	(-7.08890+004)	J(0.00000)	7.08890+004	1.90000+002	
(-5.74537+000) + J(5.24817-001)	(1.17897+004)	J(4.43157+004)	4.58571+004	7.51022+001	
(-5.74537+000) + J(-6.24817-001)	(1.17897+004)	J(-4.43157+004)	4.58571+004	-7.51022+001	
(-1.51331+002) + J(0.00000)	(7.89943+003)	J(0.00000)	7.89943+003	1.11022-016	

SENSITIVITY TO 5 5 ELEMENT OF A MATRIX: BASELINE PARAMETER VALUE = 8.00000-003

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.51331+002) + J(0.00000)	(-8.35451+002)	J(0.00000)	8.35451+002	1.80000+002	
(-9.55230+000) + J(0.00000)	(9.33026-001)	J(0.00000)	7.26421-003	1.11022-016	
(-5.74537+000) + J(5.24817-001)	(1.07909+001)	J(-8.10883+000)	1.07984-001	-3.69230+001	
(-5.74537+000) + J(-6.24817-001)	(1.07909+001)	J(8.10883+000)	1.07984-001	3.69230+001	
(-1.51331+002) + J(0.00000)	(-8.00586+000)	J(0.00000)	6.40549-002	1.80000+002	

SENSITIVITY TO 1 1 ELEMENT OF B MATRIX: BASELINE PARAMETER VALUE = 1.00000-004

POLE LOCATION	REAL	IMAGINARY	SENSITIVITY	MAGNITUDE	PHASE
(-1.51331+002) + J(0.00000)	(4.38459+004)	J(0.00000)	4.38459+000	1.11022-016	
(-9.55230+000) + J(0.00000)	(-6.20598+003)	J(0.00000)	6.20598-001	1.80000+002	
(-5.74537+000) + J(5.24817-001)	(4.78278+003)	J(3.07098+004)	3.10769+000	9.11843+001	
(-5.74537+000) + J(-6.24817-001)	(4.78278+003)	J(-3.07098+004)	3.10769+000	-9.11843+001	
(-1.51331+002) + J(0.00000)	(7.60014+003)	J(0.00000)	7.60014-001	0.00000	

20/04/70 SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

20/04/70 SYSTEM CONTROL DESIGN POINT LP62

SENSITIVITY TO 2 2 ELEMENT OF B		MATRIX:		BASELINE PARAMETER VALUE = 1.00000+002	
.....POLE LOCATION..... REAL IMAGINARY			SENSITIVITY..... REAL IMAGINARY MAGNITUDE PHASE	
(-1.51351+002) + J(0.00000)		(1.51414-002) + J(0.00000)		1.51414+000 1.11022-016	
(-9.55230+000) + J(0.00000)		(-4.47275-004) + J(0.00000)		4.47275-002 1.80000+002	
(-5.74539+000) + J(6.24817-001)		(1.45254-003) + J(1.17611-002)		1.18505+000 8.29595+001	
(-5.74539+000) + J(-6.24817-001)		(1.45254-003) + J(-1.17611-002)		1.18505+000 -9.29595+001	
(-1.51351+002) + J(0.00000)		(-1.41390-004) + J(0.00000)		1.41390-002 1.80000+002	
SENSITIVITY TO 3 3 ELEMENT OF B		MATRIX:		BASELINE PARAMETER VALUE = 2.00000-002	
.....POLE LOCATION..... REAL IMAGINARY			SENSITIVITY..... REAL IMAGINARY MAGNITUDE PHASE	
(-1.51351+002) + J(0.00000)		(1.02141+001) + J(0.00000)		2.04282-001 1.11022-016	
(-9.55230+000) + J(0.00000)		(-1.47840-001) + J(0.00000)		2.95680-003 1.80000+002	
(-5.74539+000) + J(6.24817-001)		(3.58210-001) + J(3.74589-001)		1.03659-002 4.62805+001	
(-5.74539+000) + J(-6.24817-001)		(3.58210-001) + J(-3.74589-001)		1.03659-002 -4.62805+001	
(-1.51351+002) + J(0.00000)		(-3.30137-002) + J(0.00000)		6.60275-004 1.80000+002	
SENSITIVITY TO 4 4 ELEMENT OF B		MATRIX:		BASELINE PARAMETER VALUE = 2.00000-001	
.....POLE LOCATION..... REAL IMAGINARY			SENSITIVITY..... REAL IMAGINARY MAGNITUDE PHASE	
(-1.51351+002) + J(0.00000)		(1.74947+000) + J(0.00000)		3.49894+001 1.11022-016	
(-9.55230+000) + J(0.00000)		(4.23190-005) + J(0.00000)		8.46380-006 0.00000	
(-5.74539+000) + J(6.24817-001)		(2.28429-002) + J(-3.60265-002)		8.53161-003 -5.76230+001	
(-5.74539+000) + J(-6.24817-001)		(2.28429-002) + J(3.60265-002)		8.53161-003 5.76230+001	
(-1.51351+002) + J(0.00000)		(-2.03658-005) + J(0.00000)		4.07316-006 1.80000+002	

20/00/0 OPTIMAL CONTROL DESIGN POINT LPG2

SYSTEMS CONTROL INC.(VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

SENSITIVITY TO 5 5 ELEMENT OF B MATRIX: BASELINE PARAMETER VALUE = 1.00000+000

.....POLE LOCATION.....	SENSITIVITY.....	PHASE.....	
REAL	IMAGINARY	REAL	IMAGINARY	MAGNITUDE	PHASE
(-1.51351+002)	+ J(0.00000)	(3.05453-005)	+ J(0.00000)	3.05453-001	0.00000
(-9.53230+000)	+ J(0.00000)	(3.61143-008)	+ J(0.00000)	3.61143-004	1.11022-016
(-5.74539+000)	+ J(6.24917-001)	(8.01346-007)	+ J(5.95755-007)	9.98538-003	3.66287+001
(-5.74539+000)	+ J(-6.24917-001)	(8.01346-007)	+ J(-5.95755-007)	9.98538-003	-3.66287+001
(-1.44433+000)	+ J(0.00000)	(4.13745-006)	+ J(0.00000)	4.13745-002	1.11022-016

APPENDIX G
INTEGRAL CONTROL DESIGN DATA AND EXAMPLE DESIGN

G.1 DATA FOR INTEGRAL CONTROL DESIGN

The integral control designs were carried out at the six control design points according to the procedure described in Sections 4.6 and 5.8.3 of Volume I of this report. The data used in the designs is included in this section. The matrices used in the general development presented in Section 4.6 are shown here for the conditions listed in Table G.1. Table G.2 reviews the general equations to define the matrix outputs presented. A specific example is shown in Section G.2. The order of states, outputs and controls is given in Table G.3.

Table G.1
Index of Steady-State Gain Matrices

CASE	DESIGN POINT	PLA (DEG)	ALTITUDE (FT)	MACH NO. (-)	PAGE
1	HPG1	83	45K	0.9	392
2	HPG2	83	30K	0.9	394
3	HPG3	83	0	0	396
4	HPG4	83	0	1.2	398
5	LPG1	20	30K	0.9	400
6	LPG2	20	0	0	402

Table G.2
Integral Design Relationships

$$\delta \dot{x} = F\delta x + G\delta u \quad (G.1)$$

$$\delta y = H\delta x + D\delta u \quad (G.2)$$

$$\text{For } \delta \dot{x} = 0, \quad (G.3)$$

$$\delta u = C_x \delta x + \delta u' \quad (G.4)$$

$$\delta x = -(F + GC)^{-1} G\delta u' \quad (G.5)$$

$$\delta y = \bar{H}\delta u' \quad (G.6)$$

$$\bar{H} = -(H + DC_x)(F + GC_x)^{-1}G + D \quad (G.7)$$

Integral System

$$\delta y_S = y - y_{SP} \quad (G.8)$$

$$\dot{b} = \delta y_S \quad (G.9)$$

$$\delta u' = C_b b \quad (G.10)$$

$$\dot{b} = \bar{H}C_b b \quad (G.11)$$

Table G.3
Order of States, Outputs, and Controls

STATE	SYMBOL	UNITS
1	N_1	RPM
2	N_2	RPM
3	PT6M	PSI
4	WF	LBM/HR
5	PT4	PSI
CONTROL		
1	WF	LBM/HR
2	AJ	FT ²
3	CIVV	DEG
4	RCVV	DEG
5	BLD	FRACT. COMPRESSOR FLOW
OUTPUT		
1	FN	LBF
2	WCF	LBM/SEC
3	TT4	°R
4	SMAF	---
5	SMHC	---
6*	$(\Delta p/p)_{\text{EXP}}$	---
7*	$(\Delta p/p)_{\text{AVG}}$	---

* Not included in some models

CASE 1

F+GC

	1	2	3	4	5
1	-7.6831-001	-1.2760-001	-1.0871+003	1.5061+000	1.4055+002
2	1.1874+000	-1.4418+000	-2.0423+002	9.8903+002	1.0389+002
3	1.2094+002	-5.1019-003	-1.0293+001	7.2067+003	5.4553+001
4	-7.2996+000	-1.1293+001	-3.6698+001	-1.3477+001	4.4277+001
5	-1.3463+000	1.1781+000	4.7737+002	1.0526+000	2.6144+002

(F+GC)⁻¹

	1	2	3	4	5
1	-3.2351-001	6.7577+002	2.8643+001	-2.7509+002	-9.1918+002
2	-8.2375+002	-7.0191+001	8.2923+000	-3.4271+002	-3.1173+001
3	-4.5049+005	8.2340+004	-1.0505+001	-4.9284+005	7.5412+005
4	2.5169+001	5.5003+001	-2.3491+001	-3.1198+002	2.9960+001
5	2.2258+003	2.0714+004	-3.9664+001	-2.2838+004	-3.4124+003

(F+GC)⁻¹G

	1	2	3	4	5
1	-1.8668+001	-4.5501+002	1.3743+001	-1.7989+000	1.2425+003
2	-2.6569+001	-1.4172+002	-5.4008+000	5.5897+000	5.8668+002
3	-4.0156+004	2.2535+000	5.0975+003	-2.4256+003	4.7362+000
4	-4.2223+001	3.8573+002	-3.0988+000	-3.8325+000	-1.0154+003
5	-1.5451+003	8.1130+000	5.0883+002	-3.9379+002	7.4850+001

(F+GC)⁻¹G

	1	2	3	4	5
1	1.8668-001	4.5501+002	-1.3743+001	1.7989+000	-1.2425+003
2	2.6569-001	1.4172+002	5.4008+000	-5.5897+000	-6.8668+002
3	4.0156-004	-2.2535+000	-5.0975-003	2.4256-003	-4.7362+000
4	4.2223-001	-3.8573+002	3.0988+000	3.8325+000	1.0154+003
5	1.5451-003	-8.1130+000	5.0883-002	3.9379-002	-7.4850+001

H

	1	2	3	4	5
1	1.1900-002	2.1792+001	3.4522+000	1.5263+000	-6.9023+001
2	-8.9708-004	-2.1162+000	1.2123+001	8.9635-003	-3.5414+000
3	1.7880-001	3.4736+001	1.3328+000	1.8116+000	2.4826+003
4	2.1257-005	2.4890-001	-1.7384-003	4.1239-004	6.0767-001
5	-4.0457-005	-7.6416-002	5.5148-005	-2.5857-003	-2.5617-001
6	-1.0941-005	1.5860-001	1.0446-003	-1.7131-004	3.2194-001
7	-1.3333-006	4.6121-002	4.9299-004	7.7515-007	7.9519-002

CASE 2

F+GC

	1	2	3	4	5
1	-1.1700+000	-2.1283+000	-4.6145+002	-6.6415+001	3.6321+002
2	6.0230+001	-1.7222+000	-2.0805+002	1.6144+000	5.7133+001
3	3.2257+002	5.1611+003	-1.3525+001	1.5105+002	-3.4389+001
4	-0.1529+000	-1.0000+001	-1.3411+002	-1.5824+001	2.6678+001
5	-1.3555+000	1.6044+000	1.0674+002	1.0593+000	-5.0500+002

(F+GC)⁻¹

	1	2	3	4	5
1	-3.6966+001	5.3001+002	6.4402+000	1.3284+002	-2.5857+001
2	7.3741+002	-5.2151+001	5.0429+000	-3.0653+002	6.9787+003
3	-8.8917+000	0.6407+000	-6.2693+002	-1.1004+005	-5.1721+004
4	2.9727+002	3.0369+001	-7.2922+000	-3.2471+002	5.6018+002
5	0.6246+000	-0.1154+000	-0.1273+002	-2.1193+004	-1.3467+003

(F+GC)⁻¹G

	1	2	3	4	5
1	-1.3330+001	-0.2166+002	1.5599+001	-4.5501+000	5.1823+002
2	-1.3045+001	-2.2010+002	-1.4000+000	7.6836+000	1.6217+003
3	-2.5194+000	5.3304+000	2.7355+002	-1.0229+002	2.8641+000
4	-0.3920+001	0.7557+002	-1.7551+000	-7.7537+000	-1.4971+003
5	-6.9337+004	5.6404+000	7.1701+002	-4.1041+002	1.2210+002

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

RT/0.0/30K OPTIMAL CONTROL DESIGN POINT HPG2

-(F+GC)⁻¹G

	1	2	3	4	5
1	1.3330+001	4.0146+002	-1.5599+001	4.5501+000	-5.1823+002
2	1.3965+001	2.0210+002	1.8640+000	-7.6836+000	-1.8217+003
3	2.5196+001	-1.3399+000	-2.7355+002	1.0229+002	-2.8641+000
4	4.3920+001	-4.7697+002	1.7551+000	7.7537+000	1.4971+003
5	4.9337+001	-5.4474+000	-7.1791+002	4.1081+002	-1.2219+002

H

	1	2	3	4	5
1	-2.0291+001	4.5217+002	1.7657+000	7.6374+000	6.6984+003
2	1.1245+003	4.1122+000	2.3205+001	3.7142+002	-2.7608+000
3	5.2646+002	4.0745+001	8.0716+001	3.3091+000	3.1094+003
4	1.2824+005	2.0213+001	1.4207+003	9.7613+004	1.0237+000
5	4.0649+005	-1.3656+001	2.0608+005	-2.7229+003	-8.0035+001
6	-1.7687+005	2.0000+001	1.0425+003	2.6853+004	1.0784+000
7	-1.5443+004	4.0114+002	5.5467+004	8.4227+005	2.6352+001

MS/C/OK OPTIMAL CONTROL DESIGN POINT MPG3

CASE 3

F+GC

	1	2	3	4	5
1	-3.0501+000	-5.2122+001	-7.5624+002	8.0724+001	1.8914+002
2	1.4770+000	-5.0107+000	-2.1068+002	2.3519+001	9.4269+001
3	4.2382+002	-2.0520+002	-1.4397+001	5.7035+003	5.2383+001
4	-5.1055+000	-1.0244+001	-3.0051+002	-1.2407+001	2.8550+001
5	-1.4304+000	2.7273+000	3.6324+002	4.9321+001	-3.4951+002

(F+GC)⁻¹

	1	2	3	4	5
1	-1.0049+001	-1.3380+002	6.1581+000	-9.7836+003	-7.3639+002
2	-1.2307+002	-1.2310+001	1.0638+000	-5.0512+003	-4.9489+002
3	-1.5554+000	3.8660+004	-5.0004+002	-5.2036+005	-1.9686+004
4	8.8559+002	2.6000+001	-4.3697+000	-6.7707+002	1.0597+001
5	0.1875+000	-5.3120+004	-8.4927+002	-1.3780+004	-2.9163+003

(F+GC)^{-1G}

	1	2	3	4	5
1	-1.0930+001	-4.1072+002	1.0767+001	-3.4724+000	9.6179+002
2	-0.7314+002	-3.5667+002	-5.2641+001	7.3693+000	1.4041+003
3	-2.5785+000	4.4807+000	1.0766+002	-9.1264+003	1.1880+001
4	-6.0422+001	5.4226+002	-7.6526+000	-1.0203+001	-2.4278+003
5	-0.3250+000	7.2607+000	-3.5711+002	-1.2721+001	1.9924+002

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

RT/CLK OPTIMAL CONTROL DESIGN POINT MPG3

$-(F+GC)^{-1}G$

	1	2	3	4	5
1	1.0930-001	4.1672+002	-1.9767+001	3.4724+000	-9.6179+002
2	9.7314-002	3.3447+002	5.2661-001	-7.3693+000	-1.4041+003
3	2.5745-000	-5.4307+000	-1.0768-002	9.1266+003	-1.1880+001
4	4.0426-001	-5.4294+002	7.4528+000	1.0203+001	2.4278+003
5	9.3250-004	-7.2507+000	3.5711-002	1.2721-001	-1.9924+002

H

	1	2	3	4	5
1	4.1394-002	-3.7233+001	1.3275+001	7.3647+000	2.7915+003
2	1.5873-003	4.0560+000	4.0432-001	4.9499-002	-1.2867+001
3	4.0340-002	1.3147+002	-2.2491-001	1.3421+000	2.3364+003
4	7.2722-004	1.4440-001	-7.1345-003	2.4916-004	1.8088-001
5	1.1455-005	-5.7735-002	2.7967-004	-2.1896+003	1.8820+002
6	-2.4143-004	1.1204-001	4.3497-004	-3.3480+005	2.6434-001
7	7.7560-007	1.5529-002	3.9450-004	2.9123-005	5.3197-002

R3/1.2/0K OPTIMAL CONTROL DESIGN POINT HPG4

CASE 4

F+GC

	1	2	3	4	5
1	-4.8405+000	4.1274+001	-5.3711+002	6.2353+001	1.7317+002
2	-2.2707+000	-9.6698+000	2.4385+002	-2.6698+001	7.2114+001
3	2.2403+002	-1.5412+002	-1.3092+001	1.1802+002	4.3210+001
4	-1.1008+001	-2.6511+001	1.6571+002	-1.3526+001	8.0709+001
5	2.7533+000	7.3897+000	-9.0233+001	1.1023+000	-2.6236+002

(F+GC)⁻¹

	1	2	3	4	5
1	-1.0478+001	-5.3444+002	3.7497+000	-6.5274+003	-7.4093+002
2	1.6490+002	-1.1200+001	-2.6130+000	-1.1675+003	-2.2824+002
3	-1.6459+004	1.4349+004	-4.5645+002	-8.3309+005	-1.7955+004
4	4.8784+002	2.4993+001	1.2312+000	-6.9258+002	7.5838+002
5	-3.0410+000	-2.6446+003	-5.0341+003	-3.3678+004	-4.5055+003

398

(F+GC)^{-1G}

	1	2	3	4	5
1	-6.7656+002	-5.2043+002	2.4129+001	-1.1999+001	2.9701+003
2	-6.8267+002	9.8220+001	-8.1541+001	8.5615+000	2.1051+003
3	-4.6009+004	4.6301+000	-4.3604+002	1.0833+003	2.5902+001
4	-5.7127+001	3.5075+002	-2.2504+001	-1.0463+001	-3.4225+003
5	-2.6470+003	1.1846+000	-6.7781+001	-5.6242+001	4.6899+002

#3/1.2/0K OPTIMAL CONTROL DESIGN POINT MP64

(F+GC) ⁻¹G

	1	2	3	4	5
1	6.7656-002	5.2043+002	-2.4124+001	1.1999+001	-2.9701+003
2	6.8267-002	-9.8629+001	8.1541+001	-8.5615+000	-2.1051+003
3	4.6009-004	-9.4301+000	4.3604+002	-1.0833+003	-2.5902+001
4	5.7127-001	-1.5475+002	2.2544+001	1.0463+001	3.4225+003
5	2.6876-003	-1.1144+000	6.7781+001	5.8262+001	-4.6699+002

H

	1	2	3	4	5
1	2.0066-001	-6.9544+002	-1.3510+000	-1.8840+001	2.6397+003
2	2.5432-003	1.4115+001	1.0444+000	4.2099+001	-8.8645+001
3	5.1803-002	2.0931+001	-1.7080+000	-2.4829+000	1.8564+003
4	1.7681-006	1.4455+002	-6.5249+003	1.0600+003	-1.2037+001
5	1.2624-005	-4.5492+002	1.7033+003	-2.5448+003	5.6158+002

CASE 5

F+GC				
	1	2	3	4
1	-4.5498-001	6.0351-001	-5.0490+002	1.3400+000
2	1.1813-001	-1.0040+000	-1.5458+002	2.4150+000
3	1.0294-002	-3.4016-003	-7.6093+000	1.3718-002
4	-5.7468+000	-1.4220+001	1.4280+002	-1.6911+001
5	3.1449+001	2.3255+000	9.3940+001	1.5943+000
				1.2991+002
				3.9185+001
				3.5829+001
				8.8628+001
				-1.3937+002
(F+GC) ⁻¹				
	1	2	3	4
1	-4.7262-001	-2.1575-001	2.8272+001	-9.1276-002
2	1.2421-001	-3.4413-001	-2.2639+000	-4.2467-002
3	-5.2795-004	2.2179-004	-1.1696-001	-1.4949-004
4	5.8642-002	3.5451-001	-9.5257+000	1.0751-003
5	1.3226-003	-1.4470-003	-1.6238-001	-1.0029-003
				-7.5195-003
				-4.8654-001
				-1.3861-002
				-7.6952-004
				1.3109-001
400 (F+GC) ^{-1G}				
	1	2	3	4
1	-4.2304-001	-4.4669+002	9.7043-001	-1.2066+001
2	-2.9404-001	4.2211+001	4.2073-001	5.5844+000
3	-4.9285-004	1.7003+000	-6.6143-003	-1.6305-002
4	-2.6007-001	1.4710+002	-9.9315-001	-1.6506+000
5	-4.1467-003	2.9775+000	-4.4394-002	-1.7505-001
				6.5074+001
				9.1453+002
				1.1752+003
				3.9842+000
				-2.2429+002

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

20/0.0/30K OPTIMAL CONTROL DESIGN POINT LPI

(F+GC)⁻¹G

	1	2	3	4	5
1	4.2304-001	4.4660+002	-9.7043-001	1.2046+001	-9.1453+002
2	2.9404-001	-4.2211+001	-4.2073-001	-5.5644+000	-1.1752+003
3	8.9245-004	-1.7993+000	6.6133-003	1.6305-002	-3.9842+000
4	2.4007-001	-1.4710+002	9.9315-001	1.6506+000	9.2429+002
5	6.1047-003	-2.3775+000	4.8394-002	1.7505-001	-6.5074+001

H

	1	2	3	4	5
1	4.4046-002	-5.2247+002	2.0432+000	4.2270+000	-9.9857+002
2	4.0042-003	5.1241+000	7.5073-002	1.3844-001	-7.6353+000
3	-2.5419-003	-1.2044+002	2.0045-001	-8.8488-001	1.6702+003
4	1.0044-005	1.1504+001	-4.5341-003	1.8796-003	-9.8800-002
5	3.5544-002	1.5414-002	5.5513-005	-6.5025-003	5.7449-001
6	-3.6730-005	1.7037-001	-4.2209-004	2.0060-004	2.5959-001
7	-1.7624-004	4.4205-002	7.2444-005	1.9878-004	4.5366-002

20/0/00 OPTIMAL CONTROL DESIGN POINT LPGA

CASE 6

F+GC

	1	2	3	4	5
1	6.4650-001	7.1792+000	-6.1859+003	1.3164+001	6.2468+001
2	-1.9784+000	-4.3412+000	3.1155+003	-5.5979+000	1.1668+002
3	-2.0329-003	-1.5005-002	-5.1498+001	-2.7622-002	6.6849+001
4	-2.7586-001	-2.7384+000	-1.1290+002	-1.1232+001	4.5135+000
5	1.4129+000	2.2674+000	-2.3664+003	6.8943+000	-1.5486+002

(F+GC)⁻¹

	1	2	3	4	5
1	-3.8944-001	-3.0256-001	2.3009+002	-5.0717-001	5.4338-001
2	1.9962-002	-4.9001-001	-7.1226+001	2.5612-002	-6.7021-001
3	-1.5066-004	-1.1484-004	2.0080+002	-2.5941-004	-4.2094+005
4	2.2496-003	2.0700-001	3.4492+001	-9.1030-002	3.4130-001
5	-4.7990-004	-1.4442-002	1.4415-002	-4.2003-003	-1.7595+002

(F+GC)⁻¹G

	1	2	3	4	5
1	-1.2640+000	-2.4047+002	3.4152+000	-1.1098+001	4.5841+003
2	-7.3493-001	-4.3245+001	4.2413+002	1.7744+001	1.9628+003
3	-1.0135-003	2.0156-001	-1.5701-003	-4.3876+003	3.5094+000
4	-4.1972-001	3.5484+001	-1.2963+001	9.3575+002	-1.2919+003
5	2.0199+002	-1.6174+000	-1.4006+002	-3.3976+001	1.1360+002

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

20/0/000 OPTIMAL CONTROL DESIGN POINT LRG2

$$-(F+GC)^{-1}G$$

1	1.2880+000	2.6087+002	3.6152+000	1.1098+001	-4.5861+003
2	7.3493+001	6.3285+001	-8.2413+002	-1.7748+001	-1.9828+003
3	1.0135+003	-2.0159+001	1.5701+003	6.3876+003	-3.5099+000
4	4.1972+001	-3.5886+001	1.2963+001	-9.3575+002	1.2919+003
5	3.0199+002	1.6178+000	1.8000+002	3.3976+001	-1.1366+002

$$H$$

1	8.9527+001	-2.4131+002	1.1217+000	4.6356+000	-3.0740+003
2	9.6806+003	4.7218+000	4.2511+002	1.9608+001	-6.2653+001
3	3.3914+001	-2.2753+001	-1.6846+001	-3.7149+000	1.2921+003
4	-4.4576+004	-2.2191+003	-3.9265+003	-2.1715+004	6.6431+001
5	-7.3479+004	-1.2408+002	3.1130+004	1.5020+003	2.1648+000
6	-2.3133+004	1.4067+002	-2.5380+004	1.1671+004	1.3998+001
7	-2.5698+005	5.9737+003	3.7069+005	1.1554+004	-3.2383+002

G.2 EXAMPLE OF DESIGN CYCLE WITH VERIFICATION SHOWING EIGEN-VALUES OF AUGMENTED LINEAR SYSTEMS

The procedure discussed in Section 5.8.3 (Volume I) is used to design a controller for one design point, intermediate power, sea level static conditions (83/0/0). The design proceeds by using LQR methods to produce an acceptable transient regulator design (Step 1). Next, the sensitivities of closed-loop response are used to eliminate gain elements which are not important in the controlled response (Step 2). The integral trim designs are produced and the integral poles are augmented to the original system. The closed-loop poles for the simplified transient regulator and each of three possible trim modes are calculated for the augmented linear system in Steps 3, 4, and 5. This final check assures acceptable stability with an accurate linear description of the augmented plant. Table G.4 lists the steps and indexes the tabular data representing the actual eigenvalue locations calculated by the software. Figures G.1 and G.2 graphically show the movement of the closed-loop roots as the design and evaluation proceeds.

Table G.4

STEP	COMMENT	PAGE
1	Baseline LQR synthesis at 83/0K/0	407
2	Regulator matrix reduced by eight terms	411
3	Augmented system with five integral roots - N_1 - $\Delta p/p$ trim mode	412
4	FTIT - $\Delta p/p$ trim mode	415
5	P_B - $\Delta p/p$ trim mode	418

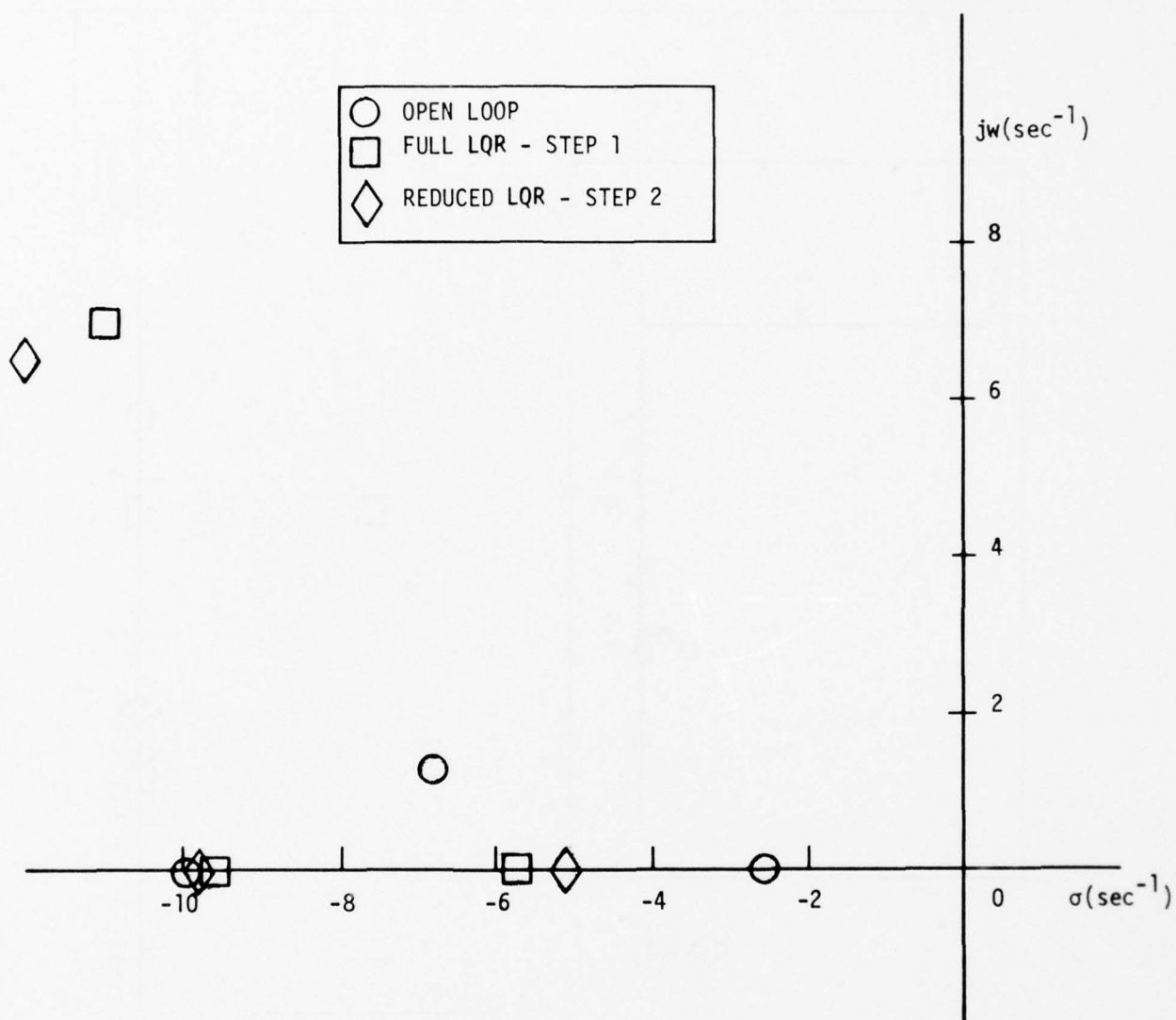


Figure G.1 Open-Loop Poles, Full LQR Poles and Simplified LQR Poles (Step 1 and Step 2)

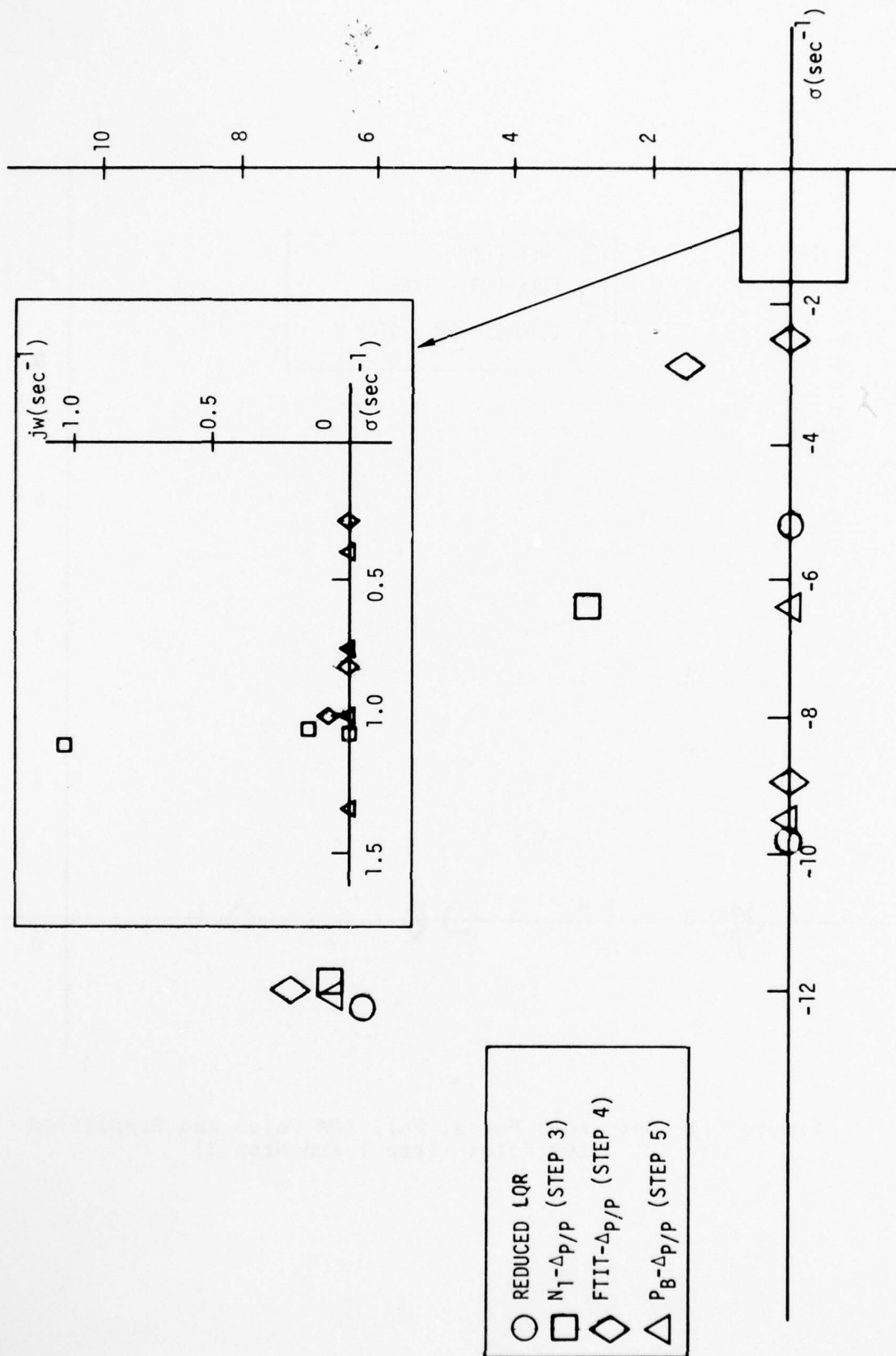


Figure G.2 Effect of Integral Control on Simplified LQR Roots - Steps 3, 4, and 5

STEP 1

```

♦-----♦
♦ INPUT DATA ♦
♦-----♦

```

```

NUMBER OF STATES = 5
NUMBER OF CONTROLS = 5
NUMBER OF OUTPUTS = 7
NUMBER OF PROCESS NOISE SOURCES = 1
NUMBER OF OBSERVATIONS = 1

```

NUMBER OF SENSITIVITY PARAMETERS = 0

DESIGN MODEL AND WEIGHTS FOR
TRANSIENT CONTROL

	1	2	3	4	5
1	0.0000-004	0.0000	0.0000	0.0000	0.0000
2	0.0000	4.0000-004	0.0000	0.0000	0.0000
3	0.0000	0.0000	1.0000-001	0.0000	0.0000
4	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000	0.0000	0.0000

	1	2	3	4	5
1	1.0000-004	0.0000	0.0000	0.0000	0.0000
2	0.0000	2.0000+001	0.0000	0.0000	0.0000
3	0.0000	0.0000	2.5000-001	0.0000	0.0000
4	0.0000	0.0000	0.0000	1.0000-001	0.0000
5	0.0000	0.0000	0.0000	0.0000	1.0000+005

A3/0/0K REDUCED LINEAR MODEL DESIGN

	1	2	3	4	5
1	-3.2450+000	-2.1580+000	-9.1550+002	5.7310+001	1.3420+002
2	1.4420+000	-5.9410+000	-2.8160+002	1.8970+001	5.7050+001
3	1.6860+002	-2.5540+002	1.0030+001	7.9940+003	5.8070+001
4	0.0000	0.0000	0.0000	1.0000+001	0.0000
5	-2.1630+000	6.8620+000	7.4050+002	1.1950+000	-1.7150+002

6

	1	2	3	4	5
1	1.4320+002	-3.5530+002	-9.9060+001	-1.5490+001	2.2200+004
2	2.8710+001	7.2860+002	2.5140+001	-6.4870+001	8.1220+003
3	-2.4690+003	-1.0330+002	6.3330+001	-3.2130+001	-7.4180+001
4	1.0000+001	0.0000	0.0000	0.0000	0.0000
5	-1.3110+001	3.2950+002	-2.5000+001	6.2570+001	-6.4450+004

HY

	1	2	3	4	5
1	1.4620+000	-1.7680+000	7.9990+001	-1.8900+001	3.7710+001
2	1.3830+002	3.1420+006	1.0000+002	1.2890+004	-1.8390+007
3	1.6940+001	-1.1290+001	-4.9590+000	7.3860+002	-1.8350+001
4	7.5900+005	3.2690+006	-1.4770+002	2.2840+006	4.3150+005
5	-4.4590+005	1.3610+004	1.1400+002	1.9510+005	-2.8880+003
6	5.1770+005	-3.9090+005	-1.2300+002	-1.2280+005	2.0790+004
7	1.5700+005	-2.2070+006	-3.2950+003	-2.6460+006	9.9150+006

OPTIMAL CLOSED-LOOP EIGENSYSTEM

CLOSED-LOOP POLES FOR
STEP 1

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-1.74618+0.02j)+j(0.00000)	0.00000	1.00000	1 (-8.06246+0.01j)+j(0.00000) 2 (-3.36304+0.01j)+j(0.00000) 3 (-3.47389+0.03j)+j(0.00000) 4 (-1.59454+0.04j)+j(0.00000) 5 (1.00000+0.00j)+j(0.00000)	-8062462 -3363044 -0034739 -0001595 1.0000000	.00000 .00000 .00000 .00000 .00000
(-1.14961+0.01j)+j(-6.93704+0.00j)+j(1.35926+0.01j)	1.35926+0.01j	.86610	1 (1.00000+0.00j)+j(0.00000) 2 (-5.66051+0.02j)+j(9.26456+0.02j) 3 (1.39971+0.02j)+j(-2.40777+0.02j) 4 (-1.05011+0.01j)+j(1.52724+0.01j) 5 (3.55219+0.02j)+j(-1.14011+0.01j)	1.0000000 .1085695 .0278506 .1842167 .1194166	.00000 121.42433 -59.82927 123.99938 -72.69475
(-5.90184+0.00j)+j(0.00000)	0.00000	1.00000	1 (-3.80943+0.01j)+j(0.00000) 2 (1.00000+0.00j)+j(0.00000) 3 (1.31485+0.02j)+j(0.00000) 4 (-3.74230+0.01j)+j(0.00000) 5 (1.09910+0.01j)+j(0.00000)	-3809432 1.0000000 .0131485 -3742304 -1099100	.00000 .00000 .00000 .00000 .00000
(-9.84470+0.00j)+j(0.00000)	0.00000	1.00000	1 (4.01643+0.02j)+j(0.00000) 2 (-1.36439+0.01j)+j(0.00000) 3 (3.74593+0.03j)+j(0.00000) 4 (1.00000+0.00j)+j(0.00000) 5 (-1.78089+0.02j)+j(0.00000)	.0441643 -1364369 .0037459 1.0000000 -0178089	.00000 .00000 .00000 .00000 .00000

THE EIGENVALUE MATRIX

83/0704 REDUCED LINEAR MODEL DESIGN

SYSTEMS CONTROL, INC. (VT) -
TIME-DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

	1	2	3	4	5
1	2.6133-005	3.4553-006	-4.2355-004	1.5270-006	1.8951-005
2	3.4553-006	3.9572-005	-9.3247-005	1.5319-006	1.5015-005
3	-4.2355-004	-9.3247-005	1.5638-002	-3.5242-005	-3.1356-004
4	1.5270-006	1.5319-006	-3.5242-005	2.1425-007	1.6125-006
5	1.8951-005	1.5015-005	-3.1356-004	1.6125-006	1.8422-005

CONTROLLER FEEDBACK GAINS

	1	2	3	4	5
1	-1.5198-001	-2.4491-001	3.4270-000	-2.4798-002	-1.9066-001
2	-2.1551-003	-2.1078-003	8.1574-002	-2.3674-004	-2.1287-003
3	1.2976-002	-8.7253-004	-2.2942-001	7.0154-004	8.6354-003
4	-6.6291-003	1.4511-002	1.2634-001	1.0811-004	1.4170-004
5	5.8176-006	5.6270-006	-8.4888-005	5.4967-007	6.2138-006

F

	1	2	3	4	5
1	-3.2450+000	-2.1540+000	9.1550+002	5.7310-001	1.3420+002
2	1.4220+000	-5.4410+000	-2.8160+002	1.8970-001	5.7050+001
3	1.6860-002	-2.5540-002	-1.0030+001	7.9940-003	5.8070-001
4	0.4900	0.0600	0.0000	-1.0000+001	0.0000
5	-2.1630+000	6.8620+000	7.4050+002	1.1950+000	-1.7150+002

G

	1	2	3	4	5
1	1.4320-002	-3.5530+002	-9.0960+001	-1.5490+001	2.2200+004
2	2.8710-001	7.2840+002	2.5140+001	-6.4870+001	8.1220+003
3	-2.4690-003	-1.0300+002	6.3330-001	-3.2130-001	-7.4180+001
4	1.0000+001	0.0000	0.0000	0.0000	0.0000
5	-1.3110-001	3.2950+002	-2.5000+001	6.2570+001	-6.4450+004

STATE FEEDBACK INFORMATION FOR STEP 1

A3/0/0K AUGMENTED LINEAR MODEL DESIGN :

SYSTEMS CONTROL, INC. (VT) •
TIME-DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

↑
CLOSED-LOOP-PIESYSTEM FOR GIVEN C-1
↑

CLOSED-LOOP POLE SHIFT AFTER GAIN
MATRIX SIMPLIFICATION - STEP 2

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-1.72626+002)+J(0.00000)	0.00000	1.00000	1 (-8.08747+001)+J(0.00000)	-.8087474	.00000
			2 (-3.08453+001)+J(0.00000)	-.3464532	.00000
			3 (-2.04250+003)+J(0.00000)	-.0020425	.00000
			4 (-6.78425+004)+J(0.00000)	-.0006784	.00000
			5 (1.00000+000)+J(0.00000)	1.0000000	.00000
(-1.21996+001)+J(6.71599+000)	1.39173+001	.87586	1 (1.00000+000)+J(0.00000)	1.0000000	.00000
			2 (-7.13601+002)+J(9.49699+002)	.1187920	126.92107
			3 (1.57867+002)+J(2.36803+002)	.0284434	-56.28781
			4 (-9.50639+002)+J(-1.49843+001)	.172856	122.42662
			5 (4.36604+002)+J(-1.12219+001)	.1204131	-68.74076
(-5.84776+000)+J(0.00000)	0.00000	1.00000	1 (-3.31401+001)+J(0.00000)	-.3314009	.00000
			2 (1.00000+000)+J(0.00000)	1.0000000	.00000
			3 (-1.27132+002)+J(0.00000)	.0127132	.00000
			4 (-3.88951+001)+J(0.00000)	-.3889510	.00000
			5 (1.06270+001)+J(0.00000)	.1062697	.00000
(-9.99991+000)+J(0.00000)	0.00000	1.00000	1 (2.56486+001)+J(0.00000)	.2564856	.00000
			2 (-1.41813+001)+J(0.00000)	-.1818128	.00000
			3 (5.87368+003)+J(0.00000)	.0058737	.00000
			4 (1.00000+000)+J(0.00000)	1.0000000	.00000
			5 (2.16772+002)+J(0.00000)	.0216772	.00000

A3/0/0K AUGMENTED LINEAR MODEL DESIGN II

↑
+ CLOSED LOOP EIGENSYSTEM FOR GIVEN C ↑
↑

SYSTEMS CONTROL, INC. (VT) •
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

AUGMENTED CLOSED-LOOP POLE
VALIDATION - N₁ - P MODE - STEP 3

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-1.72611+0n2)+J(0.00000)	0.00000	1.00000	1 (-8.08863-001)+J(0.00000) 2 (-3.46337-001)+J(0.00000) 3 (-2.04574-003)+J(0.00000) 4 (4.49323-003)+J(0.00000) 5 (1.00000+000)+J(0.00000) 6 (5.81761-005)+J(0.00000) 7 (2.09712-006)+J(0.00000) 8 (2.56798-009)+J(0.00000) 9 (-9.46864-009)+J(0.00000) 10 (4.66605-003)+J(0.00000)	-8088631 -3463372 -0020457 0044932 1.0000000 0000582 0000021 0000000 0000000 0046861	00000 00000 00000 00000 00000 00000 00000 00000 00000 00000
(-1.25608+0n1)+J(5.52150+0n0)	1.37244+0n1	.91550	1 (-5.59368-002)+J(4.91165-001) 2 (-9.91222-002)+J(-6.38267-002) 3 (1.42822-002)+J(8.98180-003) 4 (1.00000+000)+J(0.00000) 5 (7.55490-002)+J(2.46217-002) 6 (4.19165-004)+J(-1.20066-004) 7 (-1.57692-004)+J(2.45212-004) 8 (1.14486-007)+J(-1.64859-006) 9 (2.79654-006)+J(2.75991-006) 10 (1.81291-002)+J(-3.11240-002)	.4943402 .1298157 .0166717 1.0000000 .0794599 .0004360 .0002915 .0000002 .0000039 .0360169	96.49719 -139.77910 32.16501 00000 18.05096 -15.98380 122.74444 -55.22206 44.62230 -59.78006

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

A3/070K AUGMENTED LINEAR MODEL DESIGN II

(-6.45945+000)+J(3.48016+000)	7.33730+000	.88036	1 (1.97405+001)+J(5.07939+002)	.2036349	14.42966
			2 (-2.87211+002)+J(-1.61668+001)	.1641998	-100.07374
			3 (5.17292+003)+J(-5.22456+003)	.0073558	-45.31198
			4 (1.00000+000)+J(0.00000)	1.0000000	.00000
			5 (2.44232+002)+J(-3.34755+002)	.0414379	-53.89603
			6 (4.65442+005)+J(-3.08198+004)	.0003117	-81.41207
			7 (-1.44255+004)+J(5.76722+004)	.0005945	104.04317
			8 (-2.16556+007)+J(1.25604+008)	.0000002	176.68053
			9 (3.04264+006)+J(-1.23845+006)	.0000033	-21.62360
			10 (-2.04019+002)+J(-1.88554+002)	.0277806	-137.25587
(-1.13292+000)+J(1.10268+000)	1.58095+000	.71660	1 (5.75498+002)+J(-5.48412+002)	.0795100	-43.60951
			2 (9.82322+002)+J(-1.15644+001)	.1517335	-49.65417
			3 (4.56199+003)+J(4.08697+004)	.0045803	5.11932
			4 (1.00000+000)+J(0.00000)	1.0000000	.00000
			5 (2.93912+002)+J(-2.14103+003)	.0294891	-4.16640
			6 (-1.55216+003)+J(1.38413+003)	.0020797	138.27530
			7 (-1.51409+003)+J(-1.42449+003)	.0020789	-136.74637
			8 (-9.94089+007)+J(-8.50808+007)	.0000013	-138.44089
			9 (4.74438+006)+J(8.89679+006)	.0000101	-61.91032
			10 (-5.02896+002)+J(-5.40361+004)	.0502925	-179.38438
(-1.06051+000)+J(1.29624+001)	1.06840+000	.99261	1 (5.52843+002)+J(-1.15695+002)	.0564819	-11.81984
			2 (6.63134+002)+J(-1.11589+001)	.1298056	-59.27840
			3 (2.09852+003)+J(1.19283+003)	.0024138	28.61449
			4 (1.00000+000)+J(0.00000)	1.0000000	.00000
			5 (1.84244+002)+J(5.45759+004)	.0184325	1.69669
			6 (-6.55617+003)+J(5.23232+003)	.0100292	148.55310
			7 (-1.31052+002)+J(-1.32231+003)	.0131717	-17.23835
			8 (-6.77512+006)+J(-3.08045+006)	.0000074	-155.55008
			9 (-5.37255+007)+J(8.53373+006)	.0000086	-93.60240
			10 (-5.26765+002)+J(4.47081+003)	.0528659	175.14876

A3/0/0K AUGMENTED LINEAR MODEL DESIGN II
 SYSTEMS CONTROL, INC. (VT) -
 TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

(-1.01485-000)+J(0.00000) 0.00000	1.00000	1 (5.30551-002)+J(0.00000) -.0530551	.00000
			2 (2.30989-002)+J(0.00000) .0230989	.00000
			3 (-0.27556-004)+J(0.00000) -.0009276	.00000
			4 (1.00000+000)+J(0.00000) 1.0000000	.00000
			5 (1.57759-003)+J(0.00000) -.0015776	.00000
			6 (-3.40633-003)+J(0.00000) -.0034063	.00000
			7 (-8.44369-003)+J(0.00000) -.0084437	.00000
			8 (-3.01978-005)+J(0.00000) -.0000302	.00000
			9 (-2.74101-007)+J(0.00000) -.0000003	.00000
			10 (-5.22788-002)+J(0.00000) -.0522788	.00000

A3/0/0K AUGMENTED LINEAR MODEL DESIGN III

SYSTEMS CONTROL INC.(VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

↑
CLOSED LOOP EIGENSYSTEM FOR GIVEN C
↑

AUGMENTED CLOSED-LOOP POLE
VALIDATION - FTIT-Δ/P/P MODE - STEP 4

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-1.72786+002)+J(0.00000)	0.00000	1.00000	1 (-8.06548-001)+J(0.00000) 2 (-3.46337-001)+J(0.00000) 3 (-2.10616-003)+J(0.00000) 4 (-2.32999-002)+J(0.00000) 5 (1.00000+000)+J(0.00000) 6 (5.82512-005)+J(0.00000) 7 (2.15000-006)+J(0.00000) 8 (-2.55468-009)+J(0.00000) 9 (-1.27886-008)+J(0.00000) 10 (-5.76751-003)+J(0.00000)	-8055479 -3463371 -0021062 -0232999 1.0000000 -0000563 -0000022 -0000000 -0000000 -0057875	.00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000
(-1.23100+001)+J(7.54715+000)	1.44394+001	.85253	1 (1.00000+000)+J(0.00000) 2 (-1.78099-002)+J(-1.60857-001) 3 (1.19411-002)+J(-2.77603-002) 4 (-8.38698-001)+J(-1.61758-001) 5 (-1.88890-002)+J(-1.30226-001) 6 (-3.10509-004)+J(-8.21365-004) 7 (3.25920-004)+J(2.78248-004) 8 (-3.53030-007)+J(-2.44060-007) 9 (4.30624-006)+J(-4.69370-006) 10 (-5.82915-003)+J(7.00502-003)	1.0000000 1.618400 0.002380 8541542 1315883 0.0008781 0.004285 0.000004 0.000064 0.0091131	.00000 -96.31800 -66.74007 -169.08353 -81.74688 -110.70858 40.48647 145.34279 -47.47734 129.76514

(-9.00205+000)+J(0.00000)	0.00000	1.00000	1	(2.17168-001)+J(0.00000)	.2171676	.00000
			2	(-2.14366-001)+J(0.00000)	-.2143663	.00000
			3	(4.00274-003)+J(0.00000)	.0040027	.00000
			4	(1.00000+000)+J(0.00000)	1.0000000	.00000
			5	(1.16753-002)+J(0.00000)	.0116753	.00000
			6	(-2.16735-004)+J(0.00000)	-.0002167	.00000
			7	(5.70165-004)+J(0.00000)	.0005702	.00000
			8	(-1.62077-008)+J(0.00000)	.0000000	.00000
			9	(-1.22352-006)+J(0.00000)	.0000012	.00000
			10	(-1.29696-003)+J(0.00000)	-.0012470	.00000
(-3.27786+000)+J(1.81275+000)	3.74572+000	.87509	1	(1.45114-002)+J(1.17910-003)	.0145592	4.64526
			2	(7.57300-002)+J(-1.03797-001)	.1284469	-53.88567
			3	(6.37420-003)+J(-1.37022-003)	.0065198	-12.13184
			4	(1.00000+000)+J(0.00000)	1.0000000	.00000
			5	(3.80331-002)+J(-1.13817-002)	.0396496	-16.66027
			6	(5.56836-004)+J(4.16239-004)	.0006952	36.77842
			7	(-9.16838-004)+J(9.71271-005)	.0004240	173.96587
			8	(-3.49343-007)+J(1.43839-008)	.0000003	177.57114
			9	(6.13825-006)+J(2.19987-006)	.0000065	19.71698
			10	(-1.03560-002)+J(-2.25487-003)	.0105967	-167.71641
(-2.48649+001)+J(0.00000)	0.00000	1.00000	1	(1.00000+000)+J(0.00000)	1.0000000	.00000
			2	(5.49279-001)+J(0.00000)	.5492785	.00000
			3	(-2.45037-003)+J(0.00000)	-.0024504	.00000
			4	(8.18525-001)+J(0.00000)	.8185252	.00000
			5	(6.45945-003)+J(0.00000)	.0064595	.00000
			6	(3.05817-002)+J(0.00000)	.0305817	.00000
			7	(2.45562-003)+J(0.00000)	.0024558	.00000
			8	(1.19099-005)+J(0.00000)	.0001119	.00000
			9	(-7.73748-005)+J(0.00000)	-.0000774	.00000
			10	(-2.59782-002)+J(0.00000)	-.0259782	.00000

83/0/04 AUGMENTED LINEAR MODEL DESIGN III

SYSTEMS CONTROL, INC. (VT)

TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

(-8.26560-001)+J(0.00000)	0.00000	1.00000	1	(2.65166-001)+J(0.00000)	.2651665	.00000
				2	(-5.11213-001)+J(0.00000)	-.5112134	.00000
				3	(2.71872-003)+J(0.00000)	.0027187	.00000
				4	(1.00000+000)+J(0.00000)	1.0000000	.00000
				5	(9.94159-003)+J(0.00000)	.0094159	.00000
				6	(7.96285-003)+J(0.00000)	.0079629	.00000
				7	(-5.73734-002)+J(0.00000)	-.0573734	.00000
				8	(-7.35510-006)+J(0.00000)	-.0000073	.00000
				9	(1.17698-005)+J(0.00000)	.0000118	.00000
				10	(-1.20277-002)+J(0.00000)	-.0120277	.00000

(-1.01106-000)+J(1.70928-002)	1.01120+000	.99986	1	(-1.04750-004)+J(4.87949-004)	.0004991	102.11608
			2	(2.98314-003)+J(-2.11012-002)	.0213110	-81.95326
			3	(1.34802-003)+J(1.69724-004)	.0014083	6.92201
			4	(1.00000+000)+J(0.00000	1.0000000	.00000
			5	(1.50410-002)+J(-4.85578-004)	.0150489	-1.84907
			6	(-1.16108-002)+J(1.18285-003)	.0118699	174.28094
			7	(-1.94902-002)+J(-1.61138-004)	.0194908	-179.52631
			8	(-7.83018-006)+J(-1.34995-006)	.0000079	-170.21818
			9	(-3.54463-006)+J(1.49467-006)	.0000038	157.13622
			10	(-1.48804-002)+J(2.28702-004)	.0148822	176.11947

CLOSED LOOP EIGENSYSTEM FOR GIVEN C

AUGMENTED CLOSED-LOOP POLE VALIDATION -
P_B - Δp/p MODE - STEP 5

EIGENVALUE	NATURAL FREQUENCY	DAMPING FACTOR	EIGENVECTOR	MAGNITUDE	PHASE (DEG)
(-1.72625+0.021j)+j(0.00000)	0.00000	1.00000	1 (-8.08776-0.011)+j(0.00000)	.8087756	.00000
			2 (-3.46468-0.011)+j(0.00000)	.3464678	.00000
			3 (-2.04081-0.03)+j(0.00000)	.0020408	.00000
			4 (-1.14958-0.03)+j(0.00000)	.0011496	.00000
			5 (1.00000+0.00)+j(0.00000)	1.0000000	.00000
			6 (5.84124+0.05)+j(0.00000)	.0000584	.00000
			7 (2.10959+0.06)+j(0.00000)	.0000021	.00000
			8 (-2.56909-0.09)+j(0.00000)	.0000000	.00000
			9 (-1.00485-0.08)+j(0.00000)	.0000000	.00000
			10 (-1.68607-0.04)+j(0.00000)	.0001686	.00000
(-2.07283+0.011j)+j(0.00000)	0.00000	1.00000	1 (-1.30467-0.011)+j(0.00000)	.1304667	.00000
			2 (-1.72389-0.02)+j(0.00000)	.0172389	.00000
			3 (-4.63538-0.04)+j(0.00000)	.0004635	.00000
			4 (1.00000+0.00)+j(0.00000)	1.0000000	.00000
			5 (-8.75021-0.03)+j(0.00000)	.0087502	.00000
			6 (8.12274+0.05)+j(0.00000)	.0000812	.00000
			7 (-2.82815-0.05)+j(0.00000)	.0000283	.00000
			8 (4.02259-0.08)+j(0.00000)	.0000000	.00000
			9 (2.63673-0.07)+j(0.00000)	.0000003	.00000
			10 (2.38631-0.02)+j(0.00000)	.0238631	.00000

(-1.2728+001)+J(6.80243+000)	1.38190+001	.87044	1 (1.00000+000)+J(0.00000)	1.00000000	.00000
			2 (-6.44531-002)+J(1.26894-001)	.1423242	116.92739
			3 (-1.41561-002)+J(-2.67886-002)	.0302989	-62.14643
			4 (-2.10800-001)+J(-3.25191-001)	.3875382	-122.95289
			5 (3.3361-002)+J(-1.29050-001)	.1332865	-75.51607
			6 (-3.28964-004)+J(-8.11205-004)	.0008754	-112.07380
			7 (3.67402-004)+J(3.28957-004)	.0004932	41.84003
			8 (-3.75461-007)+J(-2.23623-007)	.0000004	-149.22211
			9 (-4.76792-006)+J(-4.61357-006)	.0000066	-44.05740
			10 (-6.86859-003)+J(-1.22501-003)	.0069770	-169.88763
(-9.44478+000)+J(0.00000)	0.00000	1.00000	1 (2.19512-001)+J(0.00000)	.2195118	.00000
			2 (-1.93992-001)+J(0.00000)	-.1939922	.00000
			3 (-4.74705-003)+J(-0.00000)	.0047471	.00000
			4 (1.00000+000)+J(0.00000)	1.0000000	.00000
			5 (1.61966-002)+J(0.00000)	.0161966	.00000
			6 (-1.87359-004)+J(-0.00000)	-.0001874	.00000
			7 (4.90507-004)+J(0.00000)	.0004905	.00000
			8 (-3.37896-008)+J(0.00000)	-.0000000	.00000
			9 (-1.41825-006)+J(-0.00000)	.0000014	.00000
			10 (-8.35491-004)+J(0.00000)	-.0008355	.00000
(-6.27436+000)+J(0.00000)	0.00000	1.00000	1 (-4.67134-001)+J(0.00000)	-.4671343	.00000
			2 (1.00000+000)+J(0.00000)	1.0000000	.00000
			3 (-1.60337-002)+J(-0.00000)	-.0160337	.00000
			4 (-1.26203-001)+J(0.00000)	-.1262035	.00000
			5 (1.27887-001)+J(0.00000)	.1278873	.00000
			6 (-2.11600-003)+J(-0.00000)	-.0021160	.00000
			7 (-4.16364-003)+J(0.00000)	-.0041636	.00000
			8 (-7.11455-007)+J(0.00000)	-.0000007	.00000
			9 (-1.04659-005)+J(-0.00000)	-.0000105	.00000
			10 (-4.09400-004)+J(0.00000)	-.0004094	.00000

SYSTEMS CONTROL, INC. (VT) -
TIME DOMAIN SYNTHESIS AND ANALYSIS PROGRAM

A3/0/0M AUGMENTED LINEAR MODEL DESIGN IV

(-3.68689-001)+J(0.00000)	0.00000	1.00000	1	(1.00000+000)+J(0.00000)	1.00000000	.00000
				2	(3.87287-001)+J(0.00000)	.3872870	.00000
				3	(-4.72102-003)+J(0.00000)	-.0047210	.00000
				4	(7.49082-002)+J(0.00000)	.0749082	.00000
				5	(-1.25165-002)+J(0.00000)	-.0125165	.00000
				6	(-3.47359-002)+J(0.00000)	-.0347359	.00000
				7	(-1.74672-003)+J(0.00000)	-.0017467	.00000
				8	(1.25439-005)+J(0.00000)	.0000125	.00000
				9	(-6.45110-005)+J(0.00000)	-.0000645	.00000
				10	(-1.71461-002)+J(0.00000)	-.0171461	.00000
(-7.60030-001)+J(0.00000)	0.00000	1.00000	1	(-8.06004-001)+J(0.00000)	-.8060038	.00000
				2	(1.00000+000)+J(0.00000)	1.0000000	.00000
				3	(1.29820-003)+J(0.00000)	.0012982	.00000
				4	(-7.72137-002)+J(0.00000)	-.0772137	.00000
				5	(2.64978-002)+J(0.00000)	.0264978	.00000
				6	(-4.19396-002)+J(0.00000)	-.0419396	.00000
				7	(9.27290-002)+J(0.00000)	.0927290	.00000
				8	(4.59506-006)+J(0.00000)	.0000046	.00000
				9	(-5.67254-006)+J(0.00000)	-.0000057	.00000
				10	(-2.04336-003)+J(0.00000)	-.0020434	.00000
(-1.34306+000)+J(0.00000)	0.00000	1.00000	1	(3.42753-001)+J(0.00000)	.3427528	.00000
				2	(1.00000+000)+J(0.00000)	1.0000000	.00000
				3	(-2.56769-002)+J(0.00000)	-.0256769	.00000
				4	(1.01292-001)+J(0.00000)	.1012922	.00000
				5	(-8.00102-002)+J(0.00000)	-.0800102	.00000
				6	(-6.87595-002)+J(0.00000)	-.0687595	.00000
				7	(-3.04246-002)+J(0.00000)	-.0304246	.00000
				8	(1.96214-005)+J(0.00000)	.0000196	.00000
				9	(-1.19884-004)+J(0.00000)	-.0001199	.00000
				10	(-2.84951-002)+J(0.00000)	-.0284951	.00000

SYSTEMS CONTROL, INC. (VT)
 ---TIME-DOMAIN SYNTHESIS AND ANALYSIS PROGRAM---

AS/7/14 AUGMENTED LINEAR MODEL DESIGN IV

(-2.912-3-001)+J(0.0000)	0.0000	1.0000	1 (1.0000+000)+J(0.0000)	1.000000	.0000
			2 (-1.5795-001)+J(0.0000)	-.157952	.0000
			3 (4.93637-002)+J(0.0000)	.3493637	.0000
			4 (7.34081-002)+J(0.0000)	.0734081	.0000
			5 (7.21565-001)+J(0.0000)	.7215648	.0000
			6 (-1.98719-001)+J(0.0000)	-.1987189	.0000
			7 (-4.11712-001)+J(0.0000)	-.4117118	.0000
			8 (1.07725-003)+J(0.0000)	.0010772	.0000
			9 (2.77623-005)+J(0.0000)	.0000278	.0000
			10 (1.36732-003)+J(0.0000)	.0013673	.0000

•FIN

APPENDIX H

TRANSITION CONTROL DATA

The development of the transition control is discussed in detail in Section 4.5 (Volume I). The fifth order design models were used to calculate the numerical quantities used for the transition control design. This data is presented in this section. A critical step in the design is the partition of the dynamical state equations to determine the primary set, δx_1 and the secondary set δx_2 . Since the RCVV's, CIVV's, and bleeds have only a small range of motion, these controls were not used during large accelerations in the explicit transition algorithm. Fuel flow and jet area were the two controls used for the acceleration control. The fuel flow is the primary acceleration regulating variable. Jet area has a strong effect on engine response, even though its excursions are limited, essentially, to increases about the steady-state values. Thus, the physical character of the F100 behavior was the determining factor in the choice of modulated controls.

The primary state rates chosen were the fan speed and compressor speed. These were used because the continuous state asymptotic expansion will provide continuous reference trajectories for these values which is close to being physically realizable. Also, the effects of the two controls on the speeds were independent as required by an invertible G_1 matrix. This fact is directly calculated from the equation, or physically justified by realizing that fuel affects the rotor speeds collectively while nozzle area affects the speed differentially.

The definitions of the partitions of the fifth order design models are given in Table H.1. The specific values

Table H.1
Variable Index

$$\begin{bmatrix} \delta \dot{x}_1 \\ \delta \dot{x}_2 \end{bmatrix} = \underbrace{\begin{bmatrix} F_{11} & F_{12} \\ F_{21} & F_{22} \end{bmatrix}}_F \begin{bmatrix} \delta x_1 \\ \delta x_2 \end{bmatrix} + \underbrace{\begin{bmatrix} G_1 \\ G_2 \end{bmatrix}}_G \delta u$$

$$\delta y = \underbrace{[H_1 \quad H_2]}_{HY} \begin{bmatrix} \delta x_1 \\ \delta x_2 \end{bmatrix} + \underbrace{D_1}_{DY} \delta u$$

ELEMENT	UNITS	ELEMENT	UNITS
δx_1		δu	
Low Rotor Speed	RPM	Fuel Flow Command	lbm/hr
High Rotor Speed	RPM	Nozzle Area	ft ²
δx_2		δy	
Augmentor Pressure	psia	Thrust	lbf
Fuel Flow	lbm/hr	Airflow	lbm/sec
Burner Pressure	psia	Turbine Temperature	°R
		Fan Stability Margin	---
		Compressor Stability Margin	---
		$\Delta p/p^*$	---
		$(\Delta p/p)^*_{avg}$	---

* Not included in some models

used in the design of the rate schedules are discussed in Section 5.9.2 and listed in Table 5.9 (Volume I). The formulas for the design of the rates are derived in Section 4.5 and the formulas for data provided in the printout are shown in Table H.2.

The data is presented for the equations specified in Table H.2 for the conditions used to derive the transient rates for the controller presented in Table 5.9. Eleven cases are presented as reference data and these cases are indexed in Table H.3.

A diagram of the rate limited structure of the transition model is shown in Figure H.1. For various size inputs, the normalized output is shown in Figure H.2. It is obvious that for small inputs, the response is determined by the regulator/trim control. For large transients, the transition control has authority until the steady-state condition is approached. The structure used is always globally state and does not use switching or other undesirable high gain nonlinearities which can degrade overall stability.

Table H.2
Matrix Index

Intermediate Matrices:

$$\bar{F}_1 = F_{21} - G_2 G_1^{-1} F_{11}$$

$$\bar{F}_2 = F_{22} - G_2 G_1^{-1} F_{12}$$

State Rate Computability Matrix:

$$M = \bar{F}_2^{-1} \bar{F}_1$$

State Initial Jump Matrix:*

$$\delta x_2(0) = \underline{-\bar{F}_2^{-1} [M + G_2 G_1^{-1}]} \alpha_1$$

Control Initial Jump Matrix:*

$$\delta u(0) = \underline{G_1^{-1} [I + F_{12} \bar{F}_2^{-1} (M + G_2 G_1^{-1})]} \alpha_1$$

Control Rate Matrix:*

$$r_u = \underline{-G_1^{-1} [F_{11} - F_{12} M]} \alpha_1$$

Output Jump Matrix:

$$P = -H_2 \bar{F}_2^{-1} [M + G_2 G_1^{-1}] + D G_1^{-1}$$

Output Rate Matrix:

$$Q = H_1 - D G_1^{-1} F_{11} + (H_2 + D G_1^{-1} F_{12}) M$$

*Matrix included in data is underlined

Table H.3
Index of Transition Data

CASE	POWER LEVER ANGLE (DEG)	ALTITUDE (FT)	MACH NO.	PAGE
1	83	0	0	429
2	67	0	0	433
3	52	0	0	438
4	36	0	0	443
5	24	0	0	448
6	20	0	0	453
7	83	0	1.2	458
8	83	30,000	0.9	463
9	20	30,000	0.9	468
10	83	45,000	0.9	472
11	40	45,000	0.9	476

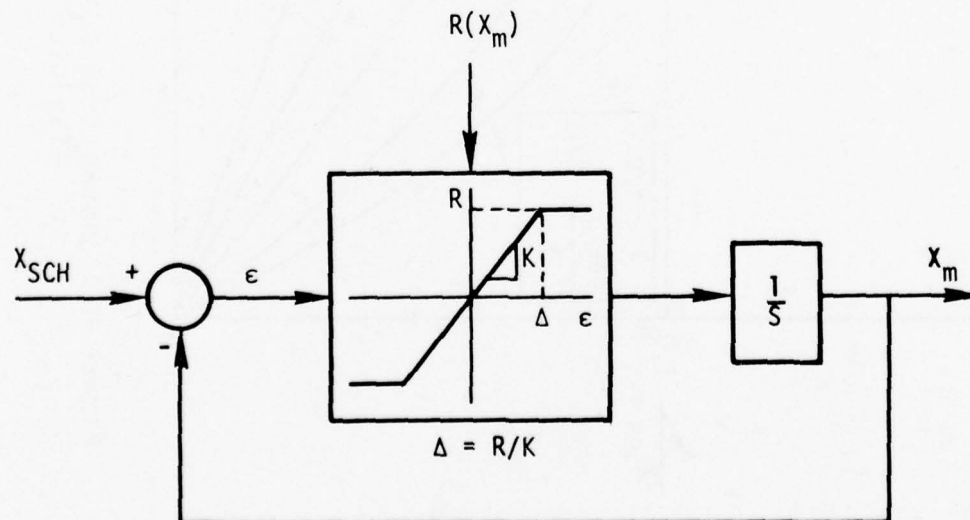


Figure H.1 Basic Structure of Transition Control Logic

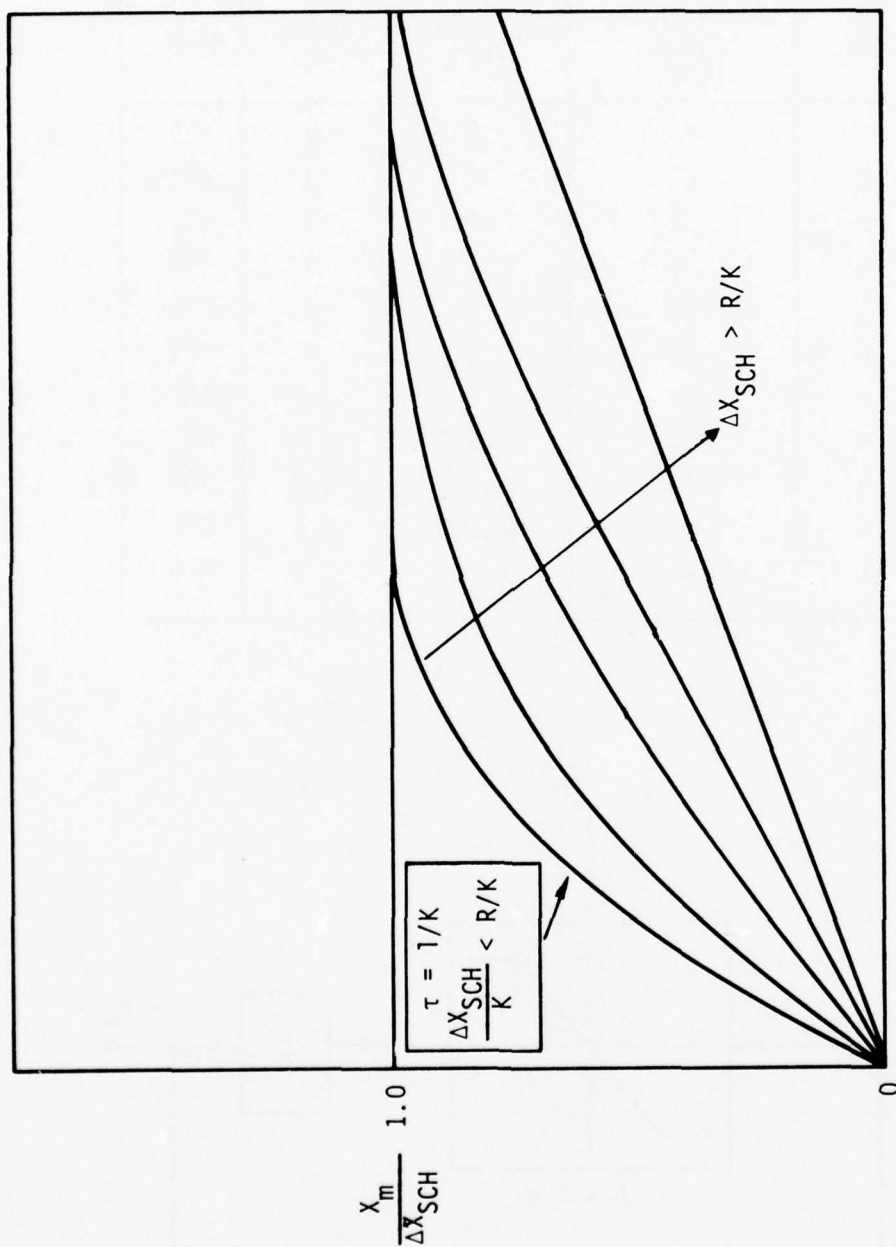


Figure H.2 Normalized Response of Transition Control to Steps in Scheduled Input X_{SCH} ($X_m(0) = 0$)

REDUCED MATRICES					FIFTH ORDER				
F	1	2	3	4	5	6	7	8	9
1	-3.245+01	-2.152+01	-0.155+03	-5.731+00	-1.342+03				
2	-1.622+01	-0.241+01	-0.241+03	-1.847+00	-5.705+02				
3	-1.456+01	-0.253+01	-0.100+03	-7.994+02	-5.807+00				
4	0.000	0.000	0.000	-1.100+02	0.000				
5	-2.163+01	-0.852+01	-7.405+03	-1.145+01	-0.1715+03				
REDUCED MATRICES					FIFTH ORDER				
G	1	2	3	4	5	6	7	8	9
1	-1.332+01	-1.353+03	-0.904+02	-1.549+02	-2.220+05				
2	-2.71+01	-7.246+03	-2.510+02	-0.647+02	-0.122+04				
3	-2.900+02	-1.130+03	-0.133+00	-0.213+00	-0.741+02				
4	-1.000+02	0.000	0.000	0.000	0.000				
5	-1.111+00	-3.305+03	-2.500+02	-0.257+02	-0.6445+05				
REDUCED MATRICES					FIFTH ORDER				
H	1	2	3	4	5	6	7	8	9
1	-1.622+01	-0.172+01	-7.994+02	-1.140+00	-0.3771+02				
2	-1.622+01	-0.172+01	-7.994+02	-1.140+00	-0.3771+02				
3	-1.622+01	-0.172+01	-7.994+02	-1.140+00	-0.3771+02				
4	-1.622+01	-0.172+01	-7.994+02	-1.140+00	-0.3771+02				
5	-1.622+01	-0.172+01	-7.994+02	-1.140+00	-0.3771+02				
6	-1.622+01	-0.172+01	-7.994+02	-1.140+00	-0.3771+02				
7	-1.622+01	-0.172+01	-7.994+02	-1.140+00	-0.3771+02				
8	-1.622+01	-0.172+01	-7.994+02	-1.140+00	-0.3771+02				
9	-1.622+01	-0.172+01	-7.994+02	-1.140+00	-0.3771+02				

F11

1	2
-3.245+00	-2.152+00
1.6420+00	-5.0410+00

F12

1	2	3
-2.155+00	5.731+00	1.342+00
-2.155+00	1.342+00	5.705+00

F21

1	2
1.456+00	-2.550+00
0.000	0.000
-2.155+00	6.8620+00

F22

1	2	3
-1.000+00	7.994+03	5.807+00
0.000	-1.000+00	0.000
7.994+00	1.145+00	-1.715+00

G1									
	1	1	1.3370-002	-1.5510+002					
	2	2	2.8710-001	7.2880+002					
G2									
	1	1	-2.8690-003	-1.6300+002					
	2	2	1.0000+001	0.0000					
	3	3	-1.3110-001	3.2950+002					
H1									
	1	1	1.6620+000	-1.7680+000					
	2	2	1.3810-002	3.1420+000					
	3	3	1.5800-001	-1.1290-001					
	4	4	7.4000-005	3.2600+006					
	5	5	-4.8590-005	1.3810+004					
	6	6	5.1770-005	-3.9090-005					
	7	7	1.5700-005	2.2070+006					
H2									
	1	1	7.0990+001	-1.8980-001	3	3.7710+001			
	2	2	-1.0000-002	1.2900+004		-1.8390-007			
	3	3	-4.9590+000	7.1640-002		-1.8350-001			
	4	4	-1.9770-002	2.2580-006		2.3150+005			
	5	5	1.1400-002	1.9510+005		-2.6880+003			
	6	6	-1.2300-002	-1.2280+005		2.0790+004			
	7	7	-3.2940-003	-2.6480+006		9.9150+008			
G1									
	1	1	1.3020-001	1.0920+002					
	2	2	1.4390-007	3.1950+001					
	3	3	2.8670-002	7.9270+001					
	4	4	1.0460-006	-7.7200+003					
	5	5	-2.3350-008	-7.8970+005					
	6	6	5.7270-006	8.4680+003					
	7	7	1.2440-006	2.1680+003					

3/10/76

M3 0/0K

CONSTANT VELOCITY CONTROLLER

	1	2	3
1	2.1020+002	-1.2450+001	-3.1573+001
2	6.8222+004	-5.8131+001	-1.0404+004
3	-8.1231+002	2.2300+000	7.6651+001

	1	2
1	4.5272+001	3.0320+001
2	1.5219+002	5.2757+002
3	-7.0385+000	1.0013+000

STATE RATE COMP. MATRIX		
	1	2
1	-3.6657+002	5.0380+002
2	-5.0370+000	9.0003+000
3	-1.9742+001	3.1072+001

STATE INITIAL JUMP MATRIX		
	1	2
1	-7.0235+003	1.0025+002
2	-1.0424+000	2.5315+000
3	-1.3710+002	5.0058+002

CONTROL INITIAL JUMP MATRIX		
	1	2
1	5.0700+000	3.1500+000
2	-2.5530+003	1.2730+000

CONTROL DATA MATRIX		
	1	2
1	-5.0370+000	9.0003+000
2	2.3089+003	-2.2950+003

OUTPUT DATA MATRIX		
	1	2
1	-7.0580+000	1.2000+001
2	1.0300+002	-2.0200+000
3	5.2100+002	3.0057+001
4	5.7300+000	-4.7300+000
5	-9.0002+000	5.3503+000
6	5.1000+000	-4.0101+004
7	1.0000+000	-1.0053+000

CONSTANT VELOCITY CONTROLLER 83 0/OK 3/10/76

	OUTPUT JUMP VECTOR	
	1	2
1	-1.3009+000	2.8140+000
2	-9.2590-004	2.4371-004
3	-4.6159-002	2.8311-001
4	1.2439-004	-1.3765-004
5	-3.4034-005	-1.0210-005
6	1.0711-004	-1.2390-004
7	2.7501-005	-3.0839-005

```

XGT  ADS
F
REDUCED MATRICES 0/OK 67 FIFTH ORDER
-.4178+01 -.1415+01 -.8026+03 .5835+00 .1364+03
-.3057+01 -.5648+01 -.9944+02 .5930+00 .6073+02
-.2978+01 -.3524+01 -.4803+01 -.1095+01 .9307+00
.0000 .0000 .0000 -.1000+02 .0000
.3883+00 .6683+01 .2732+03 .2003+01 -.1718+03
G
REDUCED MATRICES 0/OK 67 FIFTH ORDER
-.1611+00 .5493+02 -.1223+03 -.1330+01 .2072+05
-.1625+00 .7967+03 -.1470+02 -.7235+02 .9983+04
-.3299+02 -.6043+02 .8846+00 .1458+00 .4412+03
.1000+02 .8102+14 .3775+16 -.418+16 -.1649+13
-.2975+00 -.8463+03 .3263+02 .3052+02 -.6094+05
H
REDUCED MATRICES 0/OK 67 FIFTH ORDER
.1010+01 -.1433+01 .1859+03 .1052+00 .3407+02
.2580+01 .4177+03 -.1876+00 .5482+04 -.4457+04
.3395+01 -.1017+00 -.2178+01 .1703+00 .3455+00
.1081+03 .5083+04 -.1382+01 .1079+05 .4773+05
.4987+04 .3707+03 .1642+02 .3941+04 .3791+02
I
REDUCED MATRICES 0/OK 67 FIFTH ORDER
-.1407+00 .1346+03 .3129+02 -.6397+01 .7577+04
.4621+04 .1647+01 .9497+00 .6715+03 .6643+00
.7142+02 .5123+02 -.5180+00 .4989+00 .1263+04

```

-3422-05 -.2798-01 -.5638-02 .1323-03 -.2552-01
 -.1718-04 -.4152-01 .2144-03 -.3392-02 -.4376+00

F11

	1	2
1	-4.1780+000	-1.4150+000
2	-3.0570-002	-5.6480+000

F12

	1	2	3
1	-8.0260+002	5.8350-001	1.3640+002
2	-9.9440+001	5.9300-001	6.0730+001

F21

	1	2
1	-2.9780-002	-3.5240-002
2	0.0000	0.0000
3	3.8830-001	6.6830+000

F22

	1	2	3
1	-4.8030+000	-1.0950-002	9.3070-001
2	0.0000	-1.0000+001	0.0000
3	2.7320+002	2.0030+000	-1.7180+002

G1

	1	2
1	-1.6110-001	5.4930+001
2	-1.6250-001	7.9670+002

G2

	1	2
1	-3.2900-003	-6.0430+001
2	1.0000+001	8.1020-015
3	-2.9750-001	-8.4630+002

H1

	1	2
1	1.0100+000	-1.4330+000
2	2.5800-002	4.1770-004
3	3.3950-002	-1.0170-001
4	-1.0810-004	3.0830-005
5	-4.9870-005	3.7070-004

H2

	1	2	3
1	1.8500+002	-1.0520-001	3.4070+001
2	-1.8760-001	5.4820-005	-4.4570-005
3	-2.1780+000	1.7030-001	-3.4550-001

4	-1.3820-002	1.0780-004	-4.7730-006
5	1.4420-003	3.0410-002	-3.7910-003

D1

1	-1.4070-001	1.3860+002
2	-4.6210-005	-1.6470+000
3	-7.1420-003	5.1230+001
4	-3.4220-006	-2.7980-002
5	-1.7180-005	-4.1520-002

CONSTANT VELOCITY CONTROLLER 67 PLA FEB. 13.1976

F2

	1	2	3
1	7.0500+001	-2.2531-002	-8.2443+000
2	5.3086+004	2.6109+001	8.8203+003
3	2.6532+003	9.3113-001	-5.2195+002

F1

	1	2
1	4.6274-001	-3.5674-001
2	-2.7859+002	-6.8420+001
3	1.3453+001	-3.4999+000

STATE RATE COMP. MATRIX

	1	2
1	-9.5864-003	1.9692-002
2	-6.2504-001	3.8545+000
3	-2.4256-002	1.1483-001

STATE INITIAL JUMP MATRIX

	1	2
1	-2.4648-003	4.7275-003
2	-1.7262-001	1.4547+000
3	-6.8295-003	2.4048-002

CONTROL INITIAL JUMP MATRIX

	1	2
1	-6.4713+000	4.5996-001
2	-1.3607-003	1.3490-003

CONTROL RATE MATRIX

	1	2
1	-6.2504-001	3.8545+000
2	1.0285-003	-1.2887-003

OUTPUT RATE MATRIX

	1	2
1	-1.4338+000	5.8245+000
2	2.5900-002	-1.1260-003
3	1.3922-002	3.7862-001
4	2.1339-004	-2.1484-004
5	-3.0257-005	1.0691-004

CONSTANT VELOCITY CONTROLLER 67 PLA FEB. 13, 1976

	1	2
1	4.1002-002	1.9735+000
2	3.0026-003	-3.0513-003
3	-4.3732-002	2.8495-001
4	9.4812-005	-1.0320-000
5	1.8615-004	-8.9987-005

52/OK/0

```

1.  CONSTANT VELOCITY CONTROLLER 52 PLA 2/13/76
2.  SMOOTH NX=5, NY=5, NIND=2, REORD=TRUE. SEND
3.
4.  F 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27
5.  REDUCED MATRICES 0/OK 52 FIFTH ORDER
6.  --.4255+01 --.1230+01 --.5354+03 --.3101+00 .1575+03
7.  --.1048+01 --.3382+01 --.3261+02 .7345+00 .5158+02
8.  .1418-01 --.2113-01 --.6141+01 --.2547-03 .6924+00
9.  .0000 .0000 .0000 --.1000+02 .0000
10. .2091+01 .5079+01 --.9684+02 .3299+01 --.1780+03
11.  G REDUCED MATRICES 0/OK 52 FIFTH ORDER
12.  --.2134+00 .1368+04 --.9307+02 .3127+02 .3656+05
13.  --.3165+00 .7179+03 --.2441+02 --.3510+02 .8093+04
14.  --.9446-03 --.5519+02 .3213+00 .9251-03 .1351+03
15.  .1000+02 .0000 .0000 .0000 .0000
16. --.4822+00 --.2391+04 .5389+02 --.2716+02 --.6576+05
17.  HY REDUCED MATRICES 0/OK 52 FIFTH ORDER
18.  .6121+00 --.9525+00 .2669+03 --.2250+00 .3358+02
19.  .3037-01 .2250-02 --.8275+00 .1511-02 .1851-01
20. --.3804-01 --.1129+00 --.4708+01 .2276+00 --.2849+00
21. .1864-03 .5936-04 --.2176-01 .4426+04 --.4862-03
22. .6493-05 .4400-03 --.3186-02 .7207-04 --.4474-02
23.  DY REDUCED MATRICES 0/OK 52 FIFTH ORDER
24.  --.3975-01 .4417+03 .1378+02 .6186+01 .9332+04
25.  --.4410-03 --.2504+01 .7371+00 --.1712-01 --.1358+02
26.  --.3118-02 .2186+02 --.1793+01 .2361+00 .6608+03
27.  --.1159-04 .2834-01 .2874+03 --.4779-03 .3744+00
28.  --.4349-04 --.6229-01 .1560-02 --.7764-02 --.3150+00

```

F11	1	-4.2560+000	-1.2300+000	
	2	-1.0480+000	-3.3820+000	
F12	1	-5.3550+002	-3.1010+001	1.5750+002
	2	-3.2610+001	-7.3450+001	5.1580+001
F21	1	1.4180+002	-2.1130+002	
	2	0.0000	0.0000	
	3	2.0910+000	5.0790+000	
F22	1	-6.1410+000	-2.5470+000	6.9240+001
	2	0.0000	-1.0000+001	0.0000
	3	-0.6840+001	3.2990+000	-1.7800+002
G1	1	-2.1340+001	1.3680+003	
	2	-3.1660+001	7.1790+002	
G2	1	-0.4460+004	-5.5190+001	
	2	1.0000+001	0.0000	
	3	-4.8220+001	-2.3910+003	
H1	1	6.1210+001	-9.5250+001	
	2	3.0370+002	2.2600+002	
	3	-3.8000+002	-1.1290+001	
	4	1.8640+004	5.0360+005	
	5	6.4930+006	4.4000+004	
H2	1	2.4680+002	-2.2500+001	3.3580+001
	2	-4.2750+001	1.5110+003	-1.8510+002
	3	-4.7080+000	2.2760+001	-2.8490+00.

4	-2.170-002	4.4260-005	-4.8620-004
5	-3.160-003	7.2070-005	-4.4740-003

01

		1	2
1	-3.9750-002	4.4170+002	
2	-4.4100-004	-2.5940+000	
3	-3.1180-003	2.1860+001	
4	-1.1580-005	-2.4340-002	
5	-4.3490-005	-6.2290-002	

P2

	1	2	3
1	-3.9337+001	-5.4660-002	8.4974+000
2	1.2138+004	3.3851+001	-1.5186+003
3	-2.0706+003	-9.9302-001	2.2715+002

F1

	1	2
1	-2.1298-001	5.7023-002
2	5.7937+001	-1.3374+002
3	-1.0302+001	1.4367+001

STATE RATE COMP. MATRIX

	1	2
1	-4.4695-003	1.3631-002
2	1.2192-001	2.2394+000
3	5.1451-003	7.0795-002

STATE INITIAL JUMP MATRIX

	1	2
1	-2.3416-003	3.6693-003
2	-1.1524-001	1.0948+000
3	-4.0758-003	2.0164-002

CONTROL INITIAL JUMP MATRIX

	1	2
1	2.5648+000	-4.8873+000
2	1.1311-003	-7.6239-004

CONTROL RATE MATRIX

	1	2
1	1.2192-001	2.2394+000
2	8.1615-004	-1.0660-003

OUTPUT RATE MATRIX

	1	2
1	-7.9824-002	4.0017+000
2	3.1987-002	-5.1838-003
3	2.6746-002	2.8230-001
4	2.6201-004	-1.6806-004
5	-4.9640-005	2.0987-004

CONSTANT VELOCITY CONTROLLER 52 PLA 2/13/76

OUTPUT JUMP VECTOR	
	¹
1	-3.5169-001
2	-2.2187-001
3	2.7999-003
4	-1.3752-005
5	-1.6292-004

	²
	1.2667+000
	2.3837-003
	2.2565-001
	3.7236-005
	2.3733-004

36/OK/0

1.	CONSTANT VELOCITY CONTROLLER 36 PLA 2/13/76									
2.	SOPTION NXS5, NY5, NUS, NIND2, REORD=TRUE, SEND									
3.	1	2	5	3	4					
4.	F					REDUCED MATRICES 0/OK 36 FIFTH ORDER				
5.										
6.										
7.										
8.										
9.										
10.	G					REDUCED MATRICES 0/OK 36 FIFTH ORDER				
11.										
12.										
13.										
14.										
15.										
16.	MY					REDUCED MATRICES 0/OK 36 FIFTH ORDER				
17.										
18.										
19.										
20.										
21.										
22.	DY					REDUCED MATRICES 0/OK 36 FIFTH ORDER				
23.										
24.										
25.										
26.										
27.										

F11	1	-3.9810+000	-1.3540+000
	2	-8.1440-001	-2.5800+000
F12	1	-4.5640+002	1.8170-001
	2	-2.3020+002	1.6120+000
	3		4.1890+001
F21	1	1.4440-002	-2.9000-002
	2	0.0000	0.0000
	3	1.7140+000	5.2520+000
F22	1	-5.9050+000	-4.8700-001
	2	0.0000	-1.0000+001
	3	1.1740+002	2.3160+000
	3		-1.6850+002
G1	1	-4.6340-001	1.1340+003
	2	-3.7360-001	-3.4270+002
G2	1	-8.4090-003	-3.4810+001
	2	1.0000+001	0.0000
	3	-3.6440-001	-3.9930+002
H1	1	5.7830-001	-8.1240-001
	2	3.1020-002	3.1390-003
	3	-2.7710-002	-1.2620-001
	4	4.4540-005	5.4940-005
	5	1.0970-005	5.8810-004
H2	1	2.4370+002	1.1100-001
	2	-8.8770-001	3.1290-004
	3	2.3410+000	3.0690-001
	3		2.6630+001
			-3.3120-003
			-6.3350-001

4	-1.5450-002	1.8190-004	-5.1070-005
5	-2.0880-003	8.2200-005	-6.0870-003

01

	1	2
1	-1.6070-001	1.5380-001
2	-7.5740-004	7.8410-001
3	-4.1870-002	2.7950-001
4	-1.3070-005	1.7110-002
5	-3.1210-005	-2.4970-002

F2

		¹	²	³
1	-3.6968+000	-7.2746-002	1.6138+000	
2	-7.1642+003	2.2453+001	1.6669+003	
3	1.1519+002	6.6747-001	-2.0549+002	

F1

	¹	²
1	-1.8825-002	6.1156-002
2	-3.0246+001	-5.8196+001
3	2.3848+000	7.8455+000

STATE RATE COMP. MATRIX

	¹	²
1	-4.0871-003	1.1483-002
2	6.3025-002	1.6377+000
3	5.1436-003	6.2233-002

STATE INITIAL JUMP MATRIX

	¹	²
1	-2.4440-003	6.7548-002
2	-1.6378-001	5.8430-001
3	-4.7535-003	7.6964-001

CONTROL INITIAL JUMP MATRIX

	¹	²
1	-5.8836-001	-1.9469+000
2	6.2141-004	-7.9558-004

CONTROL RATE MATRIX

	¹	²
1	6.3025-002	1.6377+000
2	1.2243-003	-1.7166-001

OUTPUT RATE MATRIX

	¹	²
1	-2.8394-001	3.5547+000
2	1.5563-002	-9.3346-001
3	1.0247-002	2.0389-001
4	1.2964-004	-1.7210-004
5	-4.0112-005	2.4534-004

CONSTANT VELOCITY CONTROLLER 36 PLA 2/13/76

OUTPUT JUMP VECTOR

	1	2
1	-6.4433-001	7.5496-001
2	3.0861-003	4.0847-004
3	-9.2331-003	2.3916-001
4	5.6646-005	2.4458-004
5	2.9411-005	7.2864-005

•FIN

*ELT:IL DATA
 PROCESSED BY UNIVAC 1100 SERIES P-I-T PROCESSOR LEVEL W8 AT 214313R PM ON TUESDAY, FEBRUARY 17, 1976 (CREATING CYCLE 0)

1.	CONSTANT VELOCITY CONTROLLER	24	PLA	2/17/76
2.	OPTION NV=5, NV=5, NU=5, NIND=2, REORD=TRUE, SEND			
3.	1 2 3 4			
4.	F	REDUCED MATRICES 0/OK 24	FIFTH ORDER	
5.	-1978+01	-5117+00	-1099+04	3138+01
6.	-5220+00	-3848+01	-2664+03	-5877+00
7.	-5595+02	-2507-01	-7476+01	-1016-01
8.	.0000	.0000	.0000	-1000+02
9.	.6600+00	.5123+01	.1816+03	.2727+01
10.	G	REDUCED MATRICES 0/OK 24	FIFTH ORDER	
11.	-1183+01	-7731+03	-8319+01	-4360+00
12.	-7752+00	-7162+03	-6873+01	-5312+02
13.	-6480+02	-1505+02	-2601-01	-2240+00
14.	.1000+02	.0000	.0000	.0000
15.	-1243+01	-4509+03	.6855+01	.5297+02
16.	HY	REDUCED MATRICES 0/OK 24	FIFTH ORDER	
17.	.1910+00	-4966+00	.3726+03	.3445-01
18.	.1827-01	-4974+02	-.2526+01	.5388-02
19.	-7082-01	-2302+00	.6456+02	.4239+00
20.	.4339+04	.1404+03	-.6891-01	.1540-03
21.	.5151-04	.6666+03	-.6249-01	.2477-03
22.	DY	REDUCED MATRICES 0/OK 24	FIFTH ORDER	
23.	.2193-01	-8467+02	.1200+01	-.5402+01
24.	-.5072+02	-2623+01	.1587+00	.3382-01
25.	.2376+01	.1293+03	-.9222+00	-.1622+01
26.	-.8377-04	-.6567-01	-.2070-02	-.2230-02
27.	-.1688+03	-.1091+00	.9663+03	-.7591-02

END ELT. TIME: 0.8668 SECONDS.

24/OK/0

-0377-04 -.6567-01 -.2070-02 .2239-02 .1828+00
 -1688-03 -.1091+00 .9683-03 -.7591-02 -.1480+00

F1

	1	1	2
1	-1.0780+000	5.1170-001	
2	-5.2200-001	-3.8480+000	

F12

	1	2	3
1	-1.0990+003	3.1380+000	9.8250+001
2	2.6640+002	-5.8770-001	7.5940+001

F21

	1	2
1	5.5950-003	-2.5070-002
2	0.0000	0.0000
3	6.6000-001	5.1230+000

F22

	1	2	3
1	-7.4760+000	-1.0160-002	6.3020-001
2	0.0000	-1.0000+001	0.0000
3	-1.8160+002	2.7270+000	-1.3440+002

G1

	1	2
1	-1.1830+000	-7.7310+002
2	7.7520-001	7.1620+002

G2

	1	2
1	6.4800-003	-1.5050+001
2	1.0000+001	0.0000
3	-1.2630+000	-0.5090+002

H1

	1	2
1	1.9100-001	-4.9660-001
2	1.8270-002	0.9740-003
3	-7.0820-002	-2.3020-001
4	4.3390-005	1.4040-004
5	5.1510-005	6.4690-004

H2

	1	2	3
1	3.7250+002	3.4450-002	1.4270+001
2	-2.5250+000	5.3880-003	-2.9490-002
3	6.4550+001	4.2390-001	-3.7450-001

4	-6.8910-002	1.5400-004	-8.0430-004
5	-6.2490-002	2.4770-004	-9.3690-003

D1

		1	2
1	-2.1930-002	8.4670+001	
2	-3.0720-003	-2.6230+000	
3	2.3760-002	1.2930+002	
4	-8.3770-005	-6.5670-002	
5	-1.6880-004	-1.0910-001	

F2

1	-5.5245+001	1.4215-001	1.4079+001
2	-2.3437+004	6.2314+001	5.2056+003
3	1.8024+003	-3.2470+000	-4.9000+002

F1

1	-1.7252-001	-3.4546-001
2	-7.3408+001	-1.0520+002
3	6.0201+000	1.0853+001

STATE RATE COMP. MATRIX

1	-4.1233-003	1.2603-002
2	-3.0524-001	1.5802+000
3	-1.0793-003	5.8036-002

STATE INITIAL JUMP MATRIX

1	-2.7400-003	7.2779-003
2	-2.5037-001	1.6396+000
3	-3.8495-003	1.9430-002

CONTROL INITIAL JUMP MATRIX

1	-2.8884+000	-3.1179+000
2	3.1263-003	4.7710-002

CONTROL RATE MATRIX

1	-3.0524-001	1.5802+000
2	2.4792-003	-5.8825-001

OUTPUT RATE MATRIX

1	-1.1904+000	4.6185+000
2	2.1659-002	-9.4834-003
3	-1.5657-001	5.0850-001
4	1.4828-004	-2.7748-004
5	2.8470-005	1.0205-004

CONSTANT VELOCITY CONTROLLER 24 PLA 2/17/76

OUTPUT JUMP VECTOR

	¹	²
1	-9.8312-001	3.3811+000
2	6.3586-003	-1.3059-002
3	5.4023-002	1.7004+000
4	1.0001-004	-3.1678-004
5	2.9175-004	-2.2497-004

9FIN

20/0K/0

	REDUCED MATRICES	0/X	20	FIFTH ORDER
570000	175001	602000	1220002	6037002
195001	504001	315000	5010001	1120003
172002	217001	225000	2537001	655000
0000	0000	0000	0000	0000
145001	530001	204000	6000001	1500003
0000	0000	0000	0000	0000
705001	551000	0010001	1350002	1002005
937001	317000	1010002	3000002	5720004
203701	201000	1000001	2000000	5070002
1000002	0000	0000	0000	0000
005001	237000	1230002	5120002	1070005
0000	0000	0000	0000	0000
307001	505000	0150003	3250000	1100002
200001	707002	1007002	5370001	1200000
245000	202000	0007003	5150001	0007000
202003	2521003	5010000	1070002	3007002
100003	1770002	1021001	2010002	2507001
250003	100003	5000000	0070003	2500002
507003	202003	0077501	1200003	2000003
0000	0000	0000	0000	0000
207500	200003	707001	3000001	1000003
210001	1032002	1050000	0000001	0001002
1000003	5000003	1137001	3730002	1000004
000003	5000003	2000002	2100002	1500001
100003	110001	5350002	1200001	2727001
007003	000000	1100002	0070003	1000003
700003	500000	2251003	1000003	1000003

[illegible]

G1

		1	2
1	-7.2510+000	-5.2180+003	
2	4.3760+000	3.1720+003	

G2

		1	2
1	2.0370+002	2.0120+001	
2	1.0000+001	0.0000	
3	-4.0500+000	-2.3740+003	

CONSTANT VELOCITY CONTROLLER 20 0/OK 3/10/76

H1

1	2.4070-002	3.4050-001
2	2.4020-002	7.4740-003
3	-2.4550-001	-2.5280-001
4	2.4270-004	2.5210-004
5	7.1240-004	1.7780-003
6	2.8380-004	1.2980-004
7	5.1750-005	2.1220-005

H2

1	6.1050-002	2.2540-001	1.1850+001
2	-1.4470-001	3.3700-002	-1.2450-001
3	4.2470-002	5.1540-002	6.0470-001
4	-5.9180-001	1.0750-003	-3.9870-003
5	-1.4210-000	2.9100-003	-2.5870-002
6	-3.5930-001	6.9720-004	-2.5800-003
7	-4.7750-002	1.2050-004	-4.6850-004

DT

1	2.3750-001	2.3900+002
2	-2.1490-002	-1.5320+001
3	4.1660-001	4.0810+002
4	-7.0080-004	-5.2250-001
5	-1.9590-003	-1.3100+000
6	-4.4750-004	-3.4000-001
7	-7.5700-005	-5.6540-002

FB

	1	2	3
1	-1.8329+002	1.4069+000	9.2614+001
2	-1.0169+005	7.0706+002	4.4057+004
3	1.4882+004	-5.2911+001	-3.6357+003

FE

	1	2
1	-2.4504+001	-2.3906+000
2	-0.7276+002	-1.1865+003
3	1.4633+001	9.3519+001

STATE RATE COEF. MATRIX

	1	2
1	-5.3899+003	1.1105+002
2	-0.0001+001	1.3158+000
3	-5.3166+003	5.1461+002

STATE INITIAL JUMP MATRIX

	1	2
1	-1.2159+002	2.2409+002
2	-1.3082+000	3.0513+000
3	-2.6640+002	5.0501+002

CONTROL INITIAL JUMP MATRIX

	1	2
1	-1.2130+001	-2.0513+001
2	2.5012+002	4.1445+002

CONTROL RATE MATRIX

	1	2
1	-1.4601+001	1.3158+000
2	-0.0721+003	-1.1074+002

OUTPUT RATE MATRIX

	1	2
1	-1.8906+000	4.0725+000
2	2.2334+002	-2.1175+003
3	-2.8965+001	5.8106+001
4	1.3175+004	-2.6764+004
5	1.0546+002	3.0941+002
6	1.0001+004	-2.0922+004
7	1.3225+005	-5.0771+005

CONSTANT VELOCITY CONTROLLER 20 0/0K 3/10/76

OUTPUT	1	2
1	-5.5332+000	1.4663+001
2	1.7253+001	-3.4902+001
3	-2.2372+000	1.2311+001
4	5.5203+003	-1.1189+002
5	1.2417+012	-2.0909+002
6	3.5004+003	-7.2225+003
7	5.7550+004	-1.3734+003

83/OK/1.2

FIFTH ORDER

1.2/OK A3

REDUCED MATRICES

F

-9.45+01 -5.53+00 -5.53+00 -5.53+00 -5.53+00 -5.53+00 -5.53+00 -5.53+00 -5.53+00 -5.53+00

-19.1+01 -5.53+01 -1.41+03 -1.41+03 -1.41+03 -1.41+03 -1.41+03 -1.41+03 -1.41+03 -1.41+03

-4.10+02 -5.53+02 -5.53+02 -5.53+02 -5.53+02 -5.53+02 -5.53+02 -5.53+02 -5.53+02 -5.53+02

-5.53+00 -5.53+00 -5.53+00 -5.53+00 -5.53+00 -5.53+00 -5.53+00 -5.53+00 -5.53+00 -5.53+00

-5.53+01 -1.41+02 -1.41+02 -1.41+02 -1.41+02 -1.41+02 -1.41+02 -1.41+02 -1.41+02 -1.41+02

-3.17+01 -5.53+02 -5.53+02 -5.53+02 -5.53+02 -5.53+02 -5.53+02 -5.53+02 -5.53+02 -5.53+02

-4.03+00 -5.53+04 -1.00+03 -1.00+03 -1.00+03 -1.00+03 -1.00+03 -1.00+03 -1.00+03 -1.00+03

-2.14+02 -1.14+03 -5.53+00 -5.53+00 -5.53+00 -5.53+00 -5.53+00 -5.53+00 -5.53+00 -5.53+00

-1.0+02 -5.53+00 -5.53+00 -5.53+00 -5.53+00 -5.53+00 -5.53+00 -5.53+00 -5.53+00 -5.53+00

-5.12+00 -1.55+04 -2.30+03 -2.30+03 -2.30+03 -2.30+03 -2.30+03 -2.30+03 -2.30+03 -2.30+03

REDUCED MATRICES

1.2/OK A3

F

-9.45+00 -3.33+01 -3.33+01 -3.33+01 -3.33+01 -3.33+01 -3.33+01 -3.33+01 -3.33+01 -3.33+01

-3.33+01 -1.03+02 -1.03+02 -1.03+02 -1.03+02 -1.03+02 -1.03+02 -1.03+02 -1.03+02 -1.03+02

-4.51+01 -1.03+01 -1.00+02 -1.00+02 -1.00+02 -1.00+02 -1.00+02 -1.00+02 -1.00+02 -1.00+02

-2.27+04 -2.27+04 -4.40+02 -4.40+02 -4.40+02 -4.40+02 -4.40+02 -4.40+02 -4.40+02 -4.40+02

-2.51+04 -3.03+03 -3.30+02 -3.30+02 -3.30+02 -3.30+02 -3.30+02 -3.30+02 -3.30+02 -3.30+02

REDUCED MATRICES

1.2/OK A3

F

-4.52+00 -2.67+04 -4.40+02 -4.40+02 -4.40+02 -4.40+02 -4.40+02 -4.40+02 -4.40+02 -4.40+02

-1.187+03 -1.147+01 -1.149+01 -1.149+01 -1.149+01 -1.149+01 -1.149+01 -1.149+01 -1.149+01 -1.149+01

-3.271+01 -1.555+03 -4.021+01 -4.021+01 -4.021+01 -4.021+01 -4.021+01 -4.021+01 -4.021+01 -4.021+01

-7.590+05 -2.718+01 -5.934+02 -5.934+02 -5.934+02 -5.934+02 -5.934+02 -5.934+02 -5.934+02 -5.934+02

-1.442+00 -5.470+01 -2.940+02 -2.940+02 -2.940+02 -2.940+02 -2.940+02 -2.940+02 -2.940+02 -2.940+02

F11

1 -9.04+00+000 -6.0370+001

2 -1.0110+000 -8.4310+000

F12

1 -5.4950+002 3.4100+001 1.3220+002

2 1.6130+002 -1.0550+001 4.1260+001

F21

1 4.1400+003 -3.8440+002

2 0.0100 0.0000

3 5.1500+000 1.0570+001

F22

1 -9.0200+000 1.1250+002 5.8890+001

2 0.0100 -1.0000+001 0.0000

3 -1.5150+001 1.7700+000 -1.7220+002

G1

1 -3.1750+002 -6.5050+001

2 5.4130+001 2.5870+003

63

1	1	2
1	-2.3140-003	-1.3440+002
2	1.0000+001	0.0000
3	-5.1220-001	-1.5550+003

CONSTANT VELOCITY CONTROLLER 63 1.2/OK 3/10/76

H1

	1	2
1	-8.1010-001	-1.1100+000
2	1.1770-002	1.0010-003
3	-4.5170-002	-9.8540-002
4	2.0470-005	6.2470-005
5	2.5100-005	3.4590-004

H2

	1	2	3
1	3.4220+002	-7.0140-001	4.3470+001
2	-6.4020-002	4.0470-004	-1.4610-003
3	1.0040+001	4.2140-002	-1.2990-001
4	-4.0040-003	1.0250-005	-1.1740-004
5	-1.2010-003	1.8330-005	-1.7320-003

460 D1

	1	2
1	4.5240-001	2.4700+003
2	-1.1570-004	1.1470+000
3	3.2710-002	1.5550+002
4	-7.4500-006	-2.7040-002
5	-1.4420-005	-5.4700-002

CONSTANT VELOCITY CONTROLLER 03 1.2/OK 3/10/76

PT

	1	2	3
1	-1.200+003	7.4741-001	2.8040+002
2	-1.4422+005	2.2735+002	8.4732+004
3	4.2983+003	-1.1590+000	-1.1979+003

FT

	1	2
1	-1.045+001	-2.4343+000
2	-4.0572+003	-6.0526+002
3	7.5726+001	1.2930+001

STATE RATE COMP. MATRIX

	1	2
1	-9.0758+003	2.7345+002
2	4.4474+001	5.4940+000
3	2.7153+002	1.1271+001

STATE INITIAL JUMP MATRIX

	1	2
1	-2.4458+003	2.5736+003
2	-1.2340+001	1.1925+000
3	-2.6739+003	8.5398+003

CONTROL INITIAL JUMP MATRIX

	1	2
1	-0.4584+001	-1.4474+000
2	1.7129+002	8.2361+000

CONTROL RATE MATRIX

	1	2
1	4.4174+001	5.4940+000
2	7.0752+004	-1.2598+003

OUTPUT RATE MATRIX

	1	2
1	-4.6448+001	7.3464+000
2	3.3520+002	1.2927+000
3	1.0415+002	3.8788+001
4	4.1510+005	-2.2902+005
5	-3.1497+005	1.2578+005

CONSTANT VELOCITY CONTROLLER 03 1.2/0K 3/10/76

OUTPUT JUMP VECTOR	
	1 2
1	1.2707+000 1.4633+000
2	2.8334+002 1.7051+003
3	3.8258+001 1.4884+001
4	5.8015+005 -9.4794+005
5	1.3555+004 -2.1448+005

83/30K/0.9

FIFTH ORDER

FIFTH ORDER

FIFTH COVER

FIFTH ORDER

REDUCED MATRICES	0.730K + 83
-3387+01	-5534+03
-1127+00	-1504+01
-1728+01	-1716+03
-500+03	-1257+01
-2584+02	-1415+01
-3200+00	-1140+02
-1720	-1000+02
-4930+01	-4375+03
	-7264+01
	-2055+03
	0.730K + 83
REDUCED MATRICES	0.730K + 83
-163+00	-3317+00
-3115+03	-1667+02
-512+00	-3712+01
-5320+02	-7238+01
-100+02	-7199+01
-2260+00	-2000
-169+00	-5599+02
	-972+02
	0.730K + 83
REDUCED MATRICES	0.730K + 83
-1234+01	-3316+02
-6900+00	-3398+00
-781+02	-4425+02
-2074+03	-1405+03
-2471+03	-1764+01
-1255+04	-2265+00
-2680+03	-1173+01
-169+03	-1002+03
-1437+00	-1107+01
	-9824+04
	-6594+02
	-1559+03
	-3177+03
	0.730K + 83
REDUCED MATRICES	0.730K + 83
-5774+03	-5607+02
-304+00	-7288+01
-260+00	-3565+00
-5027+01	-901+03
-317+04	-3284+01
-164+03	-2002+02
-222+04	-1031+03
-737+03	-2011+02
	-1255+02
	-1408+01
	-1257+01
	-3249+00
	0.730K + 83
REDUCED MATRICES	0.730K + 83
-104+00	-3264+02
-2939+01	-1160+02
	-650+03

—
—
ca.

5. 3430-001 - 5.3470-000
3. 1430-001 - 2.5510-000

2.2

	I	2	3
1	4.4540+002	1.5020+000	1.7160+002
2	3.2320+002	1.2570+000	4.7720+001

121

$$\begin{array}{r} 1 \\ -5.7500-004 \\ 0.0000 \\ -2.8310+000 \\ \hline -8.5810-004 \end{array} \quad \begin{array}{r} 2 \\ -2.1860-003 \\ 0.0000 \\ \hline -4.9390+000 \end{array}$$

22

1	2	3
-1.100+001	1.250+002	5.250+001
0.0000	-1.000+001	0.0000
0.9750+002	2.750+000	-2.0550+002

G1		
	1	2
	-5.0330-001	1.4080+003
	-5.1420-001	3.1150+002
G2		
	1	2
	-5.0090-003	-5.8200+001
	1.0000+001	0.0000
	-2.2040-001	-1.6300+003

3/10/76

83 9/30K

CONSTANT VELOCITY CONTROLLED

H1

	1	2
1	1.0360+000	-1.2340+000
2	7.8510-003	-6.8900-005
3	2.0070-001	-1.1150-001
4	2.8730-004	-7.0550-005
5	-1.2430-004	2.0640-004
6	1.3370-004	-1.0690-004
7	3.7140-005	-1.6370-005

H2

	1	2	3
1	1.9150+001	-2.1920+001	5.2320+001
2	-4.8250-003	1.0050-004	1.0060-002
3	1.7250+000	2.2950-001	-8.0330-001
4	-1.1700-002	-1.0020-004	1.3330-003
5	1.1700-002	9.4240-005	-4.5940-003
6	-4.4550-003	-0.0130-005	1.5590-003
7	-1.9240-003	-2.5520-005	3.1770-004

DT

	1	2
1	-1.0950-001	8.3740+002
2	2.5070-005	3.6040-001
3	-5.9120-002	1.3530+002
4	3.1670-005	9.4930-002
5	-1.0640-005	-9.0300-002
6	2.2210-005	1.0340-001
7	7.8440-006	2.0720-002

FD

	1	2	3
1	-1.5384+001	-2.0060+003	7.6723+000
2	-2.8289+003	1.4507+001	1.7480+002
3	-1.7684+002	2.8268+000	-5.1898+000

F1

	1	2
1	2.8254+002	-1.8415+001
2	1.5672+000	-2.8850+001
3	-2.0164+000	-1.0451+001

STATE RATE CO-P. MATRIX

	1	2
1	-2.1165+002	2.7599+002
2	-2.9819+000	5.2351+000
3	-1.2100+001	1.7803+001

STATE INITIAL JUMP MATRIX

	1	2
1	-1.5000+002	1.4097+002
2	-2.3741+000	3.4528+000
3	-2.2032+002	2.2957+002

CONTROL INITIAL JUMP MATRIX

	1	2
1	3.2065+001	-1.5530+000
2	5.0582+000	8.0077+001

CONTROL RATE MATRIX

	1	2
1	-2.7014+000	5.2351+000
2	2.0028+003	-2.8265+003

OUTPUT RATE MATRIX

	1	2
1	-3.0565+000	4.0904+000
2	8.2239+003	-1.7003+002
3	8.2031+002	3.0382+001
4	-2.0040+000	-7.0287+004
5	-2.1631+005	2.2302+005
6	5.2159+004	-7.3305+004
7	1.4700+000	-1.0363+004

CONSTANT VELOCITY CONTROLLER 63 .9/30K 3/10/76

OUTPUT TIME VECTOR

	1	2
1	-3.8902+000	5.7074+000
2	-1.4167+000	7.0262+000
3	-0.5203+001	0.2173+001
4	3.6707+000	-3.8485+000
5	0.7780+005	-1.8658+004
6	2.8712+005	-2.7770+005
7	5.2905+005	-8.1676+005

FIFTH ORDER

FIFTH ORDER

FILE	1	2
	-1.1250+000	-2.7010-001
	-3.4200-002	-1.9170+000

F12		1	-5.6420+002	8.9230-001	1.2540+002
		2	-1.7770+002	2.0020+000	3.0490+001
					100+005
					200+

1	5.0540-003	-7.2730-003
2	0.0000	0.0000
3	2.32870=001	2.10500=000

1	-7.21+0.00	1.2150+0.02	3.9300+0.01
2	0.0000	-1.0000+0.01	0.0000
3	1.0780+0.02	1.5580+0.00	-1.1700+0.02

G1			
	1	1	2
	2	-4.7900-001	7.7410+001
		-5.2200-001	9.2910+000
G2			
	1	1	2
	2	-2.2450-003	-1.5350+001
	3	1.0000+001	0.0000
		-4.2770-001	-5.3170+001
H1			
	1	1	2
	2	-3.4830-002	-4.6350-001
	3	1.0950-002	1.6040-003
	4	-1.2720-002	-1.0500-001
	5	1.1540-004	1.1100-004
	6	3.5590-005	2.1440-004
	7	-2.4340-005	9.0470-003
		3.3420-005	2.6610-006
H2			
	1	1	2
	2	-2.5270+002	2.5200-001
	3	-7.5460-001	5.0550-004
	4	-1.2020+000	9.9330-001
	5	-4.9540-002	2.7310-005
	6	1.2340-002	8.8000-005
	7	-6.5740-002	-1.4340-005
		-1.4750-002	-5.3000-006
			1.0510-004
DT			
	1	1	2
	2	-2.2910-001	-3.2300+000
	3	-4.4530-004	-1.3300-001
	4	-2.0190-001	1.6580+001
	5	-3.2190-005	-1.8430-002
	6	-1.4370-005	1.2050-003
	7	-2.0440-005	8.4080-007
		-3.0420-006	2.2440-003

3/10/76

0.230K

CONSTANT VELOCITY CONTROLLER

F2

	1	2	3
1	-9.0129+001	-2.0478+001	2.0144+001
2	-1.2644+003	3.0828+001	5.2625+002
3	-1.0075+002	-0.2807+001	-7.1622+001

F1

	1	2
1	-2.0505+001	3.1271+001
2	2.0501+000	-3.8425+001
3	-7.1744+001	4.8307+000

STATE RATE COMP MATRIX

	1	2
1	-3.0123+003	9.5128+003
2	-1.9300+001	1.1504+000
3	-3.2786+003	3.9093+002

STATE INITIAL JUMP MATRIX

	1	2
1	-3.1847+003	2.5475+003
2	-1.9208+001	7.3421+001
3	-5.1082+003	9.1258+003

CONTROL INITIAL JUMP MATRIX

	1	2
1	2.5545+001	-2.1533+000
2	1.0520+002	-1.3349+002

CONTROL RATE MATRIX

	1	2
1	-1.2300+001	1.1504+000
2	1.0491+003	-3.2278+003

OUTPUT RATE MATRIX

	1	2
1	-8.0283+001	2.9858+000
2	1.3038+002	-0.0891+003
3	-1.3350+001	7.3031+001
4	2.3025+004	-3.1564+004
5	2.2324+005	-1.4031+004
6	3.1400+004	-6.4742+004
7	8.3007+005	-1.5071+004

3/10/76

.9/3AK

CONSTANT VELOCITY CONTROLLER

OUTPUT JUMP VECTOR	
1	2
-1.001+000	1.6143+000
2.1617-004	1.3029-003
0.7255-003	2.3633-001
-1.2123-004	2.0345-004
1.3501-005	-1.4574-005
3.2716-004	-2.0386-004
7.9829-005	-6.4401-005

83/45K/0.9

FIFTH ORDER

83

F
-0404+00
-5044+00
-1111+04
-1337+01
-1297+03
-7045+00
-1444+01
-2644+03
-1910+00
-9773+02
-2590+02
-5151+02
-8884+01
-7300+02
-5756+00
-6030
-0000
-1000+02
-0000
-7038+00
-1414+01
-6573+03
-1725+01
-1697+03

FIFTH ORDER

83

E
-2392+00
-3610+03
-2723+02
-4001+01
-2400+04
-4113+01
-5044+02
-1747+02
-1417+02
-7194+04
-6546+03
-2077+02
-9120+01
-7401+01
-5711+01
-1000+02
-0000
-1034+03
-1230+02
-1411+02
-1920+05

FIFTH ORDER

83

F
-3704+00
-0550+00
-4317+01
-7515+01
-4308+02
-4725+02
-1005+03
-1315+01
-2221+03
-4375+05
-1405+00
-5004+01
-3514+02
-4194+00
-1059+01
-2003+03
-1452+05
-6021+01
-1185+04
-2939+03
-2204+04
-1520+03
-4700+01
-8306+04
-1107+01
-5705+04
-3720+04
-4392+01
-4372+04
-7977+03
-1677+04
-3315+05
-1152+01
-4744+05
-4944+04

FIFTH ORDER

83

F
-5220+02
-2122+03
-6004+01
-3007+01
-5379+04
-4354+06
-2040+00
-1790+00
-3703+03
-1546+01
-1370+01
-5124+02
-2443+01
-4304+00
-1930+04
-9407+04
-2571+01
-7355+03
-1406+03
-5009+00
-2560+04
-1031+01
-1070+02
-1621+02
-2019+00
-1014+04
-2554+01
-1901+02
-2397+03
-2633+00
-2037+04
-9072+02
-6710+03
-4847+04
-6065+01

F11

1 -0.6000+001 -5.0000+001
2 7.5550+001 -1.4440+000

F12

1 -1.110+003 1.3370+000 1.2970+002
2 -5.440+002 -1.0100+001 4.7730+001

F21

1 2.5000+003 -5.1810+003
2 0.0000 0.0000
3 -7.4340+001 1.2160+000

F22

1 -1.500+000 7.3900+003 5.7550+001
2 0.0000 -1.0000+001 0.0000
3 4.5720+002 1.7250+000 -1.6970+002

G1	1	
	1	2
	1	2
	2	3
G2	1	
	1	2
	1	2
	2	3
H1	1	
	1	2
	1	2
	2	3
H2	1	
	1	2
	1	2
	2	3
H3	1	
	1	2
	1	2
	2	3

F2

	1	2	3
1	-4.0122+002	3.7270+002	7.6311+001
2	-3.4009+005	7.1033+001	6.4999+004
3	7.0180+003	-3.4002+001	-1.3158+003

F1

	1	2
1	5.5104+001	-1.5145+000
2	3.7625+002	-1.1407+003
3	-6.4717+000	2.1601+001

STATE RATE CONF. MATRIX

	1	2
1	-4.2102+003	1.1447+003
2	-1.2720+000	2.2008+000
3	-5.1579+002	7.2000+002

STATE INITIAL JUMP MATRIX

	1	2
1	-2.0652+003	1.1343+002
2	-1.1277+001	2.4036+000
3	-1.3381+002	6.2093+002

CONTROL INITIAL JUMP MATRIX

	1	2
1	-1.5559+001	-6.4173+001
2	7.5302+003	0.1907+002

CONTROL RATE MATRIX

	1	2
1	-1.2720+000	2.2008+000
2	2.0516+003	-2.2711+003

OUTPUT RATE MATRIX

	1	2
1	-1.2733+000	2.1570+000
2	0.5759+003	-1.0170+002
3	7.6049+002	2.0111+001
4	7.5+55+004	-2.9425+004
5	-2.7753+005	2.6536+005
6	4.0000+000	-6.1110+004
7	1.2181+000	-1.5+79+004

3/10/76

09/45K

B3

CONSTANT VELOCITY CONTROL LER

OUTPUT JUNE VECTOR		
	1	2
1	1.1467+000	1.2636+001
2	1.5421+003	9.2317+003
3	2.4515+001	1.9458+000
4	3.5213+004	4.3197+004
5	2.0006+004	4.8354+004
6	1.1919+004	-2.0375+004
7	5.7020+005	5.6648+005

40/45K/0.9

FIFTH ORDER

4145K

REDUCED MATRICES

6

[illegible]

FIFTH ORDER

9145x

DECEMBER 1967

2

+	98	+6	-103+01	=3773+01
+	98	+01	-3376+01	=-6751+03
+	98	+02	-5761-01	=-1103+02
+	98	+02	.000	=000
+	98	+02	.000	=000

FIFTH ORDER

9/45K

53715154 63716365

5

[illegible]

FIFTH ORDER

9145K

Rejection Rates

2

• 203 + 0	• 134 + 0	• 143 + 0	• 273 + 0	• 121 + 0
• 370 + 3	• 500 + 0	• 154 + 0	• 741 + 2	• 188 + 0
• 263 + 0	• 200 + 0	• 150 + 0	• 199 + 0	• 702 + 3
• 330 + 4	• 242 + 0	• 204 + 0	• 702 + 3	• 157 + 0
• 330 + 4	• 242 + 0	• 204 + 0	• 702 + 3	• 157 + 0

476

1994

	t	τ
1	-1.2480 ± 0.00	-2.1200 ± 0.01
2	-1.7700 ± 0.01	-1.1100 ± 0.00

25

1	-6.2200+002	2	1.0150+000	3	1.3790+002
2	-4.2140+001		8.1450+001		4.0230+001

45

$$\begin{array}{r} 8.4120-003 = 8.5140-003 \\ 0.0000 \quad 0.0000 \\ 9.4020-001 \quad 1.5130+000 \end{array}$$

222

	1	2	3
1	0.000000	0.000000	0.000000
2	0.000000	0.000000	0.000000
3	0.000000	0.000000	0.000000

AD-A052 346

SYSTEMS CONTROL INC PALO ALTO CALIF AERONAUTICAL AND--ETC F/G 21/5
F100 MULTIVARIABLE CONTROL SYNTHESIS PROGRAM. VOLUME II. APPEND--ETC(U)
JUN 77 R L DE HOFF, W E HALL, R J ADAMS

F33615-75-C-2053

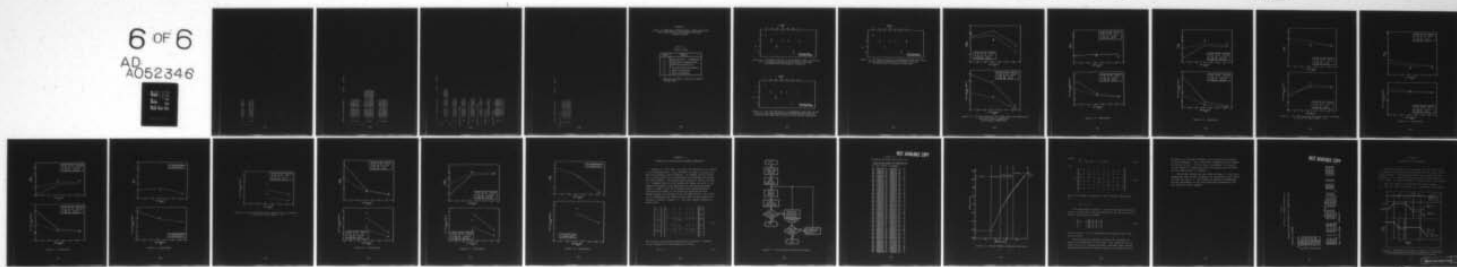
AFAPL-TR-77-35-VOL-2

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UNCLASSIFIED

6 OF 6

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DATE
FILMED

5-78

DDC

61

1	1	2
1	-1.0000-001	2.2300+001
2	-2.5200-002	5.9500+001

62

1	1	2
1	-1.0000-001	1.2300+001
2	1.0000+001	0.0000
3	-5.6000-001	-5.1400+001

09/45K 3/10/76

CONSTANT VELOCITY CONTROLLER

H1

	1	2
1	-2.0100-002	-2.7710-001
2	4.8290-003	5.0640-000
3	-5.0940-002	-4.2080-002
4	1.7570-005	4.0940-005
5	4.6110-005	4.1040-004
6	7.7110-005	-7.0190-006
7	2.6810-005	6.4450-006

H2

	1	2	3
1	1.6220+002	21.4670-001	3.4250+001
2	-7.3320-001	1.0500-003	-1.0400-002
3	-1.4940+001	1.1720+000	-1.3140+000
4	-6.7040-002	1.0600-004	-1.0050+003
5	4.2340-003	2.5050-004	-2.2300-002
6	-2.1140-002	5.4510-005	-9.6530-006
7	-2.5240-002	1.4890-005	-1.7070-004

DT

	1	2
1	-2.2030-001	1.3410+001
2	-1.2700-000	-3.0940-001
3	-2.0030-001	6.0020+000
4	-1.5200-005	-2.6420-002
5	-1.1530-000	-1.2550-002
6	-7.6470-007	-1.0120-002
7	7.9340-007	-4.3120-003

$\overline{F2}$
 1 3.0224+000 1.5508+001 5.6505+000
 2 -2.0155+000 8.9449+000 3.5733+003
 3 1.8942+003 1.5358+000 -3.2160+002

$\overline{F1}$
 1 -4.2641+004 -2.4620+001
 2 -3.4901+001 9.6463+000
 3 2.6609+000 -3.7403+001

STATE RATE COMP. MATRIX
 1 -1.0541+003 4.3957+003
 2 -2.6557+002 7.5088+001
 3 1.0220+003 2.0231+002

STATE INITIAL JUMP MATRIX
 1 -2.0304+003 3.2014+003
 2 -4.0729+002 9.2767+001
 3 -2.0873+003 1.2291+002

CONTROL INITIAL JUMP MATRIX
 1 -3.0006+000 1.0300+000
 2 -1.2784+003 1.7308+002

CONTROL RATE MATRIX
 1 -2.4557+002 7.5088+001
 2 1.0248+003 -1.7332+003

OUTPUT RATE MATRIX
 1 -1.9378+001 1.2064+000
 2 9.6844+003 -1.8628+003
 3 -5.3431+002 5.6185+001
 4 7.0541+005 -1.4500+004
 5 -2.4408+005 1.2662+004
 6 1.8306+004 -3.2434+003
 7 4.3331+005 -7.5319+005

3/10/76

.9/45K

CONSTANT VELOCITY CONTROLLER

OUTPUT DATA	
1	2
1 1.8245-001	1.1400+000
2 3.4444-003	-7.4559-003
3 4.0742-001	5.2442-001
4 2.7542-004	-5.4417-004
5 2.1242-004	-4.2604-004
6 2.4223-004	-5.7523-004
7 4.3370-005	-1.3470-004

APPENDIX I

EFFECT OF COMPONENT DETERIORATION, POWER EXTRACTION AND BLEED FLOW ON F100 TURBOFAN CONTROL SYSTEM DESIGNS

Table I.1
Index of Data

FIGURE	COMMENTS
I.1	} Altitude Points - Intermediate Power Data for Nominal Deter- ioration and Bleed Flow
I.2	
I.3	
I.4	Sea Level Static Performance*
I.5	30K/0.9 Performance*
I.6	10K/0.9 Performance*

* Data for each effect is given as a function
of power level

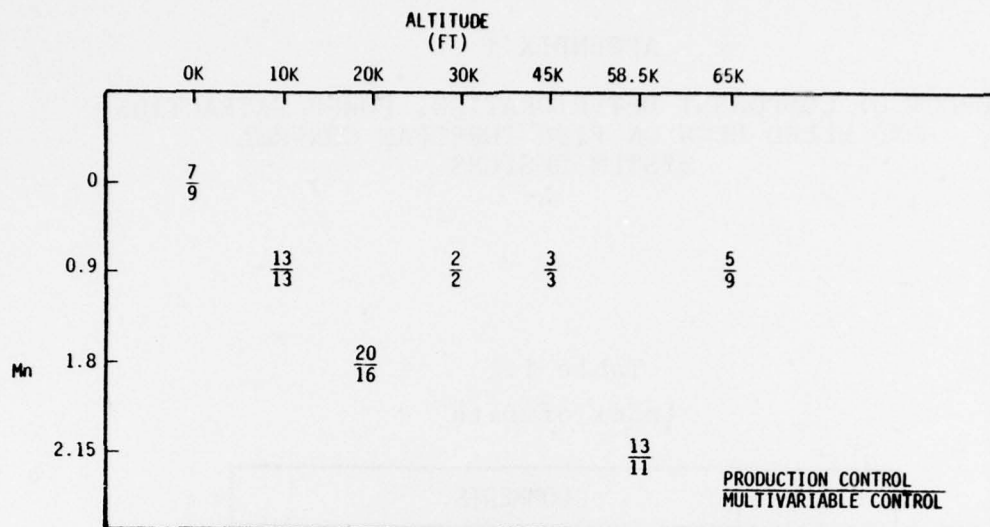


Figure I.1 Per Cent Variation in Intermediate Power Net Thrust Due to Component Deterioration at Various Altitudes and Velocities from Digital Evaluation

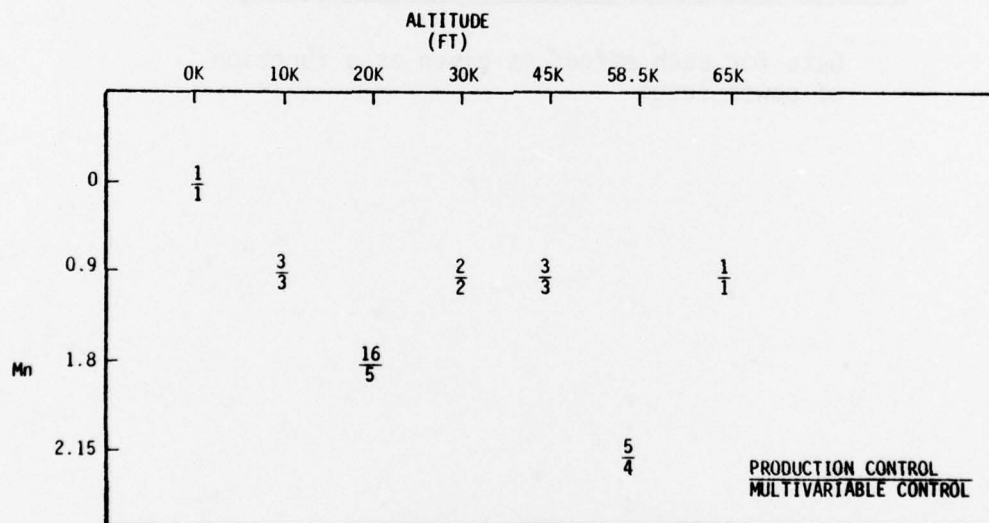


Figure I.2 Per Cent Variation in Intermediate Power Net Thrust Specific Fuel Consumption Due to Component Deterioration at Various Altitudes and Velocities from Digital Evaluation

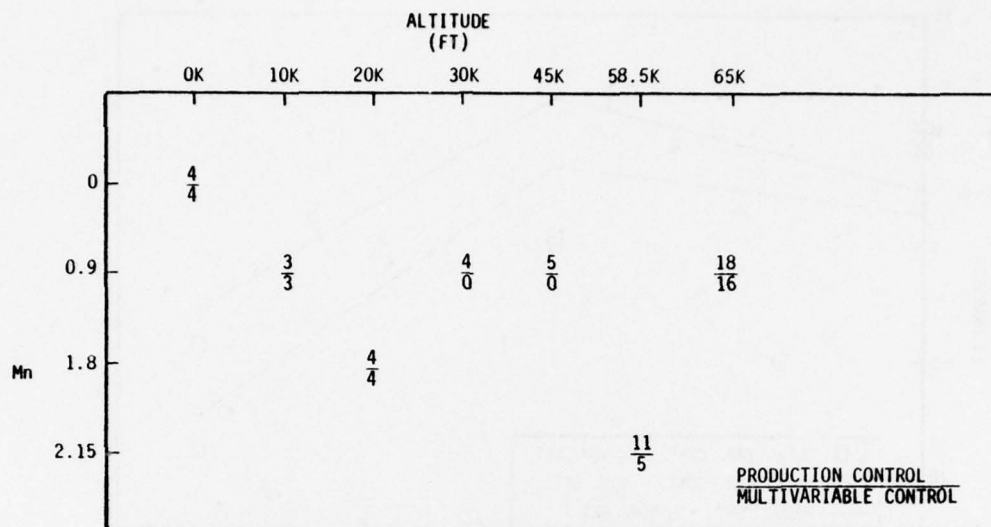


Figure I.3 Per Cent Variation in Intermediate Power Net Thrust Due to Customer Bleed Flow at Various Altitudes and Velocities from Digital Simulation

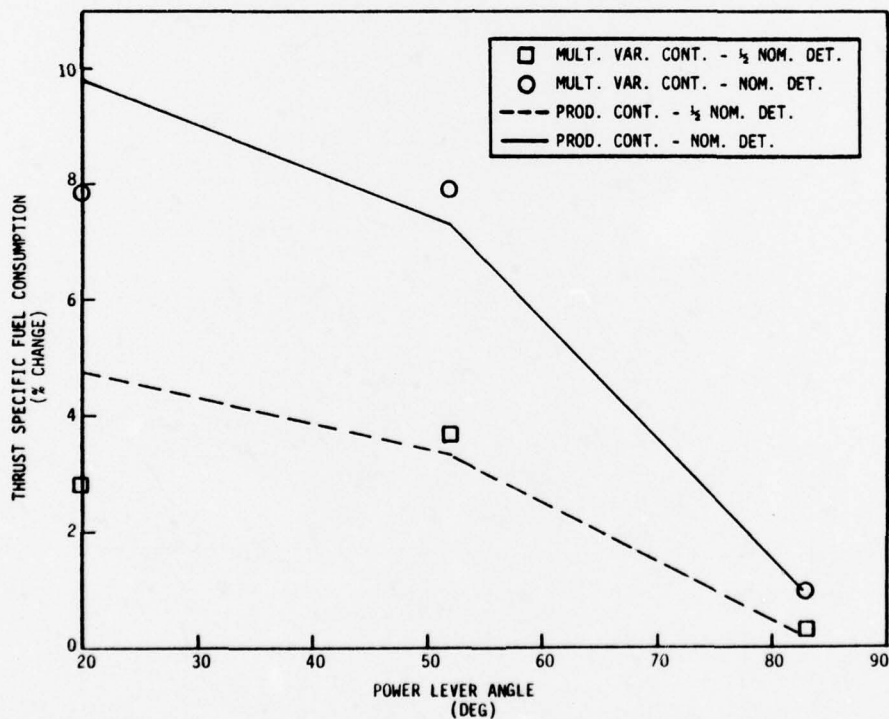
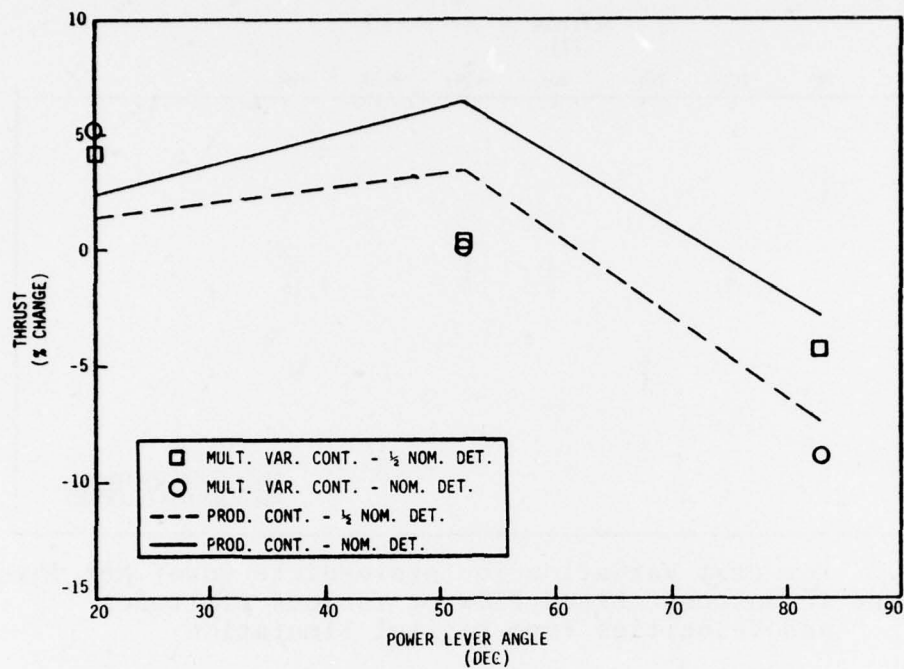


Figure I.4 Per Cent Variation in Steady-State Performance at Sea Level Static Conditions from Digital Simulation

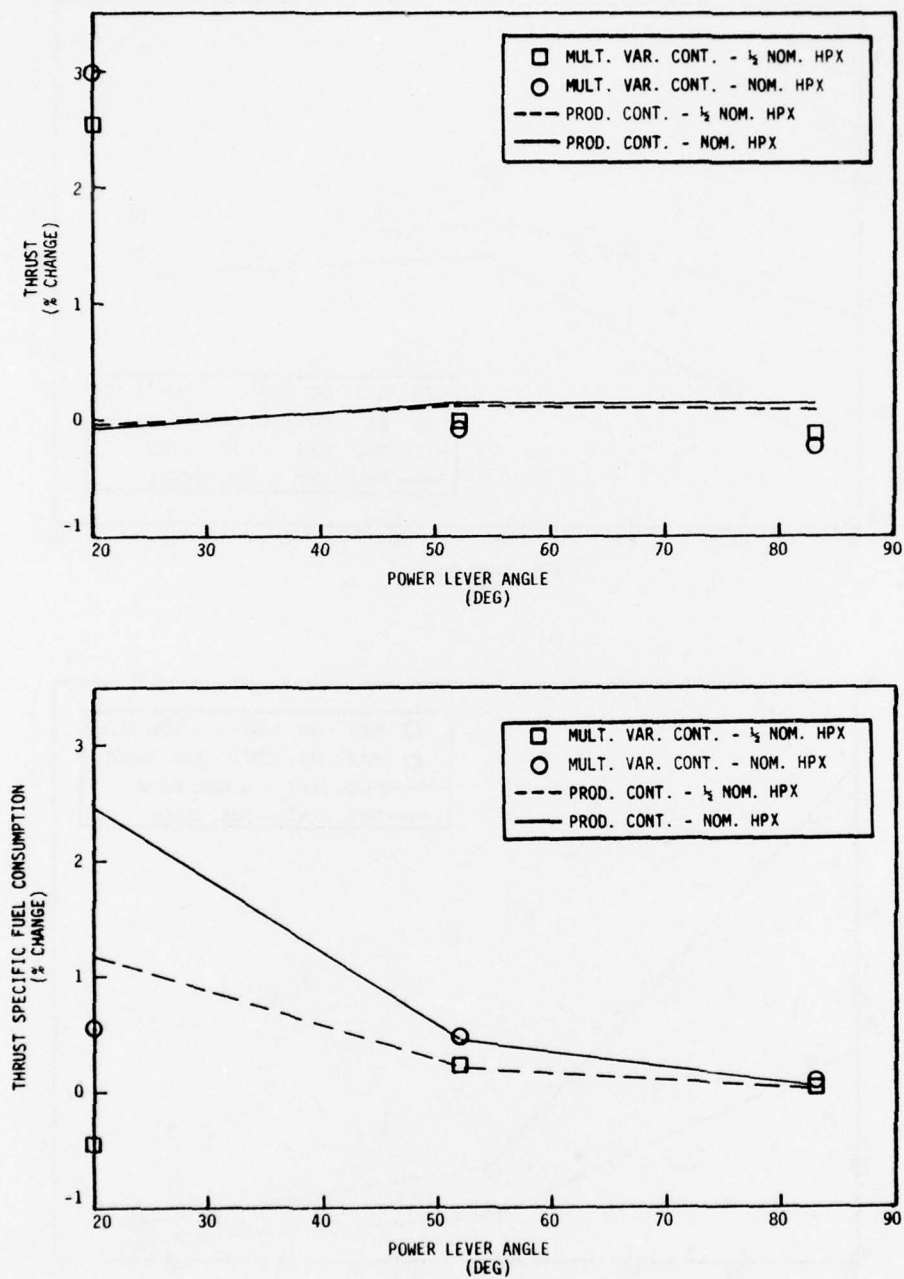


Figure I.4 (Continued)

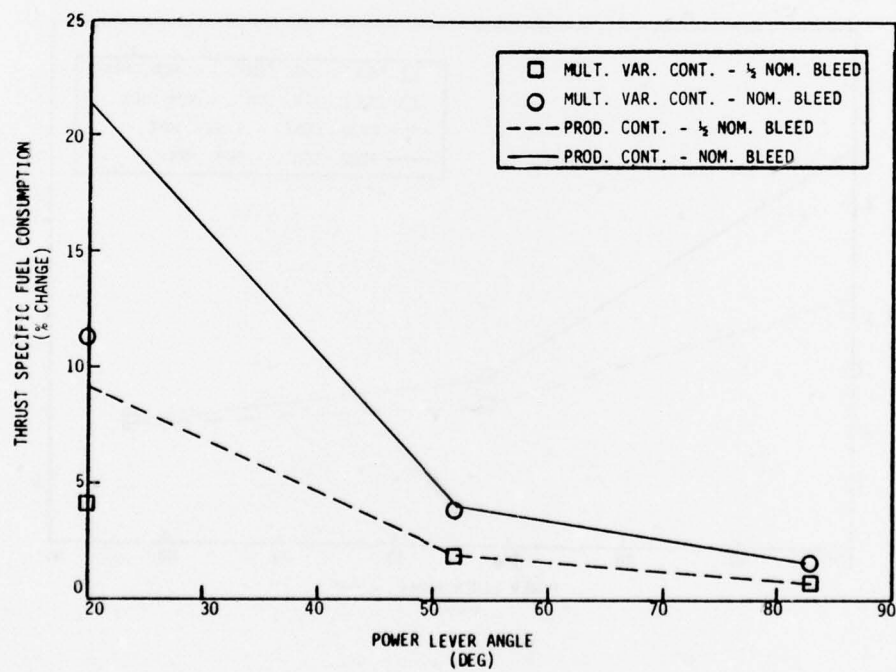
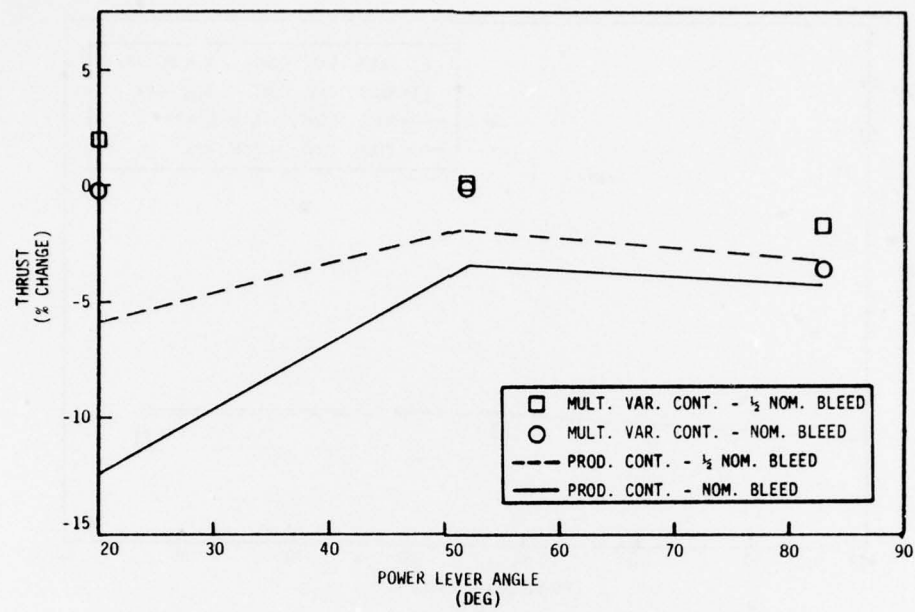


Figure I.4 (Continued)

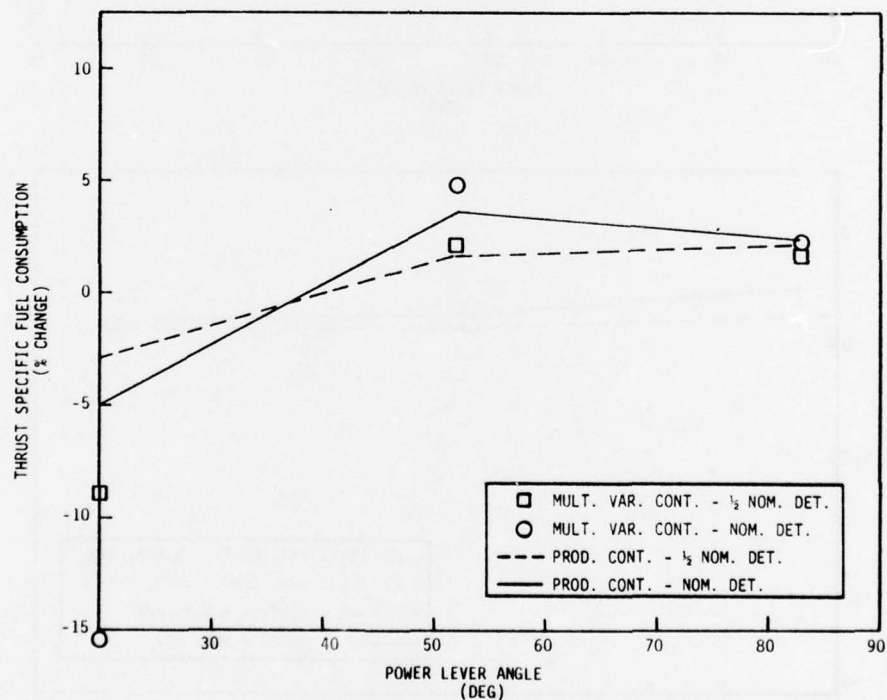
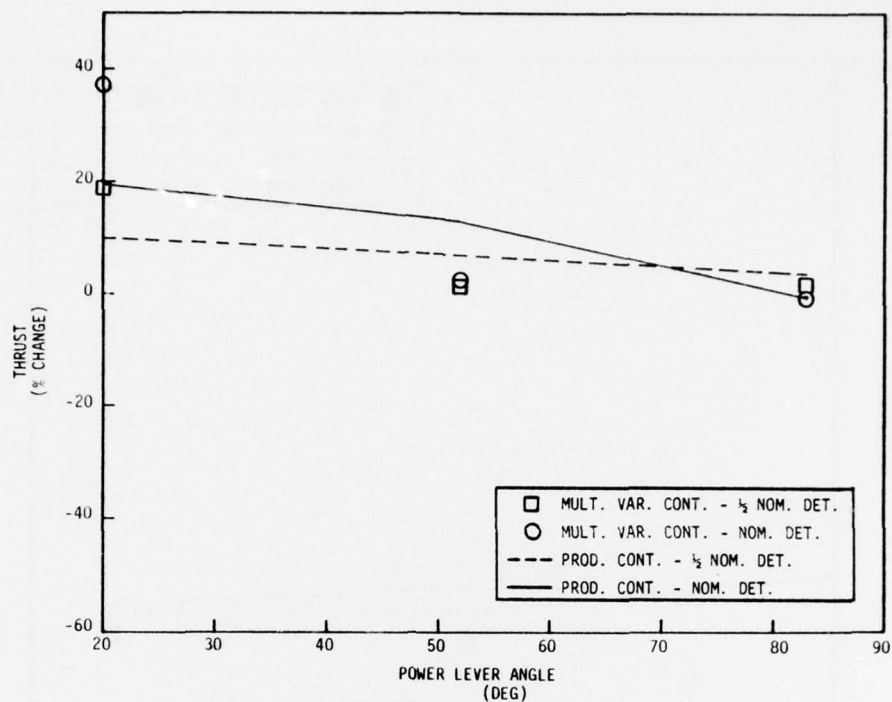


Figure I.5 Per Cent Variation in Steady-State Performance at 30,000 Ft, Mach Number = 0.9

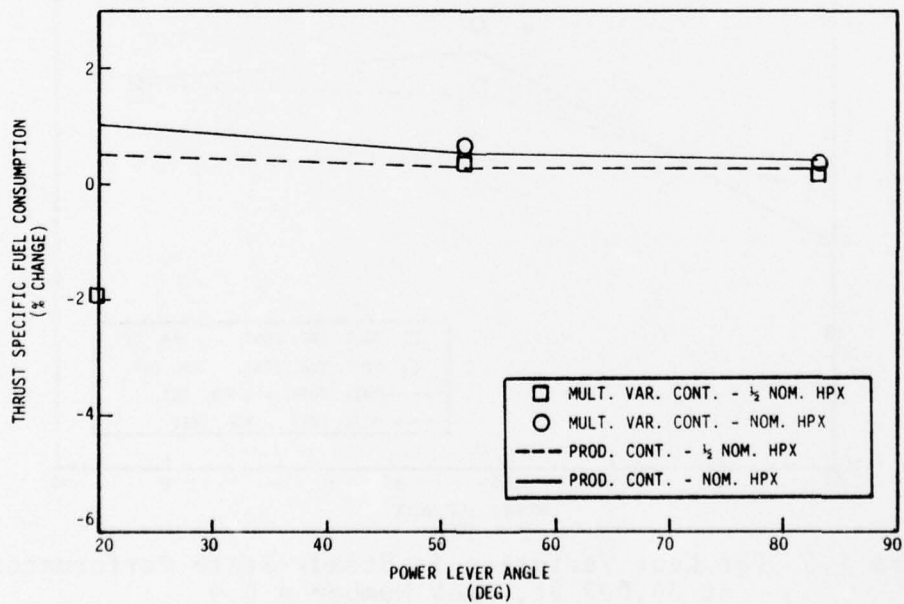
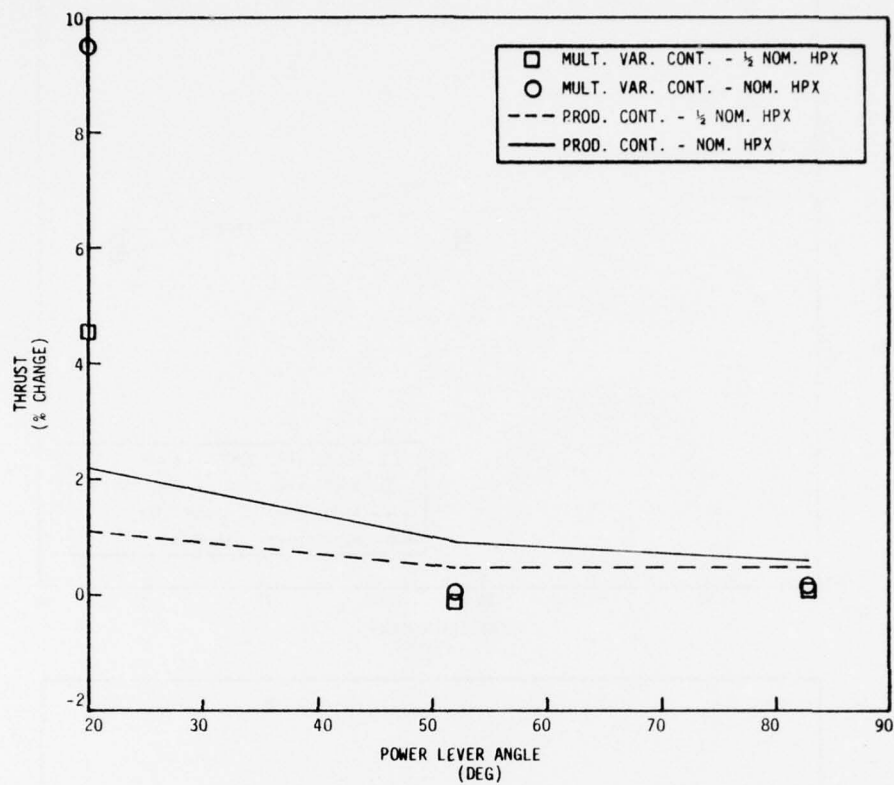


Figure I.5 (Continued)

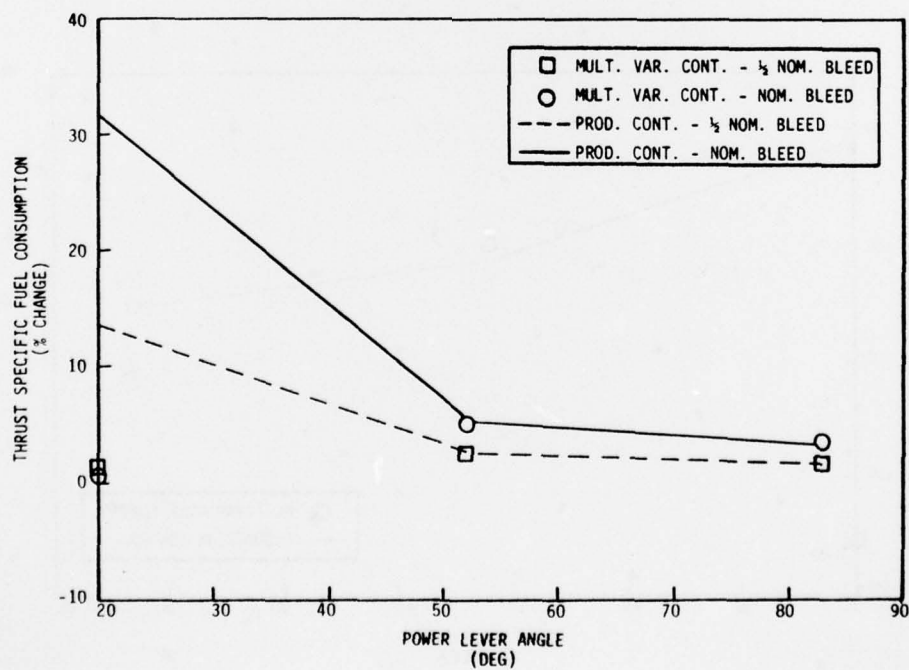
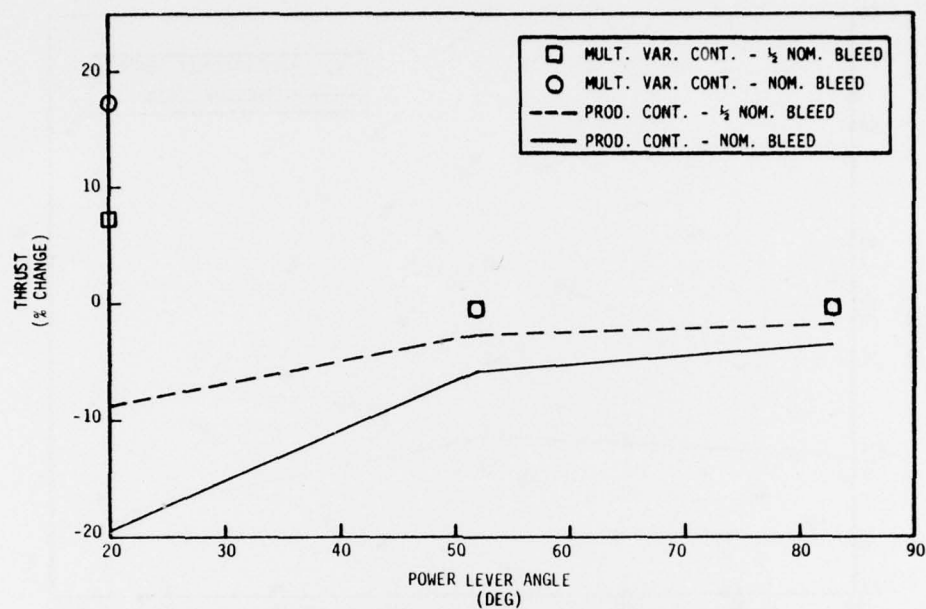


Figure I.5 (Continued)

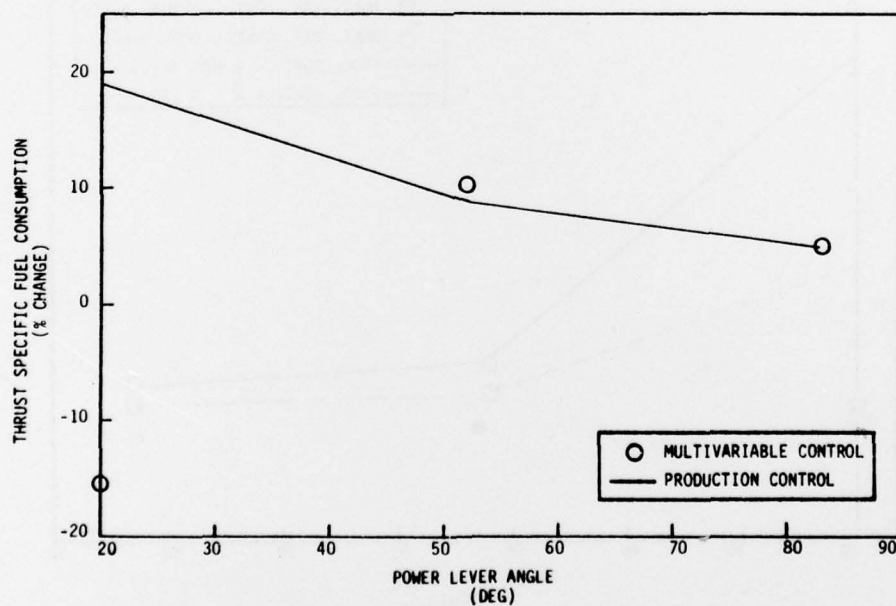
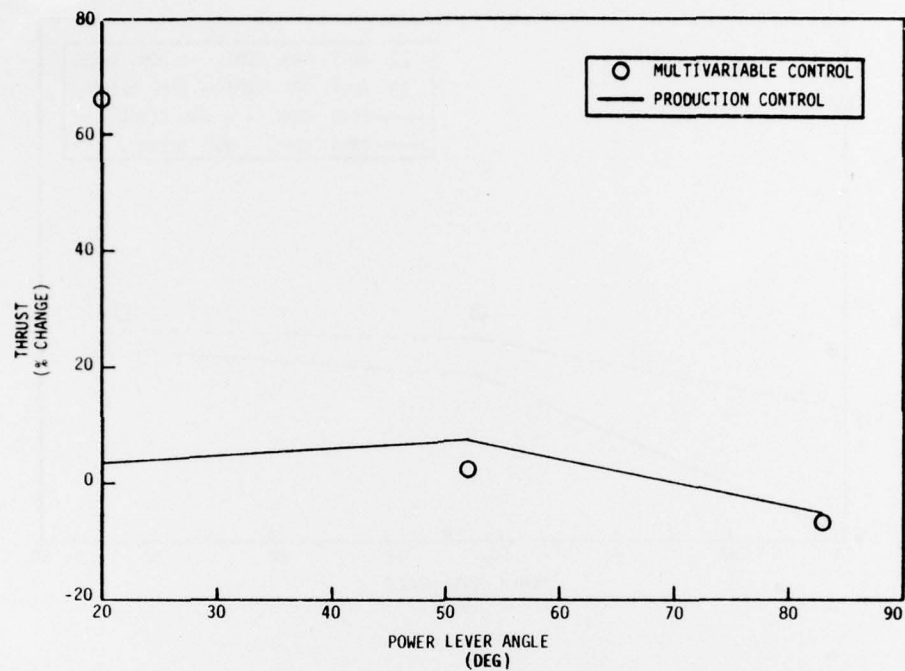


Figure I.5 (Continued)

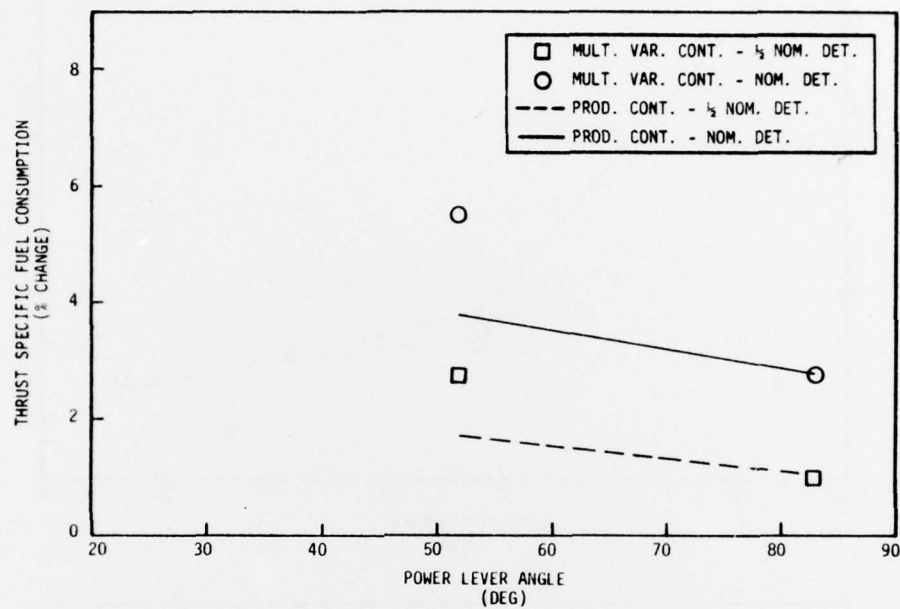


Figure I.6 Per Cent Variation in Steady-State Performance at 10,000 Ft, Mach Number = 0.9

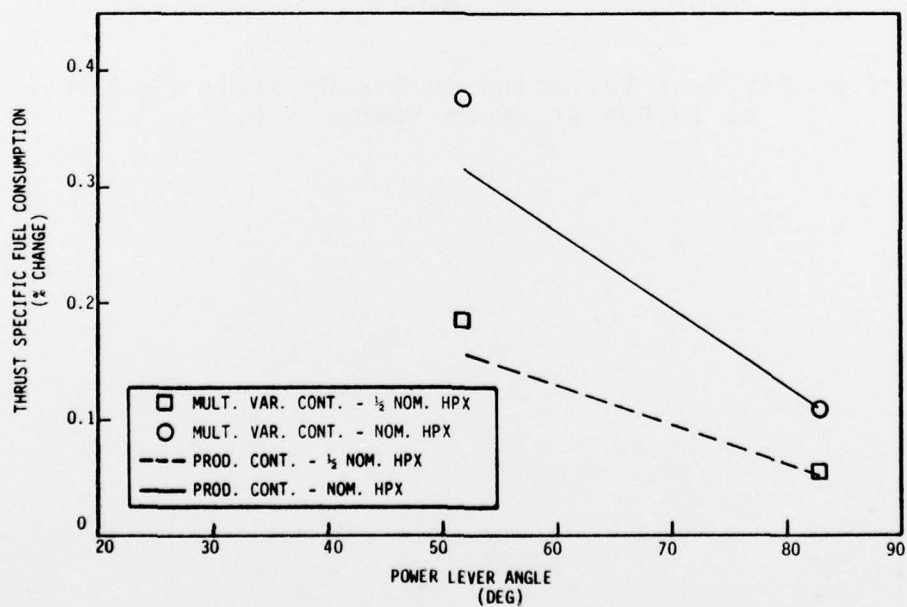
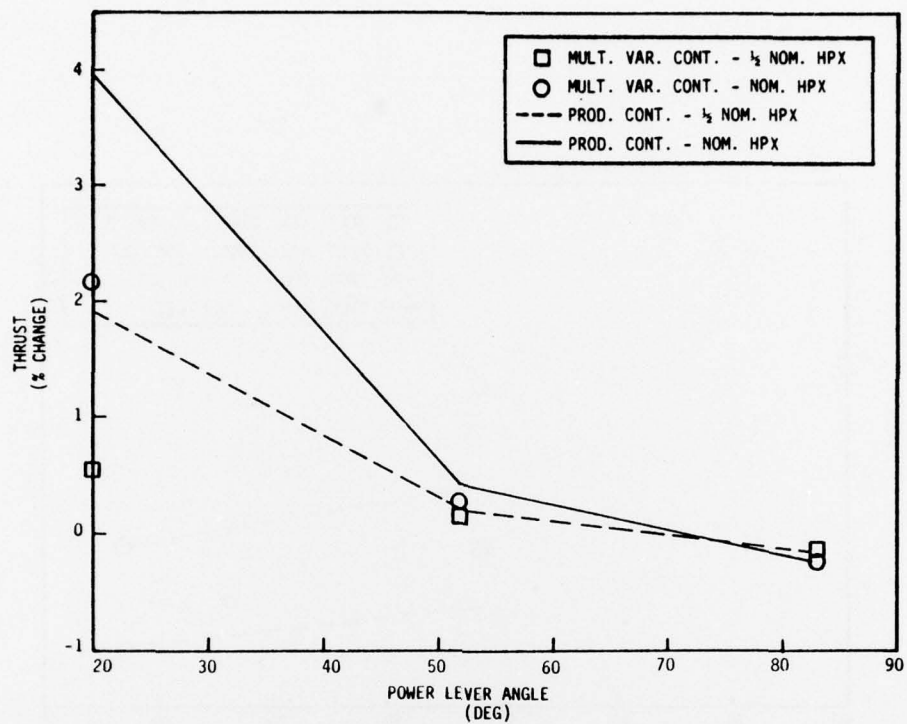


Figure I.6 (Continued)

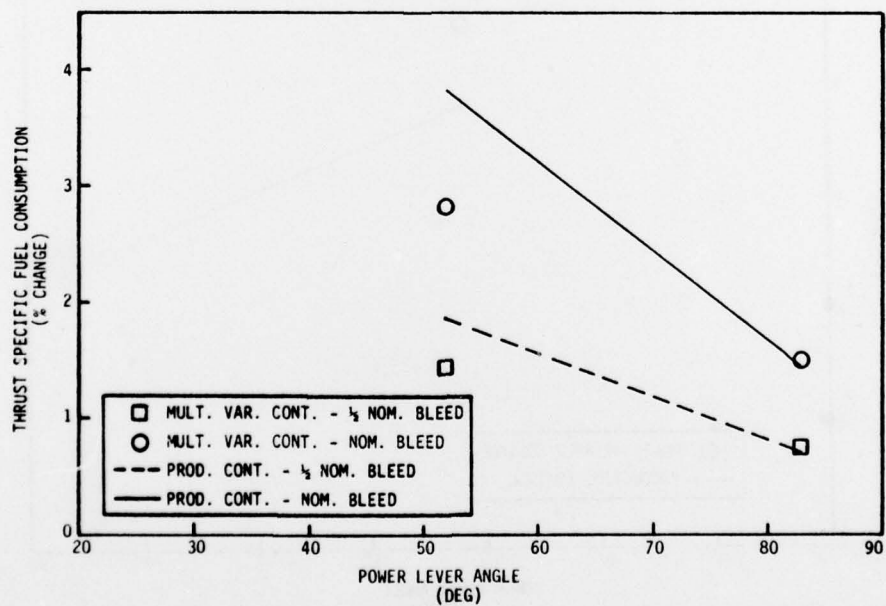
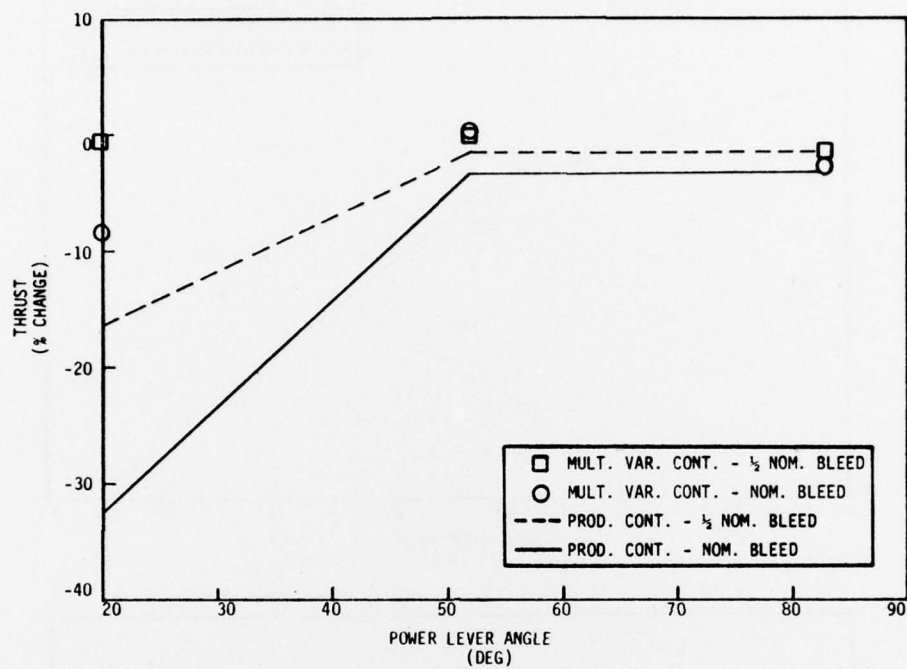


Figure I.6 (Continued)

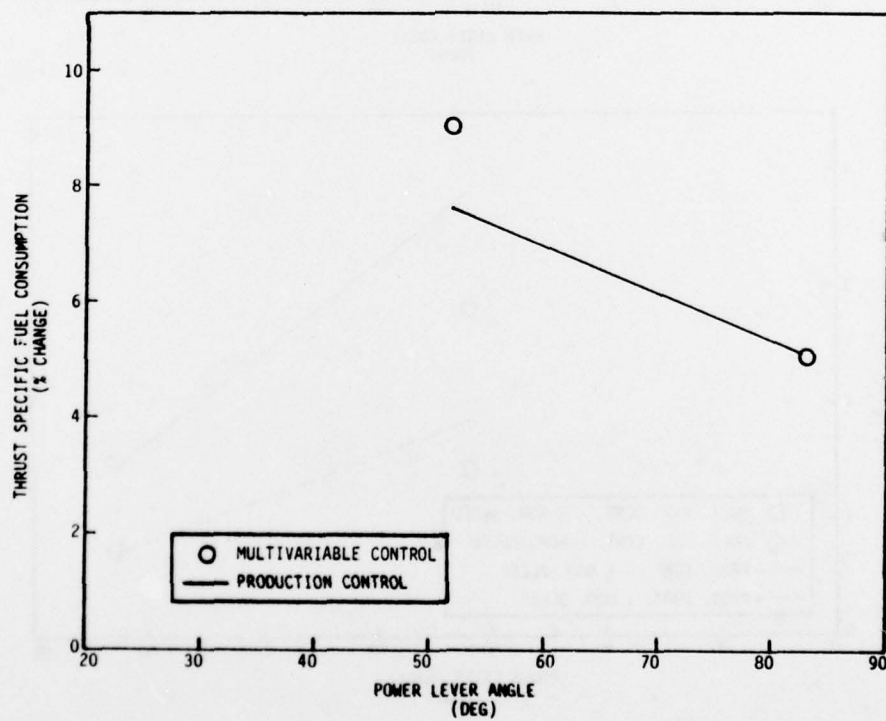
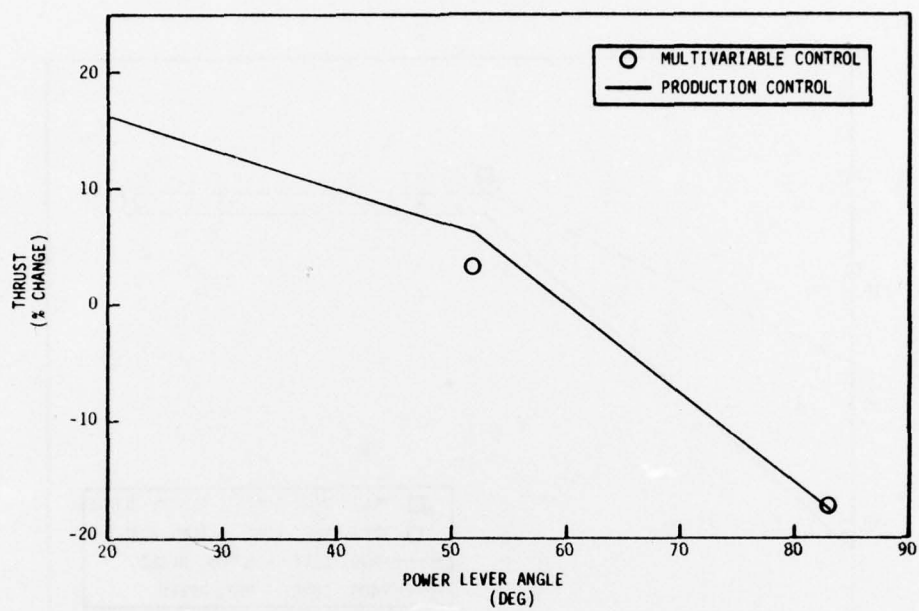


Figure I.6 (Continued)

APPENDIX J

EXAMPLE OF LINEAR SPLINE SCHEDULE GENERATION

Section 4.4 of Volume I describes the utilization of splines to fit operating data. This procedure is useful in generating gain and reference point schedules. An example of this procedure is given below for the generation of an optimum fan operating line schedule. The program flow diagram is shown in Figure J.1. Schedule data for two dimensional tables are read in and weighted according to the importance of the operating point. Table J.1 shows a list of 62 steady state operating points represented by values of corrected fan speed and airflow. Higher weights are attached to low altitude points. An initial set of breakpoints are chosen and the data is partitioned into regions as shown in Figure J.2. The least squares problem is shown below:

$$\begin{bmatrix} y_1 \\ \vdots \\ y_p \\ \hline y_{p+1} \\ \vdots \\ y_q \\ \hline y_{q+1} \\ \vdots \end{bmatrix} = \begin{bmatrix} x_1 & 1 & 0 & 0 & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ x_p & 1 & 0 & 0 & 0 \\ \hline 0 & 0 & x_{p+1} & 1 & 0 \dots \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ 0 & 0 & x_q & 1 & 0 \dots \\ \hline 0 & 0 & 0 & 0 & x_{q+1} \\ \vdots & \vdots & \vdots & \vdots & \vdots \end{bmatrix} \begin{bmatrix} a_1 \\ b_1 \\ \hline a_2 \\ \vdots \\ b_2 \\ \hline \vdots \end{bmatrix} \quad (J.1)$$

The parameter constraints representing continuity of splines at the breakpoints is represented as follows:

$$L\theta = 0 \quad (J.2)$$

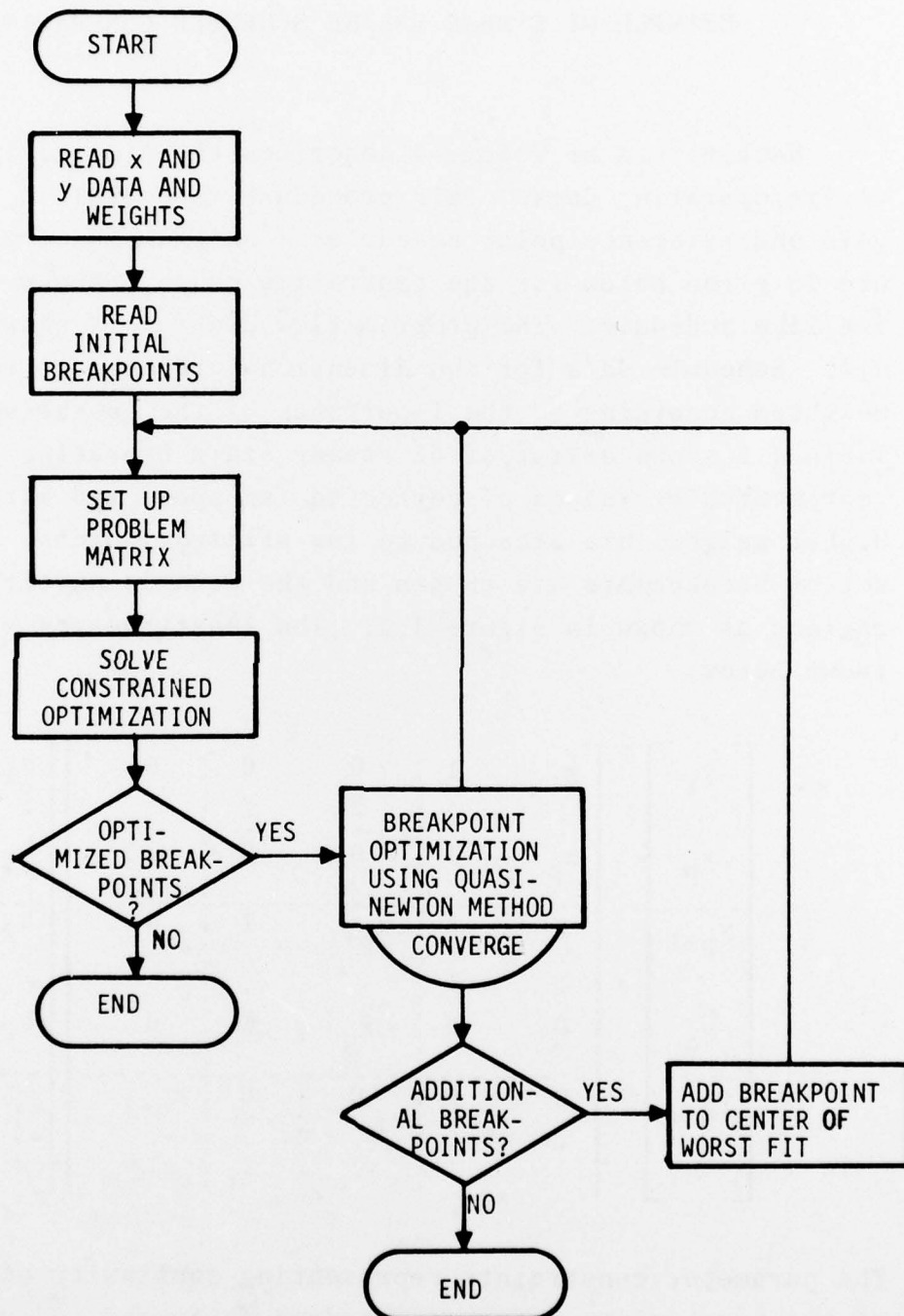


Figure J.1 Spline Table Generation Program

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Table J.1

Weighted Operating Point Data List

SPLINE FITTING PROGRAM: FAN OPERATING LINE

XS	WCF	YS	SNFCR	W = WEIGHTING	
XS	.73600+02	YS	.38930+04	WS	20
XS	.87200+02	YS	.45660+04	WS	1
XS	.94500+02	YS	.49440+04	WS	1
XS	.99800+02	YS	.53530+04	WS	1
XS	.11110+03	YS	.59130+04	WS	1
XS	.11900+03	YS	.63240+04	WS	1
XS	.11900+03	YS	.63250+04	WS	1
XS	.12400+03	YS	.66490+04	WS	20
XS	.13080+03	YS	.69030+04	WS	1
XS	.13150+03	YS	.69120+04	WS	1
XS	.13170+03	YS	.69420+04	WS	1
XS	.14050+03	YS	.72710+04	WS	1
XS	.14100+03	YS	.73420+04	WS	1
XS	.14100+03	YS	.73420+04	WS	1
XS	.14580+03	YS	.74670+04	WS	1
XS	.14600+03	YS	.74740+04	WS	1
XS	.14990+03	YS	.75990+04	WS	1
XS	.14990+03	YS	.75990+04	WS	1
XS	.15200+03	YS	.77150+04	WS	20
XS	.15600+03	YS	.78280+04	WS	0
XS	.15760+03	YS	.78780+04	WS	1
XS	.15770+03	YS	.79250+04	WS	1
XS	.16000+03	YS	.79860+04	WS	1
XS	.16090+03	YS	.79930+04	WS	1
XS	.16360+03	YS	.81610+04	WS	1
XS	.16470+03	YS	.81730+04	WS	1
XS	.16600+03	YS	.82480+04	WS	1
XS	.16780+03	YS	.83730+04	WS	1
XS	.17000+03	YS	.84080+04	WS	1
XS	.17000+03	YS	.83700+04	WS	1
XS	.17730+03	YS	.86170+04	WS	1
XS	.17870+03	YS	.86420+04	WS	1
XS	.18000+03	YS	.87560+04	WS	20
XS	.18200+03	YS	.88140+04	WS	1
XS	.18240+03	YS	.87650+04	WS	1
XS	.18700+03	YS	.89680+04	WS	1
XS	.19000+03	YS	.90580+04	WS	1
XS	.19100+03	YS	.91660+04	WS	1
XS	.19100+03	YS	.91510+04	WS	1
XS	.19270+03	YS	.93050+04	WS	1
XS	.19650+03	YS	.92710+04	WS	1
XS	.19740+03	YS	.92800+04	WS	1
XS	.19900+03	YS	.93610+04	WS	1
XS	.19900+03	YS	.93610+04	WS	1
XS	.20240+03	YS	.94910+04	WS	1
XS	.20300+03	YS	.94380+04	WS	20
XS	.20400+03	YS	.94840+04	WS	1
XS	.20700+03	YS	.95400+04	WS	1
XS	.21270+03	YS	.96990+04	WS	1
XS	.21400+03	YS	.97500+04	WS	1
XS	.21600+03	YS	.98970+04	WS	1
XS	.21800+03	YS	.98540+04	WS	1
XS	.21830+03	YS	.99110+04	WS	1
XS	.22370+03	YS	.10137+05	WS	1
XS	.22500+03	YS	.10144+05	WS	1
XS	.22640+03	YS	.10439+05	WS	1
XS	.22980+03	YS	.10273+05	WS	1
XS	.23000+03	YS	.10400+05	WS	1
XS	.23000+03	YS	.10283+05	WS	20
XS	.23160+03	YS	.10493+05	WS	1
XS	.23250+03	YS	.10440+05	WS	1
XS	.23250+03	YS	.10440+05	WS	1

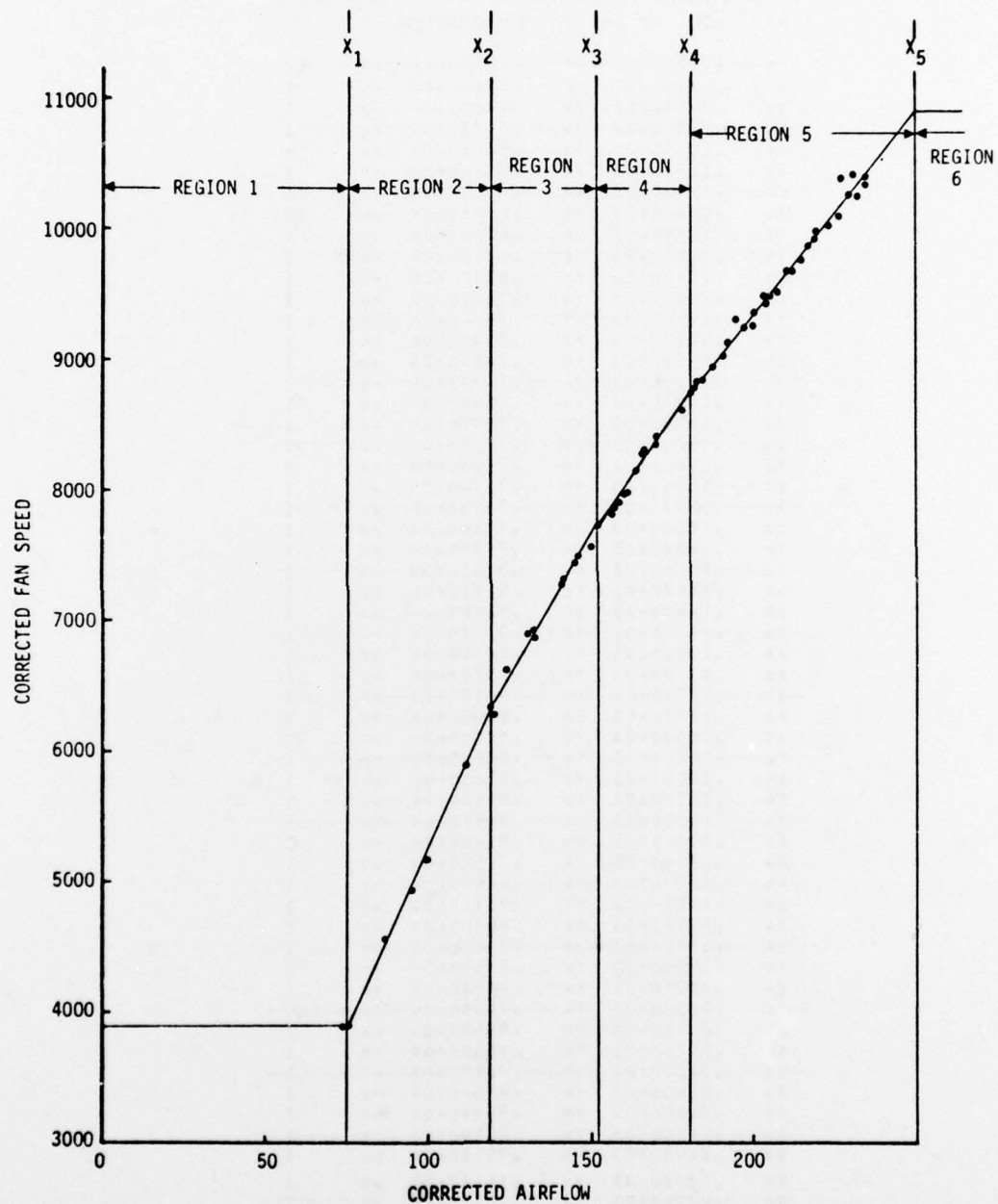


Figure J.2 Spline Schedule Generated from Data

where

$$\theta^T = [a_1, b_1, \dots, a_5, b_5] \quad (J.3)$$

and

$$L = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ X_1 & 1 & -X_2 & -1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & X_2 & 1 & -X_3 & -1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & X_3 & 1 & -X_4 & -1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & X_4 & 1 & -X_5 & -1 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \end{bmatrix} \quad (J.4)$$

where the schedule terminates in flat segments represented by

$$a_1 = a_5 = 0$$

The optimization problem is solved by adjoining the least squares problem with Lagrange multipliers for the constraints forming the algebraic problem:

$$\begin{bmatrix} A^T A & L^T \\ L & 0 \end{bmatrix} \begin{bmatrix} \theta \\ \lambda \end{bmatrix} = \begin{bmatrix} A^T y \\ 0 \end{bmatrix} \quad (J.5)$$

The solution to (J.5) is determined by decomposition of the linear system.

The program will optimally minimize the residuals by moving the breakpoints in the table. This optimization procedure utilizes a Levenberg-Marquart nonlinear least squares algorithm which does not require explicit calculation of the

derivative of the mean residuals in each region with respect to the breakpoints. Also, additional breakpoints may be added to improve the fit. In this case, a breakpoint is inserted in the center of a region which has the largest mean residual and the optimization is repeated.

The optimal spline fits are shown in Figure J.2 for these breakpoints and the mean residuals are tabulated in each region as shown in Table J.2. The effects of optimized breakpoints and the improvement in fit using additional breakpoints were not explored in this example.

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Table J.2
Results of Schedule Generation
SPLINE FITTING PROGRAM: FAN OPERATING LINE

ITERATION NUMBER: 0

PARAMETERS

a₁ .00000
b₁ .38862+04
a₂ .56154+02
b₂ .24679+03
a₃ .38791+02
b₃ .18194+04
a₄ .36867+02
b₄ .21089+04
a₅ .31032+02
b₅ .31628+04
a₆ .00000
b₆ .10921+05

MEAN ERROR TABLE		NO. POINTS		BREAK	
REGION 1	MEAN ERR=	.68408+01	20.0	BREAK 1=	.73600+02
REGION 2	MEAN ERR=	.92518+02	6.0	BREAK 2=	.11900+03
REGION 3	MEAN ERR=	.18006+02	50.0	BREAK 3=	.15200+03
REGION 4	MEAN ERR=	.23631+02	32.0	BREAK 4=	.18000+03
REGION 5	MEAN ERR=	.51724+02	67.0	BREAK 5=	.25000+03
REGION 6	MEAN ERR=	.00000	NO. POINTS=		
MEAN TOTAL ERROR=		.36960+02			

APPENDIX K DESIGN OF FTIT ESTIMATOR

The FTIT estimator can be designed directly from Figure K.1 showing the transfer functions from the two inputs to the filter outputs. The design procedure will assume that the feedback, α , is small and the gains will be calculated for $\alpha = 0$. Then, α will be chosen to provide faster step response.

The first step is to determine the filter breaks, λ_1 , λ_2 , and λ_3 . The first break, λ_1 , determines the frequency

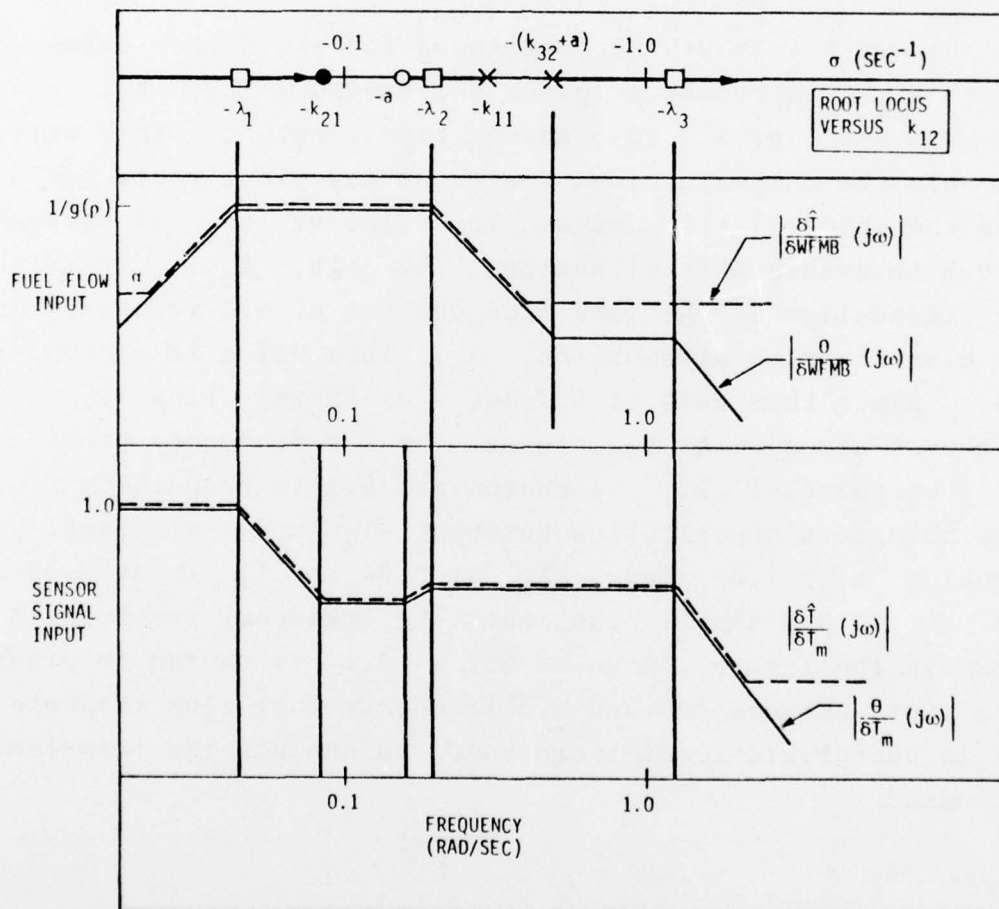


Figure K.1 Asymptotes of Frequency Response of FTIT Sensor Compensation Showing Pole-Zero Locations as a Function of Estimator Gains and Feedforward Parameter

at which fuel flow and temperature sensor inputs have the same effect. At lower frequencies than λ_1 , the sensor inputs have more effect on estimator output than fuel flow. The second root, λ_2 , determines the bandpass of fuel flow inputs. The largest magnitude root, λ_3 , determines the noise attenuation frequency of both inputs.

The first order model for the FTIT sensor is dominated by the slow component of the response. The estimator is designed to track this input to set steady performance. The higher frequency components of the response are determined by schedule and fuel flow inputs. The sensor model parameter, a , is chosen to be $1/5 \text{ sec}^{-1}$.

Figure K.1 shows the root locus for the filter poles. The gain, k_{11} , is chosen to place the bandpass lag, λ_2 , at $0.3 - 0.5 \text{ sec}^{-1}$ or a 2 to 3 second time constant. This will decouple the estimator from the transient plant roots but not from the integral trim roots. The value of k_{11} is chosen to be 0.5 to assure this situation. The gain, k_{32} , determines the attenuation of the fuel flow channel at mid-frequency and the overall noise attenuation, λ_3 . This value is chosen at 0.5 to place this pole at 0.7 sec^{-1} as shown. Finally, k_{21} is chosen along with k_{12} to set the low frequency break at λ_1 . The value of k_{21} is chosen at +0.1 to keep the approximate pole/zero cancellation between $-\lambda_2$ and $-a$. Finally, choosing $k_{12} = 2.0$ places λ_1 at 0.04 sec^{-1} , λ_2 at 0.33 sec^{-1} and λ_3 at 3.0 sec^{-1} . The resulting frequency response is shown in the figure. A value of $\alpha = 0.1$ is chosen to provide 10:1 ratio between low and mid-frequency fuel flow response and an acceptable feedforward value to enhance the transient response.